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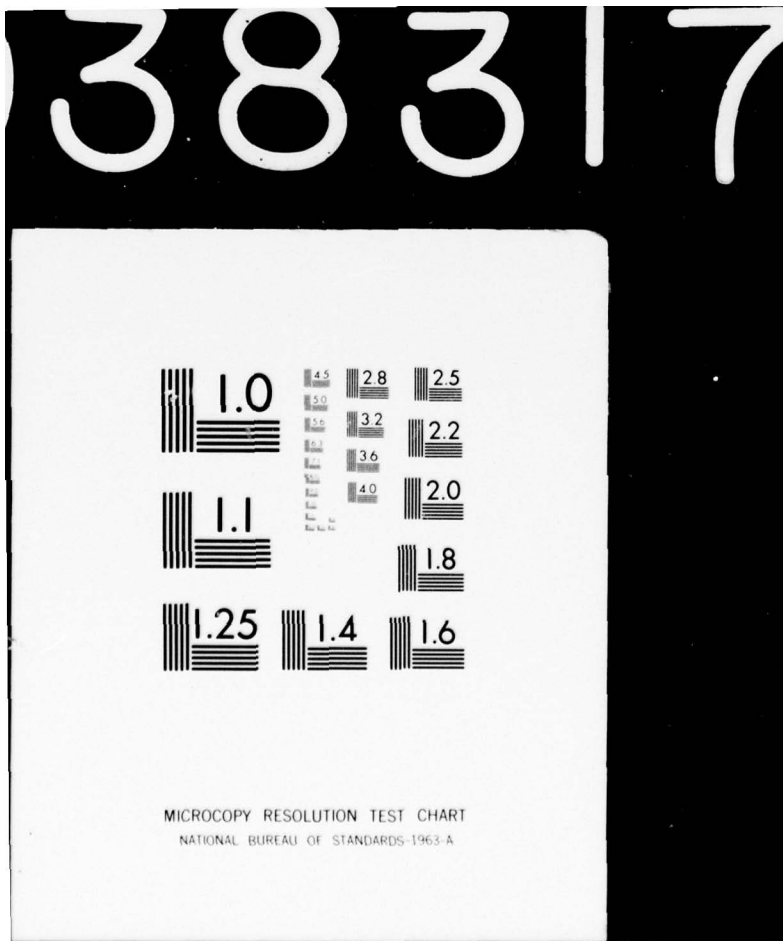
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## RELIABILITY STUDY OF SINGER

Volume II  
User's Manual

DEPARTMENT OF CIVIL ENGINEERING  
Virginia Polytechnic Institute and State University  
Blacksburg, Virginia 24061

January 1977

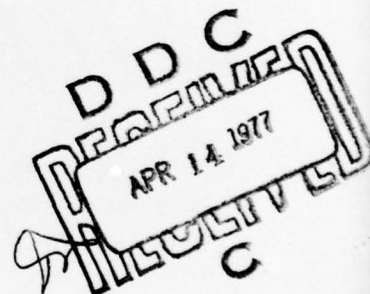
Final Report

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Director  
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Washington, DC 20305

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This technical report has been reviewed and is approved for publication.

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The second volume of this report is principally developed for the user, as an aid in the use and modification of the SINGER code. The objective is to document the experience gained through the study of problem solutions and code details. In addition, this volume includes the description of new subroutines developed and a listing of the current version of the code.		



## PREFACE

This is the second volume of a two-volume report on the work performed under the contract F29601-75-C-0050.

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## SECTION I

### INTRODUCTION

The original version of the SINGER program was developed under contract F29601-73-C-0022. Since the completion of that phase of the development, significant experience has been gained working with the program. A variety of problems has been studied, including those with steel elements and those with reinforced concrete elements. Much of the detailed understanding acquired has been documented for future reference, and code modifications have been introduced to correct errors or to improve computational accuracy. The objective of this volume is to document these areas of study for future reference.

The organization of the documentation is in the following form:

1. Additional user assistance for the preparation of input data and for the interpretation of results;
2. Additional program details not available in previous documents;
3. New subroutine documentation;
4. Listing of the program code in its current form.

## SECTION II

### ADDITIONAL USER ASSISTANCE

The objective of this section is to describe alterations and clarifications in the preparation of problem data for input and in the explanation of some output details consistent with the current status of the program. The input and output features of the original SINGER code were both documented in the User's Guide [1]. A broader understanding of the program has provided the basis for expanding this documentation for the benefit of the user. Input data preparation is discussed in Addenda to the User's Guide and Error Controls. Some output characteristics are discussed in Minimization and Convergence Problems and Strain Discontinuity.

#### ADDENDA TO THE USER'S GUIDE

Although the basic structure of the original User's Guide is still valid, some points require correction or clarification. In addition, a few modifications need to be noted. These items are listed below; the page numbers shown refer to the original User's Guide [1].

##### 1. Corrections:

- a. (p. 23), footnote no. 3: The parameter  $k$ , which defines the characteristic of the drop-elastic unloading curve for concrete, must be greater than zero or less than or equal to 1 to be an acceptable value.
- b. (p. 34), footnote no. 4: If the user inputs the number of bars and the bar size number, subroutine



BARS will calculate the area, bar size diameter, and perimeter.

- c. (p. 41), footnote no. 1: If no initial conditions are specified and IANAL = 0, a static analysis is performed according to specified load increments. If no initial conditions are specified and IANAL = 1, a static analysis is skipped and a dynamic analysis is performed.
- d. (p. 42), card 3/R, columns 1 - 5: Format I5 should be format I4, 1X.
- e. (p. 43), footnote no. 3; paragraph 3: For vertical slopes, i.e.,  $t_{i+1} - t_i = 0$  (where  $t$  represents time), the forcing function value is set to  $F_i$  in subroutine TABL.

2. Clarifications:

- a. (p. 18), footnote no. 6: The maximum relative error for determining the converged state of minimization (SERR) cannot be less than  $\sqrt{\text{EPS}}$ , where currently  $\text{EPS} = 1.E - 14$ ; otherwise an error message is printed. If this value is input as zero, the program sets its value to  $\sqrt{\text{EPS}}$ .
- b. (p. 22-23), Material Data Block: User input material functions must be defined by seven points, each with a corresponding stress and strain value. None of these strain values can be in descending order. The concrete material must have negative stress and strain values,



but the crushing strength should be a positive number.

The stress value at point 5 is used to indicate a default function for confined concrete for stress and strain modification due to confinement effects. If this stress value is zero, the stress and strain values at point 5 and the strain at point 6 are computed; if this stress is nonzero, a user input function is indicated and no additional computations are needed. (Although this computation affects the material function, it is not done in the input sequence until after the stirrup data are known.)

Both unconfined and confined concrete material functions should be input for a problem using reinforced concrete elements. If a single concrete material is desired for the element, both functions can be input with identical values.

The steel stress-strain values input by the user should be positive.

The strain corresponding to the peak stress of the user input function for concrete is the reference point for determining the unloading characteristics; unloading prior to reaching this reference strain value is a straight line parallel to the initial segment slope (path a b in figure 1); unloading after passing this strain value follows the drop-elastic path determined by the parameter  $k$ , where  $0 < k \leq 1.0$

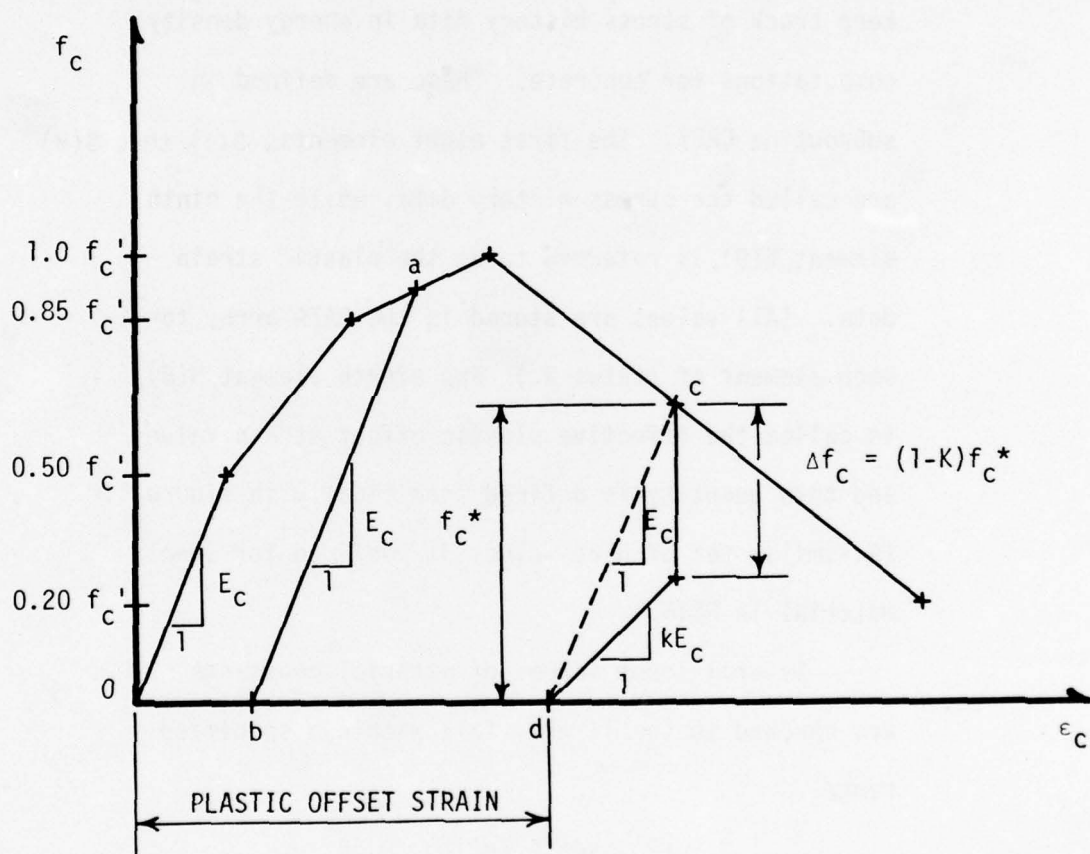


FIG. 1 CONCRETE MATERIAL PARAMETER DEFINITIONS

(path c d in figure 1). The drop-elastic parameter  $k$  is used to determine the length of the vertical stress segment as shown in figure 1.

The array  $S$  containing nine elements is used to keep track of stress history data in energy density computations for concrete. These are defined in subroutine CRET. The first eight elements,  $S(1)$  thru  $S(8)$  are called the stress history data, while the ninth element,  $S(9)$ , is referred to as the plastic strain data. (All values are stored in the DATA array for each element of status 3.) The eighth element,  $S(8)$ , is called the effective plastic offset strain value, and this quantity is defined specifically in figure 1. (A similar set of nine values is defined for steel material in REIN.)

Several input values of material constants are checked to see if they fall within a specified range.

$$0. \leq [\text{Poisson's Ratio}] < 0.50$$

$$0. \leq [\text{Shear modulus}] < 15 \times 10^6 \text{ psi}$$

$$0. \leq [\text{Material density}] < 0.50 \text{ lb/in}^3$$

$$0. < [\text{Unloading constant}] \leq 1.0$$

$$2.5 \times 10^3 \text{ psi} \leq \begin{bmatrix} \text{Unconfined concrete strength} \\ \text{Confined concrete strength} \end{bmatrix} \leq 8 \times 10^3 \text{ psi}$$

$$33 \times 10^3 \text{ psi} \leq [\text{Steel yield stress}] \leq 75 \times 10^3 \text{ psi}$$

- c. (p. 28-39), Element Data Block: Each reinforced concrete element requires the element parameter card and the concrete data card. It is advisable to have at least one longitudinal reinforcement group since no check is made to see if there is none, and some DO loops are executed over the number of groups. The lateral reinforcement card is optional. (Stirrups do not enter directly into the element energy computations.) An unreinforced section can be simulated by introducing a very small nonzero steel reinforcement group area.

Each steel wide flange element requires only the wide flange reinforcement card; and a leaf spring element (if used) requires only the leaf spring flexibility card.

The lateral reinforcement parameter  $A_v$  (p. 35) refers to the cross sectional area of the stirrup at a single location, i.e. the cross sectional area cut by a plane passing normal to the stirrup.

- d. (p. 44), Forcing Function Data Block: To input a static load which is generated by a forcing function in prescribed load increments, the following data are required: joint no. (col. 1-5), direction indicator (col. 11), the reference function number (col. 16-19),  $k$  (col. 20), 1.0 (SF) (col. 21-30), and  $LA = 0$ ,  $TA = 0$ ,  $TP = 0$  (col. 31-60). In a static analysis, time is used as a dummy variable for defining the domain of



the forcing function. The sign (+ or -) of the force should be associated with the scale factor value input in the Forcing Function Data Block (p. 44).

3. Modifications:

- a. (p. 17-18), Control Data Block: Card No. 2, Columns 21-25, have been changed from A1, 4X to 2A1, 3X. Column 22 will contain the item MPRINT = secondary print level flag.

M = suppress paging

S, d\* = standard paging

Card No. 3, Columns 6-10, have been changed from 5X to 3X, I2 with the addition of the variable IINITD, read initial guess of displacements (activated if this value is negative). This option may be selected if the user wishes to input an initial guess of the displaced configuration of the structure rather than have SINGER make the initial guess. The initial guess displacements should be placed at the end of the Forcing Function Data Block, after the zeros card, in 8E10.0 format. They should be in the order of the joint numbers and the order of X, Y, and rotation at each joint. The joint displacements should be followed by the internal node displacements for all the elements in the order of the element numbers. This gives a total of initial displacements equal to the number of degrees of freedom at the joints plus the number of elements. The displacements corresponding to the joints should be normalized by the

average element length. Columns 61-65 have been changed to I5 to add the variable INKS, output print option. This gives the user the choice to specify the time intervals at which the output will be printed. For example, if the user wants the results printed at every 10 time increments, the value 10 should be placed in columns 64-65. This will give results according to IPRINT, which is also specified at every 10 time increments. The intermediate time steps will display the time, function value, and displacements in a condensed nondimensional form.

- b. The new subroutines DEFO and STRN, written to improve the directional properties of the element model (see section V, Volume I, and also section IV, Volume II), redefine the element deformation components. Since the existing subroutines LEAF and FAIL utilize the old component definitions, both should be studied for possible modifications before all four subroutines are used within the same program.

Also, these two new subroutines do not distinguish between finite and infinitesimal joint rotations. The same transformations are used regardless of the input parameter ILIN (p. 17).

Due to the function used to compute the arc tangent value in the new DEFO subroutine, values of joint rotations are valid within the range of  $(-\pi < \theta < \pi)$ . Errors will be generated in this evaluation for rotations outside this range.

## ERROR CONTROLS

In addition to inevitable roundoff errors, the dynamic response predictions of SINGER are subject to the following errors:

1. Temporal discretization error
2. Iteration error
3. Spatial discretization error
4. Quadrature error

The temporal discretization error is caused by the representation of the motion during a time step in terms of a finite power series in time, and the iteration error is caused by the termination of the search process after a prescribed accuracy has been achieved. These two errors are controlled automatically by SINGER [2].

The spatial discretization error is caused by the finite element representation of the continuum model of the beam-column, and the quadrature error is caused by the numerical integration of the internal-energy density over the volume of the finite element. These two errors must be controlled by the user to assure accurate energy predictions. A detailed description of error controls in energy evaluations is presented in section IV of Volume I of this report.

## MINIMIZATION AND CONVERGENCE PROBLEMS

Listed below are the basic components of a general problem which may significantly influence the solution process:

1. Control parameters
2. Model characteristics
3. Load increments

1. Control parameters: The control parameters include the minimization convergence tolerance and the error measures. The state of convergence of the minimization process is controlled by the minimization tolerance parameter (SERR), a user input quantity which defines a limit to the stepsize used in a linear minimization. Also, an error value is computed which is intended to provide a measure of the quality of the converged state, referred to as the iteration error [2]. This error measurement is derived from the largest of the unbalanced generalized forces at the joints. In the program, this value is printed as the FULL TIME ERROR. For a static problem, this is the only error measure and it does not control the response in any way. For a dynamic problem, a half time error is computed, which is an error measure at the middle of the time step. It attempts to measure the truncation error due to approximate representation of the displacement function over a time step [2]. The size of the time step is controlled by the half time error.

The convergence tolerance parameter chosen too large can produce inaccurate results because the process terminates before a well defined minimum has been reached. A lower limit is placed on the parameter determined by the computer word size [1]. A range of values found to produce acceptable results for most problems is  $1. \times 10^{-5}$  to  $1. \times 10^{-7}$ . It should also be noted that since the previous converged state is the basis for initialization of the next increment, there is some interaction between successive increments. However, the exact significance of this interaction with respect to solution accuracy is not well defined.



The error measures are computed during the solution process. It is possible to reach a converged state with respect to the convergence tolerance specified but still have a poor error measure. This may be due to a complex energy surface in the neighborhood of the minimum state chosen. Experience has shown that accurate results (measured by symmetry in the element response) are achieved when the full time error is smaller than  $1. \times 10^{-2}$ ; a value of  $1. \times 10^{-1}$  is questionable; and values larger than  $1. \times 10^{-1}$  usually produce inaccurate response predictions. Good results are associated with the smaller values, such as  $1. \times 10^{-4}$  or smaller.

The half time error measure in dynamic problems is compared with a tolerance  $1. \times 10^{-3}$  (CRITU) for determining an acceptable converged state. (The magnitude of this error is usually larger than the full time error.) The time step is reduced to a magnitude of 0.60 of the previous value if this convergence limit is not achieved. The minimum time step defined in the code is  $1. \times 10^{-7}$ . It is also possible that the time step could be automatically increased to protect against roundoff error in computations. This occurs if the half time error is less than a fixed value,  $1. \times 10^{-9}$  (CRITL). The next time interval is made 1.85 times the previous interval. (For a discussion of the dynamic error control logic, see Ref. [2], pages 50-53.)

2. Model characteristics: The most significant modeling characteristic which may influence the convergence process is the element distribution. The distribution chosen must accurately represent the continuum being modeled as reflected in how well the energy distribution can be reproduced. Extremely nonlinear material characteristics,

such as an elastic-plastic bilinear function, introduce complexities into the energy distribution, frequently occurring as localized energy concentrations at concentrated loads and totally restrained joints. Any region which is likely to develop large strain gradients should be subdivided to more accurately represent the energy concentration. It appears that members should be subdivided so that no one element contributes more than 50 percent to the energy function. The effect of poor element distribution can be reflected in the following ways: Large strain discontinuities may occur at the joints (see section VI, Volume I); and the accuracy of the continuum response prediction may be unsatisfactory.

3. Load increments: The magnitude of load increments can cause various convergence problems. A relatively large load increment may produce an equilibrium state so far removed from the previous state that convergence may be difficult to achieve, particularly if complexities due to nonlinear effects exist in the total energy surface. Also, the structure may reach a state of reduced stiffness so that a small change in load produces a relatively large change in the corresponding displacements. This has been observed in the steel wide flange beams and reinforced concrete beams loaded to failure (see section VI, Volume I), and also in the study of the elastica [3]. The effect of this difficulty can usually be reduced or eliminated by decreasing the load increments.

Another source of convergence difficulty occurs as the predicted response approaches the limit point of the equilibrium path. If the load is incremented to a value very near the limit point, an extremely

large displacement state may result with a poor error measure indicated. If the load level is incremented above the limit point, the solution search produces such extremely large values that the computer control system terminates the problem. There is no automatic termination check made in the program to detect this condition.

For most structures, the choice of load increments is not critical. The minimization algorithm appears to be a stable process and convergence is usually achieved for the load increments specified. The solution time may be longer for a problem containing a few large load steps as compared to one with several small load steps because the number of iterations for convergence for each large increment may be significantly increased. However, the solution accuracy may also be increased for some problems.

Two types of normal convergence may occur. The usual and most desirable type of convergence occurs when the stepsize used in a linear minimization is reduced to the specified tolerance. The other type occurs when a zero stepsize has occurred in the direction of a linear minimization. This type of convergence is indicated by the printed message NO MOTION IN THE LINEAR MINIMIZATION. This condition may occur during an apparently normal minimization process. It may also occur when an element yields. When yielding occurs, the minimization at that load level is repeated with the status of the yielded member changed. Since yielding may have occurred only at the outer fibers of the element, the strains at the integration points may still be within the elastic range. If this is the case, no change occurs in the solution vector and no motion is indicated.



Probably the most important consideration in obtaining accurate predictions of nonlinear structural response is the user's understanding of the system behavior. This is an indispensable aid in deciding how to subdivide the members and simplify the mass discretizations. It may be necessary to obtain satisfactory results through a trial and error procedure. Also, the user can study a test member to determine the subdivision necessary to accurately represent the expected load-deformation states (see section IV, Volume I).

#### STRAIN DISCONTINUITY

If one element is required to represent large changes in strain within its length (of the order of 50 times the yield strain or larger), a strain discontinuity may occur with respect to an adjacent element which is not so severely strained. Large strain gradients occur in regions of highly localized deformations, such as the region near a concentrated load laterally applied to a reinforced concrete beam after the steel reinforcement begins to yield. The discontinuities may appear not only as differences in magnitude, but also in sign. The solution process does not appear to be adversely affected by these discontinuities. However, since the stress resultants depend on the stress values computed across the sections at the ends of an element, the strain discontinuities produce stress resultant discontinuities.

The strain discontinuity problem can be improved by subdividing the member into smaller elements within the localized region. In this manner, each element is required to represent a smaller strain change along its length. Discontinuities may still occur, but their

magnitudes should be reduced since the energy distribution can be better represented. A more complete discussion with a demonstration of these effects is presented in section VI, Volume I, of this report.

### SECTION III

#### ADDITIONAL PROGRAM DETAILS

Some program details have not been adequately explained in previous documentation. Such detailed descriptions are important for understanding the program structure, and they provide the basis for making additional modifications to the code. Program details discussed in this section include a description of selected variables, the organization of the array storage scheme called DATA and KDATA, and the procedure to be used for modifying the fixed storage allocation built into the program.

#### DESCRIPTIONS OF SELECTED VARIABLES

The variables described here are primarily those which determine the location of Gauss points and end points for both steel wide flange and reinforced concrete elements. The objective is to relate the names used in the code to the physical location of the points in the elements. The Gauss points define the locations at which energy density values are computed, and the end points are used in part as stress points from which to compute the element stress resultants. These point locations are shown in figure 6 for a reinforced concrete element and in figure 7 for a wide flange element (pages 31 and 34, respectively).

The location of a point for any element type is defined by an x coordinate and a y coordinate. The following list shows the variable names associated with the locations for both element types.

	Variable Names		
	X Location	Y Location	
		Gauss Point	End Point
Steel wide flange	XPI	YGP	YFIBR
Reinforcing bar	XPI	YBAR	YBAR
Concrete (confined and unconfined)	XPI	YGP	YFIBR

All elements use the same x location variable XPI as an array with the following form: XPI(J,M)

J =	section number
M =	element number

The section number refers to the cross sections located at the three Gauss coordinates in the longitudinal direction (for the Gauss point locations), and at the ends of the element for the end point locations.

The y location names are made identical where possible. The Gauss point locations for each type are named YGP, used as an array with the following form:

YGP(I,M)	I = y location number
	M = element number

The locations on a cross section are shown in figures 2 and 3 for the two element types. Points defined by I = 1, 2 and 6, 7 are at the Gauss locations for the flange or cover thickness. The remaining three points defined by I = 3, 4, and 5 are at the Gauss locations for the web or confined concrete depth.

The y locations for the end points use the same array name YFIBR with the following form:

YFIBR(I,M)	I = y location number
	M = element number

The locations are also shown on the cross sections of figures 2 and 3. There is a total of 11 points for each element type. The points



GAUSS POINT  
LOCATIONS

YGP(1,M)

YGP(2,M)

YGP(3,M)

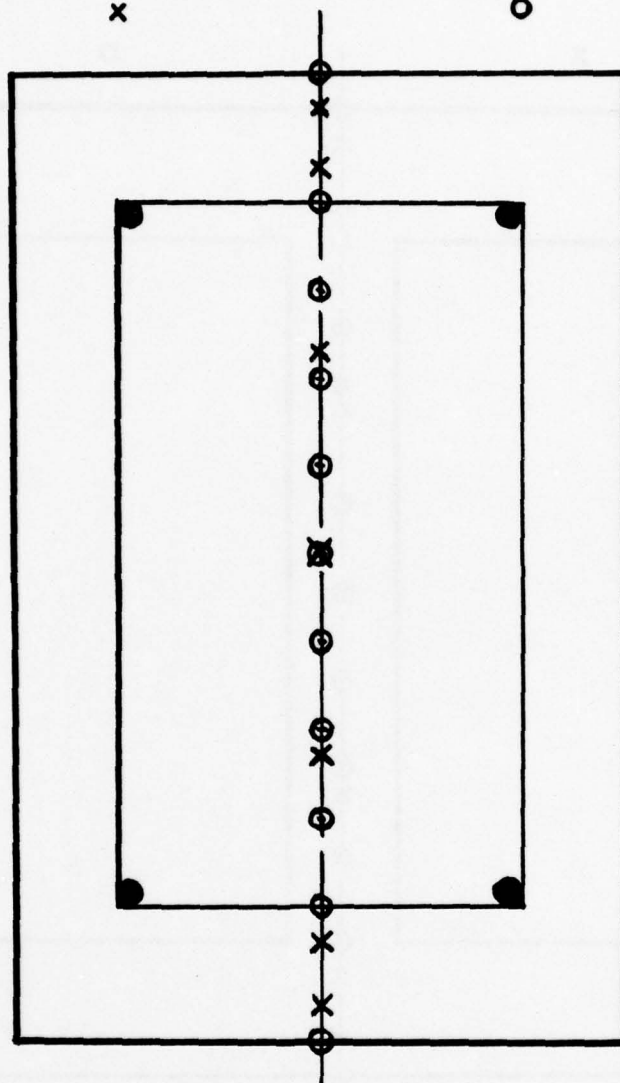
YGP(4,M)

YGP(5,M)

YGP(6,M)

YGP(7,M)

x



END POINT  
LOCATIONS

YFIBR(1,M)

YFIBR(2,M)

YFIBR(3,M)

YFIBR(4,M)

YFIBR(5,M)

YFIBR(6,M)

YFIBR(7,M)

YFIBR(8,M)

YFIBR(9,M)

YFIBR(10,M)

YFIBR(11,M)

FIG. 2 GAUSS POINT AND END POINT LOCATIONS FOR  
A REINFORCED CONCRETE SECTION.



GAUSS POINT  
LOCATIONS

END POINT  
LOCATIONS

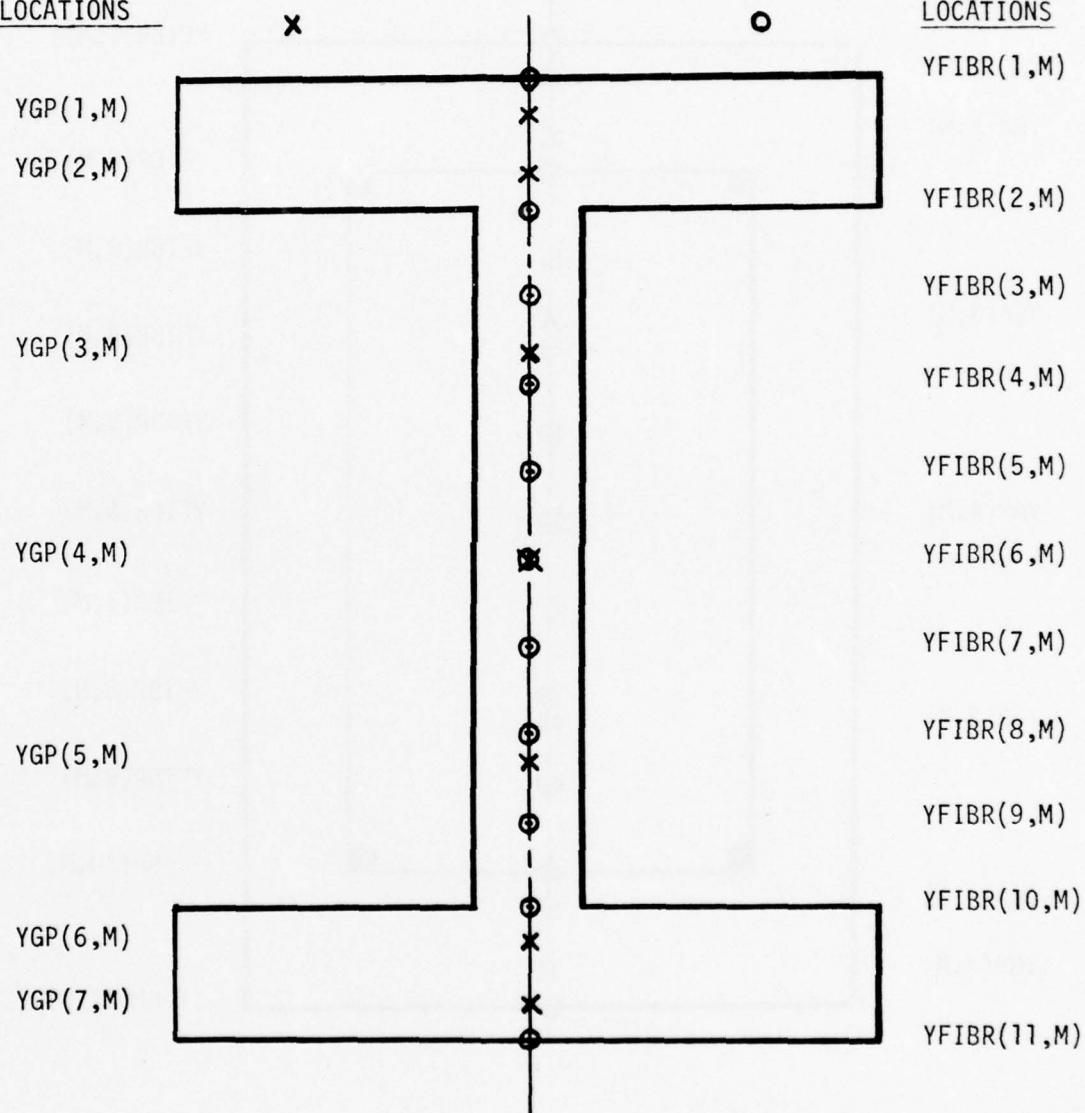


FIG. 3 GAUSS POINT AND END POINT LOCATIONS  
FOR A WIDE FLANGE SECTION.

defined by  $I = 1, 2$  and  $10, 11$  are the limits of the flange or cover thickness. The points defined by  $I = 3, 4, 5, 6, 7, 8$ , and  $9$  are determined by dividing the web or confined concrete depth by  $8$  and spacing the points evenly at the eighth points.

The  $y$  locations for the longitudinal reinforcing bar groups use the array name YBAR with the following form:

YBAR(I,M)	I = bar group number
	M = element number

The YBAR values are the  $y$  locations of each longitudinal reinforcing bar group input for an element. Figure 6a shows the points on a reinforcing bar with the length the same as the element length. This form is valid for each bar group, regardless of the input length, since each one is redefined as an equivalent group over the element length for energy computations.

The determination of whether or not a reinforced concrete element has a confined core is based on the value stored in the array NTIES(M), where  $M$  is the element number. NTIES stores the number of tie (stirrup) groups input for a reinforced concrete element. If  $NTIES = 0$ , no ties exist for the element and there is no confined core. The total section is then treated as unconfined for energy computations. If NTIES is a positive integer, then there are ties within the element and the energy is computed for both the confined core and the unconfined outer shell.

## ORGANIZATION OF DATA/KDATA STORAGE ARRAYS

Selected data values are stored in locations organized as two related arrays; one stores certain floating point data (DATA), while the other stores related integer data (KDATA). The DATA array includes the following values:

1. Curvature data
2. Reference forcing function data
3. Joint forcing function parameters
4. Plastic strain data
5. Stress history data

The KDATA array includes the following integer values:

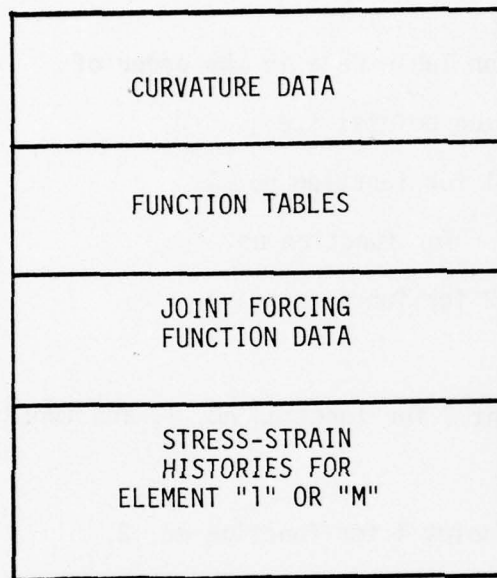
1. Reference forcing function time points
2. Joint forcing function parameters
3. Plastic strain data location indices
4. Stress history location indices

The following discussion provides the organizational details for these two arrays.

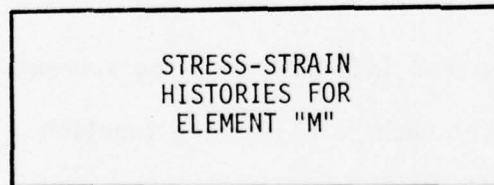
1. Organization of the DATA Array: The DATA array contains floating point data which are necessary for the solution process. It contains curvature data that are used in subroutine SEEK; it includes function tables and forcing function data; this array also contains element stress-strain histories if an element has yielded ( $MSTAT = 3$ ), or the user has input the option for storing the stress-strain histories ( $MSTAT = 3$ ) rather than using the changeable status ( $MSTAT = 2$ ). General storage in the DATA array is illustrated in figure 4.

STORAGE:

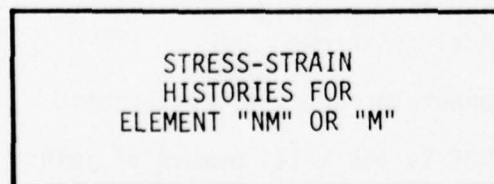
SUBSCRIPTS:



•  
•  
•



•  
•  
•



1

LTAB  
LTAB + 1

LFF  
LFF + 1

$LFF + 4 \cdot NFF = LP$   
 $KDATA(LPI + 1) = LP + 1$

$KDATA(LPI + M)$

$KDATA(LPI + NM)$

LMAX

FIG. 4 GENERAL STORAGE IN THE DATA ARRAY.



Allocation of space in the first portion of the DATA array for curvature data is made in subroutine FTAB. The total allocation is set by  $LTAB = NDF(NDF + 1)/2$  where NDF is the number of degrees of freedom of the system.

Subroutine FTAB stores the Function Table Data in the order of reference forcing functions by time-force points; i.e.,

$DATA(LTAB + 1) = \text{time point 1 for function no. 1}$

$DATA(LTAB + 2) = \text{force point 1 for function no. 1}$

$DATA(LTAB + 3) = \text{time point 2 for function no. 1}$

which is continued through

$DATA(LTAB + 2*J) = \text{force point J for function no. 1, and function table number 2 would begin with:}$

$DATA(LTAB + 2*N + 1) = \text{time point 1 for function no. 2.}$

This format continues for all function tables through the last value:

$DATA(LFF)$ , where  $LFF = LTAB + 2*J(1) + \dots + 2*J(NTAB)$ , where J is the number of time-force pairs for function table i and NTAB is the total number of function tables.

Joint forcing function data are stored into DATA array by subroutine JFOR. The following format is used for each joint forcing function:

$DATA(LFF + 1) = A = \text{scaling factor}$

$DATA(LFF + 2) = B = \text{load addition constant}$

$DATA(LFF + 3) = C = \text{time addition constant}$

$DATA(LFF + 4) = D = \text{time period for sinusoidal or cosinusoidal functions.}$

These four values are stored in this manner through the last point:

$DATA(LP)$ , where  $LP = LFF + 4*NFF$ , and NFF is the total number of joint forcing functions input by the Forcing Function Data Block.

Element stress-strain data are stored in the array only if an element has yielded or the user has forced storage during input by setting IACT to N on the element parameter card in the Element Data Block. In most problems, not all elements will have yielded before collapse takes place. For this reason, only the elements requiring storage of their stress-strain data need the storage allocation, and these data are stored in the DATA array as each element yields. (The entry points for the stress and strain data are stored in the KDATA array.) A simple five element example where elements have yielded in the order of 3, 2, and 5 is shown in Figure 5. Reinforced concrete stress-strain data are stored in the following general form for each member:

REINFORCING STEEL STRAINS:  $5 \times \text{NGRP}(\text{M})$  points

UNCONFINED CONCRETE STRAINS: 31 points

CONFINED CONCRETE STRAINS: 27 points

REINFORCING STRESS HISTORIES:  $40 \times \text{NGRP}(\text{M})$  points

UNCONFINED CONCRETE STRESS HISTORIES: 248 points

CONFINED CONCRETE STRESS HISTORIES: 216 points

Temporary storage is made from the DATA array in the S array in subroutines COEN, STEN, and OUTS. Strain and stress data are updated through the S array, which is contained in the common block FIBER, in subroutines CRET and REIN. The S array contains nine values which reference one point within the element. The values S(1) through S(8) correspond to the stress history at a particular point, and S(9) contains the strain at that point within the element. These values are directly transferred between the S and DATA arrays when MSTAT is set

## KDATA

SUBSCRIPT	STORAGE
LPI + 1	$LP_3 + 1$ $LP + 1$ $LP_2 + 1$
LPI + 2	
LPI + 3	
LPI + 4	
LPI + 5	
LPSI + 1	$LP_3 + 1 + R_2$ $LP + 1 + R_3$ $LP_2 + 1 + R_5$
LPSI + 2	
LPSI + 3	
LPSI + 4	
LPSI + 5	

## DATA

ELEMENT	STORAGE	SUBSCRIPT
3	$R_3$ $S_3$	$LP + 1$ $LP + 1 + R_3$
2	$R_2$ $S_2$	$LP_3 + 1$ $LP_s + 1 + R_2$
5	$R_5$ $S_5$	$LP_2 + 1$ $LP_2 + 1 + R_3$

$R_m$  = STRAIN DATA

$S_m$  = STRESS DATA

$LP_m$  = LAST POINT STORED

$m$  = ELEMENT "m"

NOTE: ELEMENTS HAVE YIELDED IN THE ORDER 3, 2, 5; ELEMENTS 1 & 4 HAVE NOT YIELDED.

FIG. 5 RELATION BETWEEN DATA AND KDATA;  
5-ELEMENT EXAMPLE.

to 3 for the element. If MSTAT is not set to 3 for the element, there is no transfer between these arrays at any of the points within the element.

Storage in the DATA array is made in the order of Gauss points (integration points) and force points (end points) for each of the six general groups of strain and stress listed above for each element. These point locations are defined in the preceding subsection, DESCRIPTIONS OF SELECTED VARIABLES.

Storage of the strain points of element M is made in the following way:

$LP = KDATA(LPI + M) - 1$  is the reference point as shown in Figures 4 and 5.

An example for two steel reinforcing bars is illustrated in Figure 6a. The storage for an element containing two bars is made as follows:

DATA (LP + 1)

LP + 2

LP + 3

LP + 4

LP + 5

LP + 6

where 1 through 6 refer to the Gauss points (x) in Figure 6a.

Storage continues with:

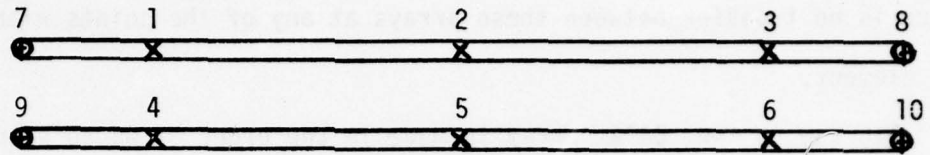
DATA (LP + 7)

LP + 8

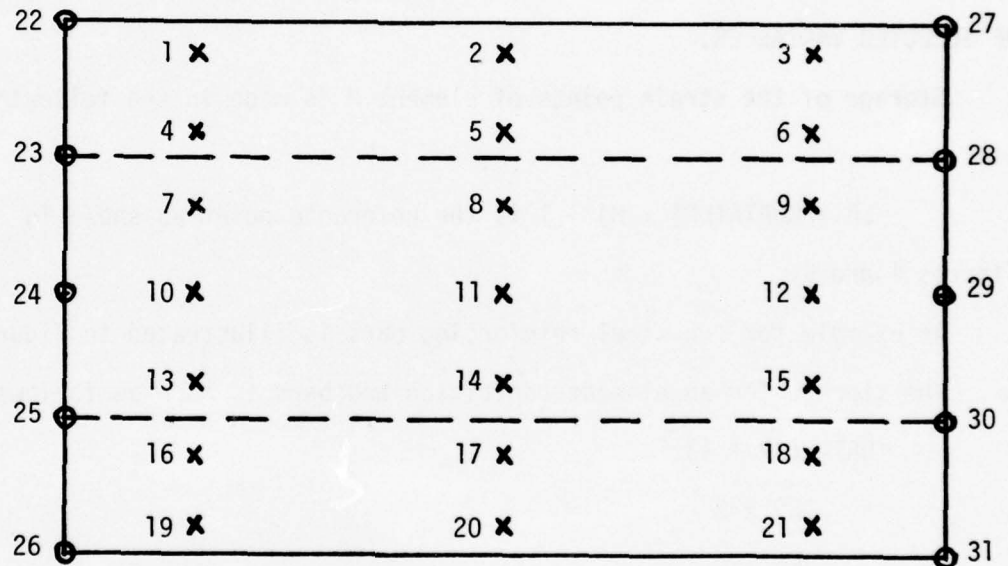
LP + 9

LP + 10

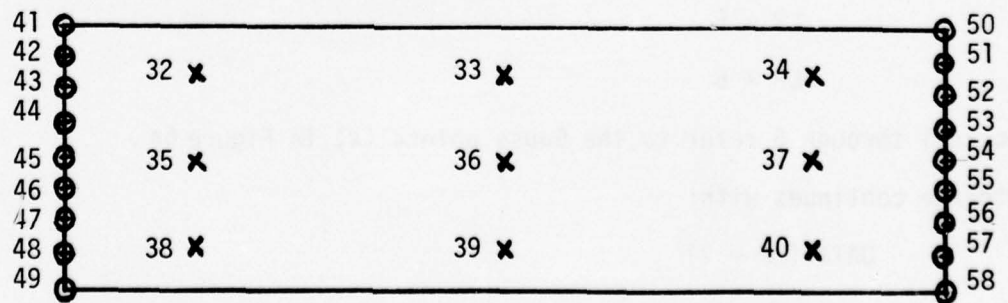




a. LONGITUDINAL STEEL BARS



b. UNCONFINED CONCRETE



c. CONFINED CONCRETE

FIG. 6 STRESS-STRAIN STORAGE FOR REINFORCED CONCRETE ELEMENTS.

where 7 through 10 refer to the force points (o) in Figure 6a.

The concrete strain points are referenced by  $KRAIN = KDATA(LPI + M) + 5 * NGRP(M) - 1$ , where  $NGRP(M)$  is the number of groups of reinforcing bars in element M. The subscripts for the unconfined and confined concrete in the DATA array continue from  $DATA(KRAIN + 1)$  to  $DATA(KRAIN + 58)$  as illustrated in Figures 6b and 6c.

The reinforcing steel stress histories are referenced by  $KRESS = KDATA(LPSI + M) - 1$  which is illustrated in Figure 5. Eight values are stored for each of the Gauss points and force points in Figure 6a. In this example with two bars, the subscripts would continue with  $KRESS + 2$  through  $KRESS + 48$  for the Gauss points (1-6) and  $KRESS + 49$  through  $KRESS + 60$  for the force points (7-10). For each reinforcing bar group there are 24 storage locations for Gauss points and 16 locations for end force points which totals 40 points for each group.

The concrete stress histories are referenced by  $KRESS = KRESS + 40 * NGRP(M)$ . Eight values are stored at each of the points shown in Figures 6b and 6c. Storage is made for the unconfined concrete at the Gauss points with subscripts  $KRESS + 1$  through  $KRESS + 168$  which are  $21 * 8$  values. The force points are stored with subscripts  $KRESS + 169$  through  $KRESS + 248$  which are  $5 * 8 + 5 * 8$  values. Stress histories at the Gauss points of the confined concrete begin with the subscript  $KRESS + 249$  and continue through  $KRESS + 320$  which are  $9 * 8$  values. The force point stress histories continue from  $KRESS + 321$  through  $KRESS + 464$  which are  $9 * 8 + 9 * 8$  values.

Following is a summary of the storage in the DATA array of a reinforced concrete element, M, where  $NG = NGRP(M)$ .

<u>Strains</u>	<u>Values Stored</u>	<u>Total</u>
Reinforcing steels:		
Gauss points	3*NG	3*NG
Force points	2*NG	5*NG
Unconfined concrete:		
Gauss points	21	5*NG + 21
Force points	10	5*NG + 31
Confined concrete:		
Gauss points	9	5*NG + 40
Force points	18	5*NG + 58

<u>Stress Histories</u>	<u>Values Stored</u>	<u>Total</u>
Reinforcing steels:		
Gauss points	24*NG	24*NG
Force points	16*NG	40*NG
Unconfined concrete:		
Gauss points	168	40*NG + 168
Force points	80	40*NG + 248
Confined concrete:		
Gauss points	72	40*NG + 320
Force points	144	40*NG + 464

Storage in the DATA array for a steel wide flange element is done in a similar way as that for a reinforced concrete element. The indexing for the strain data begins with  $KRAIN = KDATA(LPI + M) - 1$ . The Gauss point (x) subscripts range from  $KRAIN + 1$  through  $KRAIN + 21$  as shown in Figure 7. The subscripts for the force point strains range from  $KRAIN + 22$  through  $KRAIN + 43$ . The stress histories are referenced

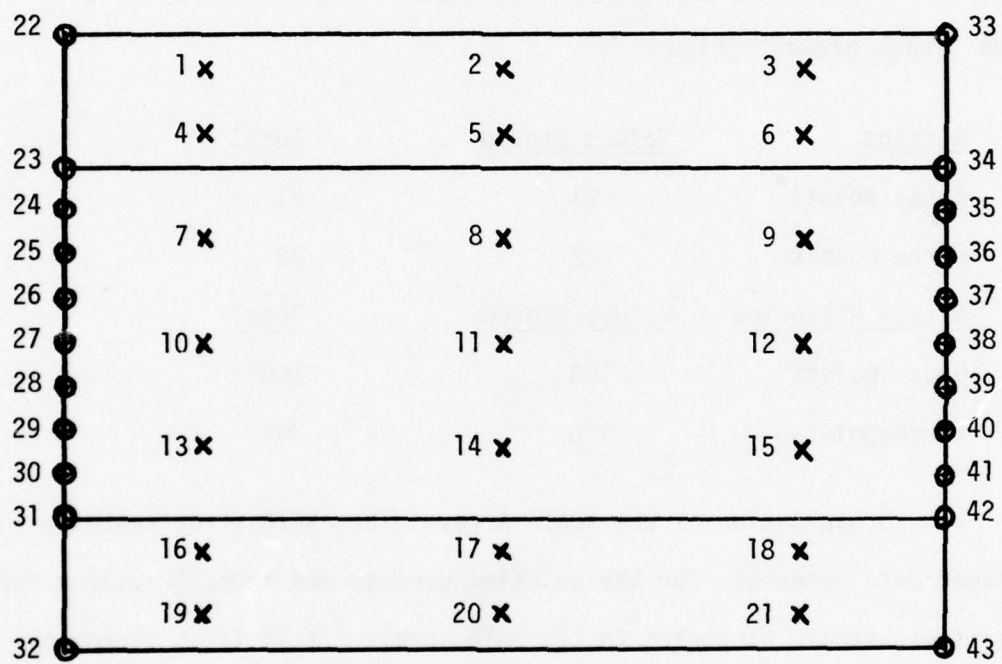


FIG. 7 STRESS-STRAIN STORAGE FOR WIDE FLANGE ELEMENTS.



by  $KRESS = KRAIN + 43$ . The subscripts for the Gauss point stress histories range from  $KRESS + 1$  through  $KRESS + 168$  which are  $21 \times 8$  values. The stress history subscripts for the force points range from  $KRESS + 169$  through  $KRESS + 344$  which are  $11 \times 8 + 11 \times 8$  values.

The following is a summary of storage in the DATA array of a wide flange element (Figure 7):

<u>Strains</u>	<u>Values Stored</u>	<u>Total</u>
Gauss points	21	21
Force points	22	43
<u>Stress Histories</u>	<u>Values Stored</u>	<u>Total</u>
Gauss points	168	168
Force points	176	344

2. Organization of the KDATA Array: The KDATA array contains integer data necessary for the solution process and index locations for the stress-strain histories in the DATA array. It is first stored by subroutine FTAB with function table data. The variable LTABI, which is the load table index, is the locator for each function table input into the program through the Function Table Data Block. This variable is initialized to zero in ABET. The function table data are stored in the following format:

$$KDATA(LTABI + 1) = LTABI + 1$$

$$KDATA(LTABI + 2) = \text{number of time points for each reference forcing function through the last forcing function table: } KDATA(LFFI),$$

where  $LFFI = LTABI + 2 \times NTAB$

and NTAB is the total number of reference forcing functions.

Forcing function data are stored in KDATA in subroutine JFOR through input in the Forcing Function Data Block. Storage is in the following format:

KDATA(LFFI + 1) = loaded joint number  
KDATA(LFFI + 2) = reference joint number  
KDATA(LFFI + 3) = direction  
KDATA(LFFI + 4) = reference function number  
KDATA(LFFI + 5) = last forward time point used for  
each joint forcing function through  
the last input forcing function:  
KDATA(LPI),

where  $LPI = LFFI + 5 \cdot NFF$  and  $NFF$  is the total number of joint forcing functions used.

The index or subscript values that define the locations of the element stress-strain histories in the DATA array are set in subroutine STOR. The following format is used:

KDATA(LPI + 1) = start of strain data for element 1  
KDATA(LPI + 2) = start of strain data for element 2, and  
for each element, where KDATA(LPSI) is the  
starting point for the strain data of element  
NM and  $LPSI = LPI + NM$ .  
KDATA(LPSI + 1) = start of stress history data for element 1  
KDATA(LMAXI) = start of stress history data for element NM

where  $LMAXI = LPSI + NM = LPI + 2 \cdot NM$ .

#### MODIFICATION OF FIXED STORAGE ALLOCATION

When a problem is sufficiently large or computer storage is critical, various arrays within SINGER must be modified to accommodate these restrictions. The key to successful storage modification is an understanding of the several key variables which describe in general the

problem size in question. These variables are defined as follows:

<u>Variable</u>	<u>Definition</u>	<u>Current Value</u>
NDFD	Maximum number of degrees of freedom	90
NJD	Maximum number of joints	50
NLD	Maximum number of leaf springs	20
NMATD	Maximum number of materials	9
NMAX	Maximum index of DATA array	10000
NMAXI	Maximum index of KDATA array	500
NMD	Maximum number of members	45

Every change of storage within SINGER can be accomplished by changing those arrays which depend on these seven variables. Other program variations are possible, but a complete reprogramming would be necessary. These include having greater than 10 groups of reinforcing steel in one member, varying the Gaussian quadrature system in the program, and varying the number of elemental distortion components (varying the number of internal nodes).

Table 1 gives a list of the common storage data arrays and the variable arrays that must be changed. Table 2 gives other variables that must be dimensioned differently. Table 3 shows where the different common blocks are found within the subroutines. Table 4 gives example sizes for linear and nonlinear problems of the KDATA and DATA arrays.

Given a fixed storage requirement, the largest problem that can be solved by SINGER would consist of one where the material response is strictly linear in nature. All arrays, even though they are not used by a particular problem, should have a minimum value of 1.

TABLE 1 - COMMON VARIABLE ARRAYS

LOCATION	VARIABLE ARRAY	CURRENT VALUE	NECESSARY VALUE
COMMON	DATA	10000	NMAX
	KDATA	500	NMAXI
COMMON/CONBK	COAREA	4,45	4,NMD
	SIGMA	5,45	5,NMD
COMMON/ELEMENT	IP	45	NMD
	IPL	45	NLD
	IQ	45	NMD
	IQL	45	NLD
	MATR	45	NMD
	MATW	45	NMD
	MBAR	10,45	10,NMD
	MCODE	45	NMD
	MSHEAR	45	NMD
	MSTAT	45	NMD
	MTIES	45	NMD
	MTYPE	45	NMD
	NGRP	45	NMD
	NSPACE	6,45	NMD
	NTIES	45	NMD
COMMON/FIBER	DENS	9	NMATD
	EC	9	NMATD
	EPSU	9	NMATD
	ET	9	NMATD
	FCFY	9	NMATD



	G	9	NMATD
	PR	9	NMATD
	SLOPG	8,9	8,NMATD
	STN	8,9	8,NMATD
	STS	8,9	8,NMATD
	UNLK	9	NMATD
	ICODE	9	NMATD
	NAME	9	NMATD
COMMON/JOINTS	ACC	3,50	3,NJD
	BET	3,50	3,NJD
	DAS	3,50	3,NJD
	DIS	3,50	3,NJD
	ERJF	3,50	3,NJD
	ERJH	3,50	3,NJD
	ERJZ	3,50	3,NJD
	F	3,50	3,NJD
	FOR	3,50	3,NJD
	VEL	3,50	3,NJD
	X	50	NJD
	XDJ	3,50	3,NJD
	Y	50	NJD
	DER	3,50	3,NJD
	RESENG	3,50	3,NJD
	IDFI	90	NDFD
	IDFII	90	NDFD
COMMON/MEMBER	AGRP	10,45	10,NMD
	ATIES	6,45	6,NMD

BMEM	45	NMD
BPP	45	NMD
BDM	10,45	10,NMD
BWF	45	NMD
D	45	NMD
DP	45	NMD
DPP	45	NMD
DWF	45	NMD
EFFL	10,45	10,NMD
EFLM	45	NMD
HMEM	45	NMD
HTOP	45	NMD
HTWF	45	NMD
PDP	7,45	7,NMD
SPRING	5,20	5,NLD
STIES	7,45	7,NMD
TFWF	45	NMD
TWWF	45	NMD
UDM	45	NMD
URM	45	NMD
XBEG	10,45	10,NMD
XBEGM	45	NMD
XBEGS	6,45	6,NMD
XL	45	NMD
XPI	5,45	5,NMD
YBAR	10,45	10,NMD
YGP	7,45	7,NMD

	YFIBR	11,45	11,NMD
	YLDS	45	NMD
	XDM	45	NMD
	PDF	7,45	7,NMD
	DISM	45	NMD
COMMON/SAVEBK	SAVACC	3,50	3,NJD
	SAVAXL	2,45	2,NMD
	SAVCRV	2,45	2,NMD
	SAVMOM	2,45	2,NMD
	SAVSHR	2,45	2,NMD
	SAVSRP	3,20	3,NLD
	SAVSRQ	3,20	3,NLD
	SAVXDJ	3,50	3,NJD
	SAVEL	3,50	3,NJD
	SVSTRN	12,45	12,NMD
	SVSTRS	12,45	12,NMD
COMMON/SEEKBK	DEFOR	90	NDFD
	STPSIZ	90	NDFD
	GRAD	90	NDFD
	GRADI	90	NDFD
	DELTAG	90	NDFD
	DIRECT	90	NDFD
	DIAG	90	NDFD

TABLE 2 - OTHER VARIABLES

<u>SUBROUTINE</u>	<u>VARIABLE (CURRENT SIZE)</u>	<u>NECESSARY VALUE</u>
ABET	SOLN(90)	NDFD
	NDFD=90	NDFD
	NJD=50	NJD
	NLD=20	NLD
	NMATD=9	NMATD
	NMAX=10000	NMAX
	NMAXI=500	NMAXI
	NMD=45	NMD
ADYN	SOLN(90)	NDFD
ASAN	SOLN(90)	NDFD
CUTS	KIND(45)	NMD
DELT	SOLN(90)	NDFD
ELIN	KIND(45)	NMD
ERRS	SOLN(90)	NDFD
JFOR	IERROR(50,5)	NJD,5
MATD	IERROR(9,16)	NMATD,16
POTE	SOLN(90)	NDFD
REJO	IRESTR(3,50)	3,NJD
	IERROR(5,50)	5,NJD
	JNUM(50)	NJD
SEEK	DEFORM(90)	NDFD
	CURV(4095)	$\frac{NDFD*(NDFD+1)}{2}$



TABLE 3 - SUBROUTINES AND COMMON BLOCKS

SUBROUTINE	COMMON BLOCKS TO CHANGE							
	COMMON	COMMON/CONBK	COMMON/ELEMENT	COMMON/FIBER	COMMON/JOINTS	COMMON/MEMBER	COMMON/SAVEBK	COMMON/SEEKBK
ABET	X		X	X	X	X	X	X
ACIN	X		X	X	X	X		
ADYN	X		X	X	X	X	X	X
ASAN	X				X	X		X
BEAM			X	X		X		
BODY			X	X	X	X		
BOND			X	X		X		
COEN	X	X	X	X	X	X		
CONC		X	X	X		X		
CRET				X				
CUTS			X		X	X		
DEFO			X		X			
DELT			X		X	X		
ELIN			X	X		X		
ENDS						X		
ENGY			X					
ERRS					X	X		X
FAIL	X		X	X		X	X	
FORK			X			X		

SUBROUTINE	COMMON	COMMON/CONBK	COMMON/ELEMENT	COMMON/FIBER	COMMON/JOINTS	COMMON/MEMBER	COMMON/SAVEBK	COMMON/SEEK BK	
FORS	X				X				
FTAB	X								
GIDE					X			X	
INIT					X				
JFOR	X								
LEAF			X			X			
LINK			X	X	X	X			
LUMP					X				
MASS			X		X				
MATP				X					
MATY				X					
MEMB			X			X			
OUTS	X		X	X	X	X	X	X	
PLOG			X			X	X		
POTE					X	X		X	
REGO	X		X	X	X	X		X	
REIN				X					
REJO					X				
SECT			X				X		
SEEK	X		X					X	
STEN	X		X	X		X			
STOR	X		X						

SUBROUTINE	COMMON	COMMON/CONBK	COMMON/ELEMENT	COMMON/FIBER	COMMON/JOINTS	COMMON/MEMBER	COMMON/SAVEBK	COMMON/SEEKBK	
STRN						X			
SUMY			X	X	X	X			
TABL	X								
TEST			X	X		X			
WIDE	X		X	X		X			
BLOCK DATA				X			X		
TOTAL CHANGES	16	2	29	22	21	28	7	9	

TABLE 4 - SIZE OF KDATA AND DATA ARRAYS

LINEAR	PROBLEM	
<u>ARRAY</u>	<u>NECESSARY SIZE</u>	<u>CURRENT VALUE</u>
KDATA	$LPI = (2*NTAB) + (5*NFF) + (2*NM)$	500
DATA	$LP = (NDF*(NDF+1)/2) + \sum_{i=1}^{NTAB} 2*J(i) + 4*NFF$	10000
	NDF = Number of degrees of freedom NFF = Number of joint forcing functions NM = Number of members NTAB = Number of forcing function tables J(i) = Number of time-force pairs	
NONLINEAR	PROBLEM	
<u>ARRAY</u>	<u>NECESSARY SIZE</u>	<u>CURRENT VALUE</u>
KDATA	LPI	500
DATA	$LP + NMC*[40*NG + 464] + NMWF*344$	10000
	NG = Number of groups of reinforcing steel in member NMC = Number of R/C members NMWF = Number of WF members	

TYPICAL PROBLEMS

Problem A

10 members  
 40 degrees of freedom maximum  
 2 forcing functions  
 6 time-force pairs for each function  
 8 joints loaded  
 All R/C members with three groups of reinforcing steel

Problem B

50 members  
 200 degrees of freedom  
 10 forcing functions  
 6 time-force pairs for each  
 20 joints loaded  
 All R/C members with three groups of reinforcing steel

	KDATA SIZE	DATA SIZE
<u>Linear Problem</u>		
Problem A	64	876
Problem B	220	20300
<u>Nonlinear Problem</u>		
Problem A	64	6716
Problem B	220	49500

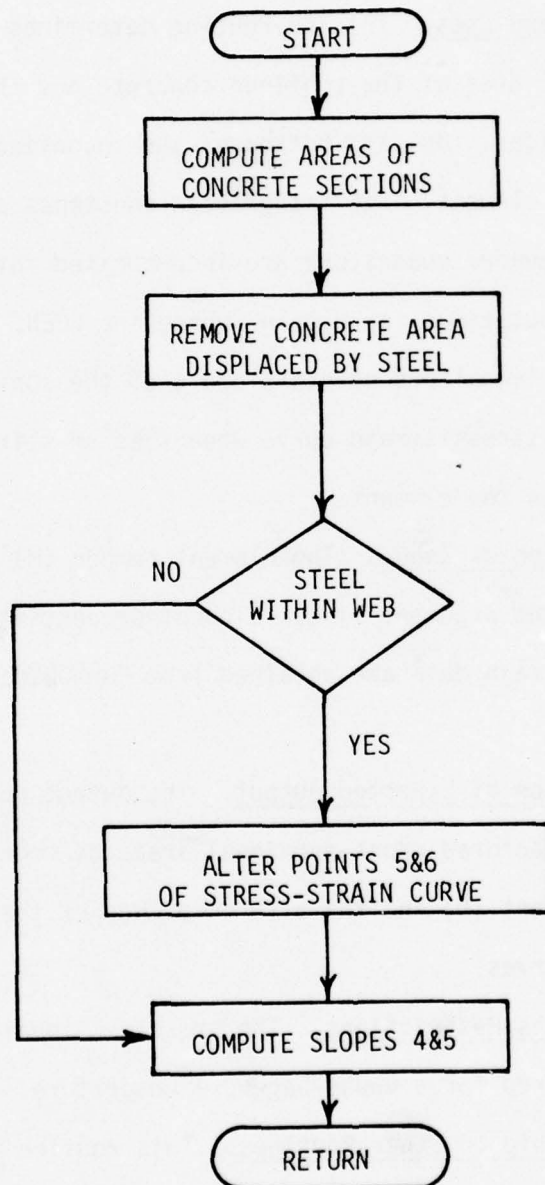


## SECTION IV

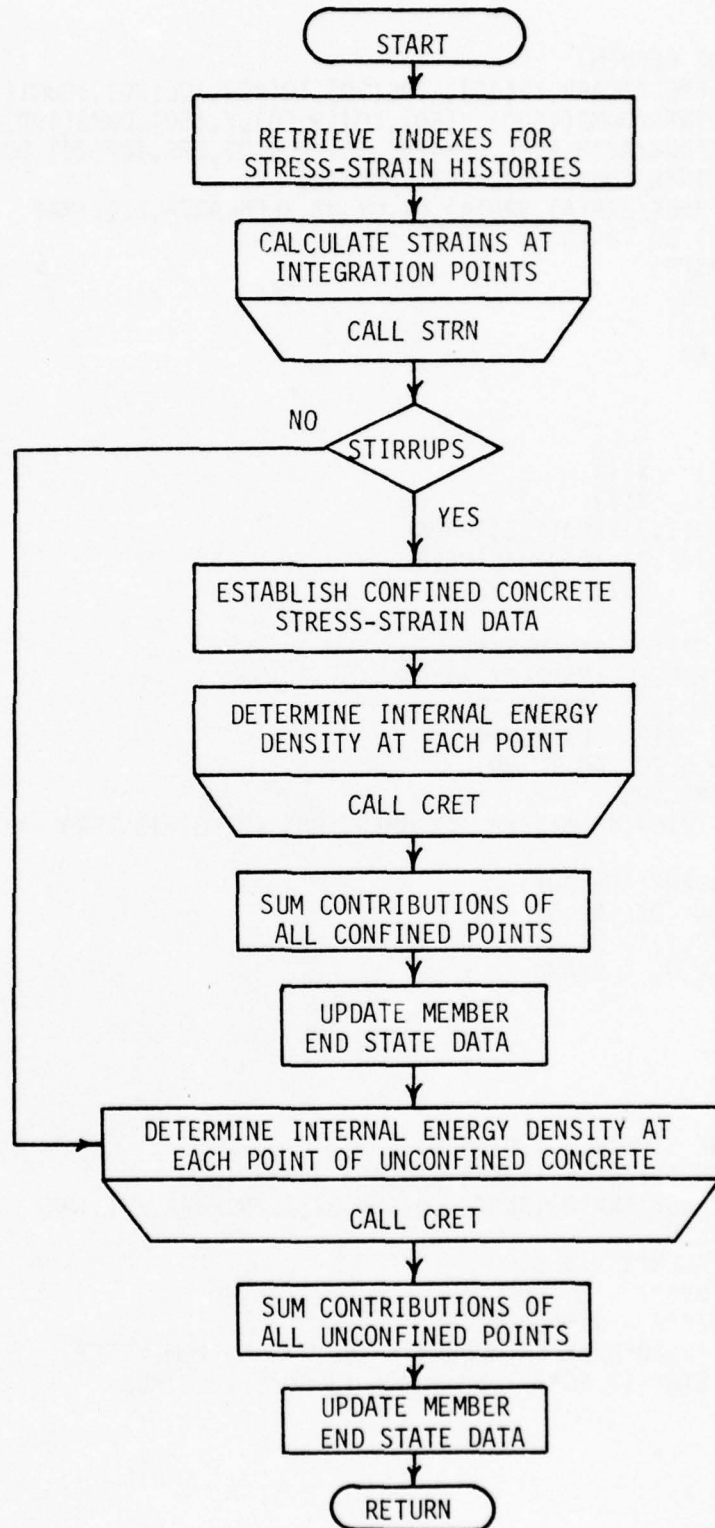
### NEW SUBROUTINE DOCUMENTATION

Three new subroutines were developed and one was significantly altered for efficiency and improved accuracy. Subroutine COEN was modified by removing a segment of computations which could be more efficiently done in a separate subroutine during the input sequence. The new subroutine, CONC, is described in this section as well as the revised organization of COEN. The description of subroutine COEN is available in the Program Document of a previous contract report [4]. In addition, two new subroutines were written to replace DEFO and STRN as required by the details of the new finite element model (for development details, see section V, Volume I, of this report). The description details for these two subroutines are basically the same as the original documentation [4]; only the computational details have been changed. The source listings for both DEFO and STRN are included in this section since they are currently introduced into the program at the option of the user, and they are not included in the complete program listing in the Appendix of this volume.

1. Name of Subroutine - CONC(M)
2. Description of Subroutine
  - a. Purpose and Uses. This subroutine determines the cross-sectional area of the confined concrete and the areas of the sides, top, and bottom of the unconfined concrete for each element. The integration constants of the Gauss-Legendre quadrature are incorporated into these area computations for use in subroutine COEN. This routine also alters points 5 and 6 of the confined concrete stress-strain curve when ties or stirrups are within the element.
  - b. Description of Input. The element number (M) is input through the argument list. Element properties and stress-strain data are obtained from COMMON data storage.
  - c. Description of Expected Output. The output quantities are the factored cross-sectional areas of concrete for each element (M) and the altered points of the stress-strain curves.
  - d. Limitations/Restrictions. The cross-sectional areas are factored for a Gauss-Legendre quadrature.
  - e. Relationship to Other Routines. This routine is called by subroutine ACIN.



SUBROUTINE COEN





```

SUBROUTINE DEFO(M)
COMMON/ELEMET/ICARD,IP(45), IPL(20),IQ(45),IQL(20),IDUM1(1125)
COMMON/JOINTS/DUM2(1500),X(50),XDJ(3,50),Y,(50),DUM3(480)
COMMON/LEADBK/AVDM,AVGL,DUM4(5),ID1(20),DT,EPS,ID2(20),DUM5(11)
COMMON/MAINBK/IDUM2(42),NPRT,IDUM3(6)
COMMON/STRNBK/SRP(4),SRQ(4),UX,UY,UZ,XLEN,AREA,ZZI,IMAT
IF(M.GT.0) GO TO 10
ILS = IABS(M)
I = IPL(ILS)
J = IQL(ILS)
XLEN = 1.E0
GO TO 20
10 I = IP(M)
J = IQ(M)
20 DX1 = X(J) - X(I)
DX2 = Y(J) - Y(I)
DU1 = (XDJ(1,J)-XDJ(1,I))*AVGL
DU2 = (XDJ(2,J)-XDJ(2,I))*AVGL
DX1P = DX1 + DU1
DX2P = DX2 + DU2
DXLEN = SORT(DX1**2+DX2**2)
DXLENP = SORT(DX1P**2+DX2P**2)
ADX = DX1*DX2P - DX2*DX1P
BDX = DX1*DX1P + DX2*DX2P
IF(BDX.NE.0.E0) GO TO 30
WRITE (NPRT,40)
40 FORMAT (///10X,43H***** ARGUMENT BDX (DEFO) IS ZERO *****//)
RETURN
30 RBANG = ATAN2(ADX,BDX)
UX = 0.5E0*(DXLENP-DXLEN)
UY = XDJ(3,I) - RBANG
UZ = XDJ(3,J) - RBANG
RETURN
END

```

```

SUBROUTINE STRN(M,X,Y,STRAIN)
COMMON/MEMBER/DUMMY1(5365),XDM(45),DUMMY2(360)
COMMON/STRNBK/SRP(4),SRQ(4),UX,UY,UZ,XLEN,AREA,ZZI,IMAT
ETA = Y/XLEN
T = 2.E0/XLEN*X - 1.E0
ALPHA = (UY**2 - 0.5E0*UY*UZ + UZ**2)/15.E0
BETA = (UZ**2 - UY**2)/16.E0
STRAIN = (2.E0*UX/XLEN+ALPHA) + (BETA-4.E0*XDM(M))*T
1 - ETA*((3.E0*T-1.E0)*UY + (3.E0*T+1.E0)*UZ)
RETURN
END

```

#### REFERENCES

1. Melosh, R. J., et al., SINGER: A Computer Code for General Analysis of Two-Dimensional Concrete Structures, AFWL-TR-74-228, Vol. III, Air Force Weapons Laboratory, Kirtland Air Force Base, NM, May 1975.
2. Holzer, S. M., et al., SINGER: A Computer Code for General Analysis of Two-Dimensional Concrete Structures, AFWL-TR-74-228, Vol. I, Air Force Weapons Laboratory, Kirtland Air Force Base, NM, May 1975.
3. Bradshaw, J. C., Nonlinear Analysis of Plane Frames, Master Thesis, Virginia Polytechnic Institute and State University, May 1975.
4. Barker, R. M., et al., SINGER: A Computer Code for General Analysis of Two-Dimensional Concrete Structures, AFWL-TR-74-228, Vol. II, Air Force Weapons Laboratory, Kirtland Air Force Base, NM, May 1975.

APPENDIX  
PROGRAM SOURCE LISTING

The complete listing of the SINGER code is included in this section with the exception of the two new subroutines DEFO and STRN developed to implement the logic of the new finite element model (section V, Volume I). The listing for these two subroutines is included in section IV of this volume.

```

CABET 0 10
C
C      AFWL VERSION OF *SINGER*, A COMPUTER CODE FOR SIMULATING
C      INELASTIC AND NONLINEAR GEOMETRIC EFFECTS ON REINFORCED CONCRETE
C      BEAM-COLUMN ELEMENTS.
C
C      THIS VERSION IS UPDATED AS OF 6 MAY 1976.
C      ORIGINAL VERSION BEGAN BY V. P. I. AND S. U., BLACKSBURG, VA.
C
C      MAIN EXECUTIVE ROUTINE
C
COMMON DATA(10000),KDATA(500)
COMMON/ELEMENT/ICAPD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),
1 SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),DIS(3,50),ERJF(3,50),
1 ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
1 XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),OT,EPS,HEAD(20),
1 PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLT,IPRINT,
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCH,
2 NCRD,NDF,NDFD,NDFJ,NDIS,NOL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,
4 NTIMES,NVEL,IINITO
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BDM(10,45),
1 BWF(45),D(45),OPP(45),DMF(45),EFFL(10,45),EFLM(45),
2 HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),
ABET 0
ABET 10
ABET 20
ABET 30
ABET 40
ABET 50
ABET 60
ABET 70
ABET 80
ABET 90
ABET 100
ABET 110
ABET 120
ABET 130
ABET 140
ABET 150
ABET 160
ABET 170
ABET 180
ABET 190
ABET 200
ABET 210
ABET 220
ABET 230
ABET 240
ABET 250
ABET 260
ABET 270
ABET 280

```



```

3   TFWF(45), TWF(45), UDM(45), URM(45), XBEG(10,45),
4   XBEGM(45), XBEGS(6,45), XL(45), XPI(5,45), YBAR(10,45), YGP(7,45),
5   YFIBR(11,45), YLDS(45), XDM(45), PDF(7,45), DISM(45)
COMMON /PLOTBK/ ITER
COMMON/SAVEBK/SAVACC(3,50), SAVAXL(2,45), SAVCRV(2,45), SAVMOM(2,45)
1   , SAVSHR(2,45), SAVSRP(3,20), SAVSRQ(3,20), SAVXDJ(3,50),
2   SAVVEL(3,50), SVSTRN(12,45), SVSTRS(12,45)
COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB,
1   LTABI,NMAX,NMAXI
COMMON/SEEK8K/DEFOR(90), STPSIZ(90), GRAD(90), GRADI(90), DELTAG(90),
1   DIRECT(90), DIAG(90), STEP(4), DSTEP(4), FVAL(4), VALUES(7),
2   DISACC,SSIZE,FUNACC,FUNMIN,CRITL,CRITU,NLIN
COMMON/STRN9K/SRP(4), SRG(4), UX,UY,UZ,XLEN,AREA,ZZI,IMAT
COMMON /TIMEBK/ TCUM,INIT,KNT

INTEGER HEAD,DHEAD
DIMENSION SOLN(90)

CORE ALLOCATION PARAMETERS

NDFD=90
NJD=50
NLD=20
NMTD=9
NMAX=10000
NMAXI=500
NMD=45
PERIPHERAL UNIT PARAMETERS
NCRD=5
NPLOT=10

```

```

ABET 290
ABET 300
ABET 310
ABET 320
ABET 330
ABET 340
ABET 350
ABET 360
ABET 370
ABET 380
ABET 390
ABET 400
ABET 410
ABET 420
ABET 430
ABET 440
ABET 450
ABET 460
ABET 470
ABET 480
ABET 490
ABET 500
ABET 510
ABET 520
ABET 530
ABET 540
ABET 550
ABET 560
ABET 570
ABET 580

```

C

C

C

C

C	NPRT=6	ABET 590
C	NSAVE=11	ABET 600
C	NTAPE=11	ABET 610
		ABET 620
	PRECISION CONTROL PARAMETERS	ABET 630
		ABET 640
	CRITL=1.E-9	ABET 650
	CRITU=1.E-3	ABET 660
	EPS=1.E-14	ABET 670
	FUNACC=1.E-13	ABET 680
	FUNMIN=-1.E0	ABET 690
	SSIZE=1.E-5	ABET 700
	TINY=1.E-36	ABET 710
		ABET 720
C	OTHER CONFIGURATION PARAMETERS	ABET 730
C		ABET 740
C	NL=66	ABET 750
		ABET 760
C	INITIALIZE ERROR COUNTERS AND PAGE NUMBER	ABET 770
C		ABET 780
C	IERR=0	ABET 790
3	IFAIL=0	ABET 800
	IPAGE=0	ABET 810
	IREC=0	ABET 820
	IYLD = 0	ABET 830
	LERR=0	ABET 840
C		ABET 850
C	INITIALIZE INDEXES FOR STORAGE IN DATA ARRAY	ABET 860
C		ABET 870
	LCURV=0	ABET 880



```

C C INITIALIZE MEMBER ENERGY.
C
8      DO 10 I=1,NM
      URM(I)=0.E0
      UDM(I)=0.E0
10
C C PERFORM STATIC ANALYSIS.
C
      NLIN=10*NDF
      IF (IANAL.EQ.1) GO TO 30
      CALL ASAN(SOLN)
      IF(IERR.EQ.0.AND.LERR.EQ.0.AND.IFAIL.EQ.0) GO TO 19
      PRINT 12
12     FORMAT(1H,69H*** ERRORS IN STATIC ANALYSIS. THIS PROBLEM IS TERMINATED. (ABET) ***)
      GO TO 50
19     WRITE(NPRT,20)
20     FORMAT (//1H,44HNORMAL COMPLETION OF STATIC ANALYSIS (ABET)./1H)
      GO TO 3
C C PERFORM DYNAMIC ANALYSIS.
C
30     CALL ADYN(SOLN)
      IF(IERR.EQ.0.AND.LERR.EQ.0.AND.IFAIL.EQ.0) GO TO 39
      PRINT 23
23     FORMAT(1H,70H*** ERRORS IN DYNAMIC ANALYSIS. THIS PROBLEM IS TERMINATED. (ABET) ***)
      GO TO 50
39     WRITE(NPRT,40)

```

```

ABET1190
ABET1200
ABET1210
ABET1220
ABET1230
ABET1240
ABET1250
ABET1260
ABET1270
ABET1280
ABET1290
ABET1300
ABET1310
ABET1320
ABET1330
ABET1340
ABET1350
ABET1360
ABET1370
ABET1380
ABET1390
ABET1400
ABET1410
ABET1420
ABET1430
ABET1440
ABET1450
ABET1460
ABET1470
ABET1480

```



```

40  FORMAT(//1H ,45HNORMAL COMPLETION OF DYNAMIC ANALYSIS (ABET)./1H1)ABET1490
GO TO 3      ABET1500
STOP        ABET1510
C          ABET1520
C          ABET1530
C          ABET1540
C          ABET1550
C          ABET1550
C          ABET1550
C          ABET1570
C          ABET1530
C          ABET1530
C          ABET1590
C          ABET1600
C          ABET1610
C          ABET1620
C          ABET1630
C          ABET1640
C          ABET1650
C          ABET1660
C          ABET1670
C          ABET1680
C          ABET1690
C          ABET1700
C          ABET1710
C          ABET1720
C          ABET1730
C          ABET1740
C          ABET1750
C          ABET1760
C          ABET1770
C          ABET1780

C ***** GLOSSARY FOR ABET *****

C ACC      = ACCELERATION COMPONENTS, BY DEGREE OF FREEDOM.
C AGRP     = AREA OF STEEL IN LONGITUDINAL REINFORCEMENT GROUP.
C ATIES    = EFFECTIVE AREA OF STEEL IN A TIE OR STIRRUP.
C AVDM     = AVERAGE DIMENSIONALIZING PARAMETER = AVGL * AVGA * AVGE.
C AVGL     = AVERAGE ELEMENT LENGTH.
C BET      = JERK COMPONENTS, BY DEGREE OF FREEDOM.
C BETA     = SHEAR COEFFICIENT, BY ELEMENT.
C BPEM     = ELEMENT GROSS WIDTH, BY ELEMENT.
C BPP      = CONFINED CONCRETE WIDTH, BY ELEMENT.
C BWF      = FLANGE WIDTH OF WIDE FLANGE BEAM, BY ELEMENT.
C CA       = MACRO SHEAR FAILURE CONSTANT, SURFACE INTERCEPT.
C CB       = MACRO SHEAR FAILURE CONSTANT, CURVE SLOPE.
C CC       = MACRO SHEAR FAILURE CONSTANT, UPPER BOUND.
C CD       = MACRO SHEAR FAILURE CONSTANT, UPPER BOUND AXIAL.
C D        = DISTANCE- CONCRETE TOP TO LOWER STEEL, BY ELEMENT.
C DAS      = MASS COMPONENTS, BY DEGREE OF FREEDOM.
C DATA    = IN-CORE STORAGE FILE.
C DENS     = DENSITY (SPECIFIC WEIGHT) OF MATERIAL.
C DHEAD    = INPUT BLOCK HEADING IMAGE.
C DIS      = DISPLACEMENT COMPONENTS, BY DEGREE OF FREEDOM.
C DP       = DISTANCE- CONCRETE TOP TO UPPER STEEL, BY ELEMENT.
C DPP      = CONFINED CONCRETE HEIGHT OF ELEMENT, BY ELEMENT.
C DT       = INITIAL TIME INTERVAL FOR TRANSIENT INTEGRATION.
C DMF      = WIDE FLANGE BEAM DEPTH, BY ELEMENT.

```

C EC	= YOUNG+S MODULUS IN COMPRESSION.	ABET1790
C EFFL	= EFFECTIVE LENGTH OF LONGITUDINAL REBAR GROUP.	ABET1800
C EFLM	= EFFECTIVE LENGTH OF ELEMENT, BY ELEMENT.	ABET1810
C EGSIF	= FORCE CONVERSION FACTOR FROM ENGLISH TO SI UNITS.	ABET1820
C EGSIL	= LENGTH CONVERSION FACTOR FROM ENGLISH TO SI UNITS.	ABET1830
C EGSIS	= STRESS CONVERSION FACTOR FROM ENGLISH TO SI UNITS.	ABET1840
C ELEMET	= COMMON BLOCK OF ELEMENT INTEGER DATA.	ABET1850
C EPS	= SMALLEST RELATIVE NUMBER IN THE MANTISSA	ABET1860
C EPSL	= STRAIN ASSOCIATED WITH MAXIMUM CONCRETE STRESS.	ABET1870
C ERJF	= JOINT FULL-TIME ERROR, BY DEGREE OF FREEDOM.	ABET1880
C ERJH	= JOINT HALF-TIME ERROR, BY DEGREE OF FREEDOM.	ABET1890
C ERJ7	= JOINT ZERO-TIME ERROR, BY DEGREE OF FREEDOM.	ABET1900
C ET	= YOUNG+S MODULUS IN TENSION.	ABET1910
C F	= CURRENT VALUE OF THE JOINT FORCING FUNCTION, BY D.O.F.	ABET1920
C FCFY	= CRUSHING STRENGTH OF CONCRETE OR YIELD STRENGTH OF STEEL.	ABET1930
C FIBER	= COMMON BLOCK OF STRESS-STRAIN CURVE DATA.	ABET1940
C FOR	= INITIAL JOINT FORCES, BY DEGREE OF FREEDOM.	ABET1950
C G	= SHEAR MODULUS, BY MATERIAL.	ABET1960
C HEAD	= PROBLEM PAGE HEADING IMAGE.	ABET1970
C HTOP	= DISTANCE- TOP OF CONCRETE TO REFERENCE AXIS, BY ELEMENT.	ABET1980
C HTWF	= DISTANCE- TOP OF WIDE FLANGE TO REFERENCE AXIS.	ABET1990
C HMEM	= GROSS HEIGHT OF ELEMENT, BY ELEMENT.	ABET2000
C IANAL	= ANALYSIS TYPE FLAG. (0=STATIC,1=DYNAMIC)	ABET2010
C ICARD	= SEQUENCE NUMBER OF ELEMENT DATA CARDS.	ABET2020
C ICODE	= MATERIAL TYPE CODE. (0=UNCONF.CONC.,1=CONF.CONC.,2=STEEL)	ABET2030
C ICURV	= CURVATURE MATRIX FLAG. (0=NO CHANGE, 1=USE IDENTITY )	ABET2040
C IDFI	= JOINT NUMBER OF DEGREE OF FREEDOM.	ABET2050
C IDFII	= DIRECTION NUMBER OF DEGREE OF FREEDOM.	ABET2060
C IINITD	= INDEX FOR INITIAL GUESS OF DISPLACEMENTS. (.LT.1=READ)	ABET2070
C ILIN	= ANALYSIS COMPLEXITY FLAG. (0=LINEAR SYSTEM,,NE.0, NON-LIN)	ABET2080

C IFOR	= INITIAL JOINT FORCE FLAG. (0=NONE,.NE.0 GIVEN )	ABET2090
C IERR	= NUMBER OF INPUT ERRORS.	ABET2100
C IPAGE	= CURRENT NUMBER OF PAGE BEING OUTPUT.	ABET2110
C IP	= FIRST JOINT NUMBER, PER NON-LEAF SPRING ELEMENT	ABET2120
C IPL	= FIRST JOINT NUMBER, PER LEAF SPRING COMPONENT.	ABET2130
C IPLOT	= DATA RETRIEVAL FILE FLAG. (0=DO NOT WRITE RETRIEVAL FILE)	ABET2140
C IPRINT	= PRINT LEVEL FLAG. (0=MINIMUM, 1=STANDARD, 2=DETAILED)	ABET2150
C IQ	= SECOND JOINT NUMBER, PER NON-LEAF SPRING ELEMENT.	ABET2160
C IQL	= SECOND JOINT NUMBER, PER LEAF SPRING COMPONENT.	ABET2170
C IREC	= NUMBER OF RECOVERABLE ERRORS.	ABET2180
C ISTART	= SOURCE OF INPUT DATA. (0=CARD FILE, .NE. 0=OTHER FILE)	ABET2190
C ISTOP	= ERROR OVERRIDE FLAG. (0=STOP, .NE. 0 GO IF COND. ERRORS)	ABET2200
C ISTRES	= STRESS PRINT FLAG. (0=NO STRESSES,.NE. 0 PRINT STRESSES)	ABET2210
C ITAPE	= CONTINUATION DATA DUMP SITE. (0=NO DUMP,.NE.0,OTHER FILE)	ABET2220
C IUNITS	= INPUT-OUTPUT DIMENSIONAL UNITS FLAG.	ABET2230
C IYFLAG	= NEWLY YIELDED ELEMENT FLAG. (0=NONE,1=YIELD DETECTED)	ABET2240
C IYLD	= COUNTER FOR NO. OF ELEMENTS WITH MSTAT(M)=3.	ABET2250
C JOINTS	= COMMON BLOCK OF JOINT DATA.	ABET2260
C KDATA	= INDEXES OF RECORDS IN IN-CORE FILE CALLED DATA.	ABET2270
C LCURV	= STARTING INDEX OF CURVATURE DATA IN DATA ARRAY.	ABET2280
C LEADBK	= COMMON BLOCK OF DATA LEADING PROBLEM SOLUTION.	ABET2290
C LERR	= STORAGE ERROR FLAG. (0= NO ERRORS)	ABET2300
C LFF	= STARTING INDEX OF JOINT FORCING FUNCTIONS IN DATA ARRAY.	ABET2310
C LFFI	= STARTING INDEX OF JOINT FORCING FUNCTIONS IN KDATA ARRAY.	ABET2320
C LINE	= CURRENT NUMBER OF THE LINE BEING OUTPUT.	ABET2330
C LMAX	= MAXIMUM NUMBER OF DATA LOCATIONS USED IN THIS PROBLEM.	ABET2340
C LMAXI	= MAXIMUM NUMBER OF KDATA LOCATIONS USED IN THIS PROBLEM.	ABET2350
C LP	= STARTING INDEX OF PLASTIC STRAIN DATA IN DATA ARRAY.	ABET2360
C LPI	= STARTING INDEX OF PLASTIC STRAIN DATA IN KDATA ARRAY.	ABET2370
C LPSI	= STARTING INDEX OF STRESS HISTORY DATA IN KDATA ARRAY.	ABET2380



C LTAB	= STARTING INDEX OF FUNCTION TABLES IN DATA ARRAY.	ABET2390
C LTAB1	= STARTING INDEX OF FUNCTION TABLES IN KDATA ARRAY.	ABET2400
C MAINBK	= COMMON BLOCK FOR PRINCIPAL SIMULATION CONSTANTS.	ABET2410
C MATR	= CONFINED CONCRETE MATERIAL I.D., BY ELEMENT.	A3ET2420
C MATW	= MATERIAL OF WIDE FLANGE BEAM COMPONENT, BY ELEMENT.	ABET2430
C MBAR	= MATERIAL OF LONGITUDINAL REINFORCEMENT, BY ELEMENT.	ABET2440
C MCODE	= UNCONFINED CONCRETE MATERIAL I.D., BY ELEMENT.	ABET2450
C MEMBER	= COMMON BLOCK OF MEMBER PARAMETERS	ABET2460
C MSHFAR	= ELEMENT SHEAR FLAG. (0=IGNORE, 1=CHECK)	ABET2470
C MSTAT	= ELEMENT STATUS FLAG, BY ELEMENT.	ABET2480
C MTIFS	= MATERIAL OF LATERAL REINFORCEMENT, BY ELEMENT.	ABET2490
C MTYPE	= TYPE OF ELEMENT.	ABET2500
C NACC	= NUMBER OF INITIAL ACCELERATIONS SPECIFIED BY USER.	ABET2510
C NAME	= NAMES OF MATERIALS FOR THIS PROBLEM.	ABET2520
C NCRD	= NUMBER OF PERIPHERAL FILE FOR CARD DATA.	ABET2530
C NOF	= NUMBER OF DEGREES OF FREEDOM FOR THIS PROBLEM.	ABET2540
C NDFD	= MAXIMUM NUMBER OF DEGREES OF FREEDOM MAPPED.	ABET2550
C NOFJ	= NUMBER OF DEGREES OF FREEDOM AT JOINTS.	ABET2560
C NDIS	= NUMBER OF INITIAL DISPLACEMENTS SPECIFIED BY USER.	ABET2570
C NOL	= NUMBER OF DISTRIBUTED LOADINGS GIVEN BY USER.	ABET2580
C NFF	= NUMBER OF FORCING FUNCTIONS SPECIFIED BY USER.	ABET2590
C NGRP	= NUMBER OF GROUPS OF LONGITUDINAL REINFORCEMENT, BY ELEM.	ABET2600
C NINC	= NUMBER OF INITIAL CONDITIONS SPECIFIED BY USER (TOTAL)	ABET2610
C NJ	= NUMBER OF JOINTS FOR THIS PROBLEM.	ABET2620
C NJ0	= MAXIMUM NUMBER OF JOINTS MAPPED.	ABET2630
C NJER	= NUMBER OF CONDITIONAL STOP ERRORS.	ABET2640
C NJOR	= NUMBER OF JOINTS WITH POINT LOADINGS GIVEN BY USER.	ABET2650
C NL	= NUMBER OF LINES THAT MAY BE PRINTED ON AN OUTPUT PAGE.	ABET2660
C NLD	= MAXIMUM NUMBER OF LEAF SPRINGS MAPPED.	ABET2670
C NLS	= NUMBER OF LEAF SPRINGS FOR THIS PROBLEM.	ABET2680



C NLSR	=	NUMBER OF LEAF SPRING RIGIDITY CONSTRAINTS.	ABET2690
C NM	=	NUMBER OF ELEMENTS FOR THIS PROBLEM.	ABET2700
C NMAS	=	NUMBER OF MASSES FOR THIS PROBLEM. (INCLUDES BODY MASS)	ABET2710
C NMAT	=	NUMBER OF MATERIALS FOR THIS PROBLEM.	ABET2720
C NMATD	=	MAXIMUM NUMBER OF MATERIALS MAPPED.	ABET2730
C NMAX	=	MAXIMUM INDEX OF DATA ARRAY.	ABET2740
C NMAXI	=	MAXIMUM INDEX OF KDATA ARRAY.	ABET2750
C NMD	=	MAXIMUM NUMBER OF ELEMENTS MAPPED	ABET2760
C NPLOT	=	NUMBER OF PERIPHERAL UNIT FOR RETRIEVAL FILE DATA.	ABET2770
C NPRT	=	NUMBER OF PERIPHERAL UNIT FOR PRINT DATA.	ABET2780
C NSAVE	=	NUMBER OF PERIPHERAL UNIT FOR CONTINUATION DATA. (WRITES)	ABET2790
C NSPAG	=	NUMBER OF TIMES A PARTICULAR STIRRUP SPACING OCCURS.	ABET2800
C NTAB	=	NUMBER OF FUNCTION TABLES SPECIFIED BY USER.	ABET2810
C NTAPE	=	NUMBER OF PERIPHERAL UNIT FOR CONTINUATION DATA. (READS)	ABET2820
C NTIES	=	NUMBER OF LATERAL REINFORCEMENT GROUPS, BY ELEMENT.	ABET2830
C NTIMES	=	MAXIMUM NUMBER OF TIME EVALS FOR THIS PROBLEM.	ABET2840
C NVEL	=	NUMBER OF INITIAL VELOCITIES SPECIFIED BY USER.	ABET2850
C PDP	=	CONCRETE CONFINEMENT FACTOR, BY ELEMENT.	ABET2860
C PI	=	3.1415926535897800.	ABET2870
C PERF	=	POISSON'S RATIO, BY MATERIAL ERRORS.	ABET2880
C RERH	=	MAXIMUM OF JOINT HALF-TIME ERRORS.	ABET2890
C RERZ	=	MAXIMUM OF JOINT ZERO-TIME ERRORS.	ABET2900
C S	=	STRESS DATA ARRAY FOR CURRENTLY ACTIVE POINT.	ABET2910
C SCALE	=	COMMON BLOCK OF SCALE FACTORS FOR DIMENSIONAL UNITS.	ABET2920
C SERR	=	MAXIMUM TOLERABLE RELATIVE ERROR IN THE TOTAL ENERGY.	ABET2930
C SLOPE	=	SLOPES OF SEGMENTS OF STRESS-STRAIN CURVES.	ABET2940
C SPRING	=	LEAF SPRING FLEXIBILITY COEFFICIENTS, BY LEAF.	ABET2950
C ST	=	STRESS-STRAIN DATA FOR DEFAULT STEELS.	ABET2960
C STIES	=	SPACING OF TIES OR STIRRUPS.	ABET2970
			ABET2980

C STN	= STRAIN COORDINATES OF MATERIALS FOR THIS PROBLEM.	ABET2990
C STORE	= COMMON BLOCK OF STORAGE INDEXES.	ABET3000
C STS	= STRESS COORDINATES OF MATERIALS FOR THIS PROBLEM.	ABET3010
C TBEGIN	= TIME AT WHICH TRANSIENT INTEGRATION BEGINS.	ABET3020
C TFWF	= THICKNESS- FLANGE OF WIDE FLANGE BEAM, BY ELEMENT.	ABET3030
C THALT	= TIME AT WHICH TRANSIENT INTEGRATION ENDS.	ABET3040
C TIME	= CURRENT TIME OF TRANSIENT INTEGRATION.	ABET3050
C TINK	= APPROXIMATE TRANSIENT TIME FOR PRINTING STATE DATA.	ABET3060
C TINY	= THE SMALLEST NUMBER THE COMPUTER RECOGNIZES.	ABET3070
C TPROB	= MAXIMUM TIME PERMITTED FOR THIS COMPUTER RUN.	ABET3080
C TWWF	= THICKNESS- WEB OF WIDE FLANGE BEAM, BY ELEMENT.	ABET3090
C UNLK	= UNLOADING CURVE CONSTANT FOR CONCRETE.	ABET3100
C VEL	= VELOCITY COMPONENTS, BY DEGREE OF FREEDOM.	ABET3110
C WFPI	= PRINCIPAL MOMENT OF INERTIA OF WIDE FLANGE BEAM.	ABET3120
C X	= X COORDINATE, BY JOINT.	ABET3130
C XBEG	= DISTANCE- JOINT +P+ TO START OF LONGITUDINAL REBAR GROUP.	ABET3140
C XBEGM	= DISTANCE- JOINT +P+ TO EFFECTIVE START OF ELEMENT.	ABET3150
C XBEGS	= DISTANCE- JOINT +P+ TO START OF STIRRUPS.	ABET3160
C XDJ	= CURRENT VALUE OF GLOBAL JOINT DISPLACEMENTS, BY D.O.F.	ABET3170
C XL	= ELEMENT LENGTH, BY ELEMENT.	ABET3180
C Y	= Y COORDINATE, BY JOINT.	ABET3190
C YBAR	= DISTANCE- REFERENCE AXIS TO LONGITUDINAL REBAR.	ABET3200
C YLDS	= YIELD STRESS OF STIRRUPS, BY ELEMENT.	ABET3210
C ZI	= AVG. CRACKED MOMENT OF INERTIA OF CONCRETE, BY ELEMENT.	ABET3220
		ABET3230

END

```

CACIN 0 10
SUBROUTINE ACIN
C
C THIS SUBROUTINE READS INPUT DATA FROM CARDS
C
COMMON DATA(10000),KDATA(500)
COMMON/ELEMENT/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),
1 SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),DIS(3,50),ERJF(3,50),
1 ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
1 XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1 PI,REFR,RERH,REZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
INTEGER HEAD,DHEAD
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLDT,IPRINT,
1 IREG,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,
2 NCRD,NDF,NDFD,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJO,NJER,NL,NLD,
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,
4 NTIMES,NVEL,IINITD
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BDM(10,45),
1 BWF(45),D(45),DP(45),DPP(45),DWF(45),EFFL(10,45),EFLM(45),
2 HMEM(45),HTOP(45),HTWF(45),HWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),
3 TFWF(45),TWF(45),UDM(45),URM(45),XBEG(10,45),
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),
5 YFIBR(11,45),YLOS(45),XDM(45),PDF(7,45),DISM(45)
COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB,
ACIN 0
ACIN 10
ACIN 20
ACIN 30
ACIN 40
ACIN 50
ACIN 60
ACIN 70
ACIN 80
ACIN 90
ACIN 100
ACIN 110
ACIN 120
ACIN 130
ACIN 140
ACIN 150
ACIN 160
ACIN 170
ACIN 180
ACIN 190
ACIN 200
ACIN 210
ACIN 220
ACIN 230
ACIN 240
ACIN 250
ACIN 260
ACIN 270
ACIN 280

```

1	LTABI,NMAX,NMAXI	ACIN 290
C		ACIN 300
C		ACIN 310
C	READ CONTROL DATA, BLOCK 1.	ACIN 320
C		ACIN 330
	CALL GIDE	ACIN 340
	IF (TPROB.EQ.-1.0E0) GO TO 250	ACIN 350
	IF (ISTART.EQ.0) GO TO 30	ACIN 360
C		ACIN 370
C	READ RECOVERY DATA.	ACIN 380
	CALL REGO(ISTART)	ACIN 390
	GO TO 70	ACIN 400
C		ACIN 410
C	READ JOINT COORDINATES AND CONSTRAINTS, BLOCK 2.	ACIN 420
C		ACIN 430
30	CALL REJO	ACIN 440
C		ACIN 450
C	READ MATERIAL TABLE DATA, BLOCK 3.	ACIN 460
C		ACIN 470
	CALL MATP	ACIN 480
C		ACIN 490
C	READ ELEMENT DATA, BLOCK 4.	ACIN 500
C		ACIN 510
	CALL BEAM	ACIN 520
	CALL LINK	ACIN 530
C		ACIN 540
C	READ LUMPED MASS DATA, BLOCK 5.	ACIN 550
C		ACIN 560
	CALL MASS	ACIN 570
	CALL BODY	ACIN 580



C	SET NEGLIGIBLE MASSES ZERO AND MAKE COUNT.	ACIN 590
C	IF (NMAE.EQ.0) GO TO 60	ACIN 600
	RHO=0.E0	ACIN 610
	DO 40 J=1,NJ	ACIN 620
	DO 40 I=1,3	ACIN 630
40	RHO=RHO+DAS(I,J)	ACIN 640
	IF (RHO.EQ.0.E0) GO TO 60	ACIN 650
	I1=0	ACIN 660
	TEST=EPS*10.E0	ACIN 670
	DO 50 J=1,NJ	ACIN 680
	DO 50 I=1,3	ACIN 690
	I1=I1+1	ACIN 700
	IF (DAS(I,J)/RHO.GT.TEST) GO TO 50	ACIN 710
	I1=I1-1	ACIN 720
	DAS(I,J)=0.E0	ACIN 730
50	CONTINUE	ACIN 740
	NMAE=I1	ACIN 750
C	READ INITIAL CONDITIONS, BLOCK 6.	ACIN 760
C		ACIN 770
C	CALL INIT	ACIN 780
60		ACIN 790
C	READ FUNCTION TABLES, BLOCK 7.	ACIN 800
C		ACIN 810
C	CALL FTAB	ACIN 820
C		ACIN 830
C	READ JOINT FORCING FUNCTIONS, BLOCK 8.	ACIN 840
C		ACIN 850
C	CALL JFOR	ACIN 860
		ACIN 870
		ACIN 880

```

C C GENERATE EXTRA ELEMENT DATA FOR INTERIOR JOINTS.
C CALL CUTS
C C CALCULATE LOCATION OF INTEGRATION POINTS.
C CALL SECT
C C ESTABLISH INTEGRATION CONSTANTS FOR CONCRETE AND POINTS 5 AND 6
C OF THE STRESS-STRAIN CURVE.
C DO 65 M=1,NM
C IF (M*TYPE(M).LT.4) CALL CONC(M)
C CONTINUE
C PRINT PROBLEM DESCRIPTIVE SUMMARY
C CALL SUMY
C NOTE ERROR STATUS.
C IF (IERR.EQ.0) GO TO 90
C PRINT 80, IERR
C GO TO 250
C 80 FORMAT (/1H,38H *** NUMBER OF INPUT ERRORS DETECTED =,I5,33H,
C 1ROBLEM TERMINATED (ACIN). ***)
C INITIALIZE STORAGE ADDRESS FOR PLASTIC STRAIN AND STRESS DATA.
C LMAX=LP
C LPSI=LPI+NM
C LMAXI=LPSI+NM
C 90
ACIN 890
ACIN 900
ACIN 910
ACIN 920
ACIN 930
ACIN 940
ACIN 950
ACIN 960
ACIN 970
ACIN 980
ACIN 990
ACIN1000
ACIN1010
ACIN1020
ACIN1030
ACIN1040
ACIN1050
ACIN1060
ACIN1070
ACIN1080
ACIN1090
ACIN1100
ACIN1110
ACIN1120
ACIN1130
ACIN1140
ACIN1150
ACIN1160
ACIN1170
ACIN1180

```

```

100 IF (LMAXI.LE.NMAXI) GO TO 110
    PRINT 100
    FORMAT (//1H ,63H*** PROBLEM STORAGE REQUIREMENTS EXCEED KDATA ARR
110 1AY (ACIN). ***)
    LERR=1
    GO TO 140
    NM2=2*NM
    DO 120 M=1,NM2
    K=LPI+M
    KDATA(K)=0
120
C
C
C
    ESTABLISH DATA STORAGE FOR PLASTIC STRESS-STRAIN HISTORY.
    DO 130 M=1,NM
    IF(MSTAT(M).EQ.1) IYLD = IYLD + 1
    IF(MSTAT(M).EQ.3) CALL STOR(M)
    CONTINUE
130
C
C
C
    PRINT STORAGE LOCATION INDEXES.
    IF (LERR.NE.0) GO TO 190
    WRITE (NPRT,150)
    FORMAT (//10X,46HSTORAGE LOCATION INDEXES IN DATA ARRAY (ACIN)./)
150 WRITE (NPRT,160) LCURV,LTAB,LFF,LP,LMAX,NMAX
    FORMAT (14X,17HMINIMIZATION DATA,I19/14X,15HFUNCTION TABLES,I21/14X,14X
160 1X,17HFORCING FUNCTIONS,I19/14X,19HPLASTIC STRAIN DATA,I17/14X,12HEACIN1440
    2ND OF ARRAY,I24/14X,16HSPACES ALLOCATED,I20//)
    WRITE (NPRT,170)
    FORMAT (10X,47HSTORAGE LOCATION INDEXES IN KDATA ARRAY (ACIN)./)
170 WRITE (NPRT,180) LTABI,LFFI,LPI,LPSI,LMAXI,NMAXI
    ACIN1190
    ACIN1200
    ARRACIN1210
    ACIN1220
    ACIN1230
    ACIN1240
    ACIN1250
    ACIN1260
    ACIN1270
    ACIN1280
    ACIN1290
    ACIN1300
    ACIN1310
    ACIN1320
    ACIN1330
    ACIN1340
    ACIN1350
    ACIN1360
    ACIN1370
    ACIN1380
    ACIN1390
    ACIN1400
    ACIN1410
    ACIN1420
    ACIN1430
    ACIN1440
    ACIN1450
    ACIN1460
    ACIN1470
    ACIN1480

```

```

180  FORMAT (14X,15HFUNCTION TABLES,I21/14X,17HFORCING FUNCTIONS,I19/14ACIN1490
190  1X,19HPLASTIC STRAIN DATA,I17/14X,19HSTRESS HISTORY DATA,I17/14X,12ACIN1500
200  2HEND OF ARRAY,I24/14X,16HSPACES ALLOCATED,I20)
    GO TO 210
C
210  PRINT 200
    FORMAT (//1H ,110H*** PREVIOUS DATA ERROR, CALCULATION OF STORAGE
1INDEXES FOR DATA AND KDATA ARRAYS IS NOT COMPLETED (ACIN). ***)
    GO TO 250
C
C  CALCULATE DIMENSIONALIZING PARAMETERS.
C
210  AVGL=0.E0
    AVGA=0.E0
    DO 230 M=1,NM
        AVGL=AVGL+XL(M)
        IF (M*TYPE(M).EQ.4) GO TO 220
        AVGA=AVGA+HMEM(M)*BMEM(M)
    GO TO 230
220  AVGA=AVGA+2.E0*BWF(M)*TFWF(M)+TWWF(M)*(HTWF(M)-2.E0*TFWF(M))
230  CONTINUE
    AVGL=AVGL/FLOAT(NM)
    AVGA=AVGA/FLOAT(NM)
    AVGE=0.E0
    DO 240 I=1,NMAT
        AVGE=AVGE+ET(I)+EC(I)
        AVGE=AVGE/(2.E0*FLOAT(NMAT))
        AVDM=AVGL*AVGA*AVGE
C
250  RETURN

```



ACIN1790  
ACIN1800

C      END

```

CADYN      0 10
C          SUBROUTINE ADYN(SOLN)

COMMON DATA(10000), KOATA(500)
COMMON/ELEMET/ICARD, IP(45), IPL(20), IQ(45), IQL(20), MATR(45),
1  MATH(45), MBAR(10,45), MCODE(45), MSHEAR(45), MSTAT(45), MTIES(45),
2  MTYPE(45), NGRP(45), NSPAC(6,45), NTIES(45)
COMMON/FIBER/DENS(9), EC(9), EPSU(9), ET(9), FCFY(9), G(9), PR(9), S(9),
1  SLOPE(8,9), ST(17,6), STN(8,9), STS(8,9), UNLK(9), ICODE(9), NAME(9)
COMMON/JOINTS/ACC(3,50), BET(3,50), DAS(3,50), DIS(3,50), ERJF(3,50),
1  ERJH(3,50), ERJZ(3,50), F(3,50), FOR(3,50), VEL(3,50), X(50),
1  XOJ(3,50), Y(50), DER(3,50), RESENG(3,50), IOFI(90), IOFII(90)
COMMON/LEADBK/AVDM, AVGL, CA, CB, CC, CD, CE, DHEAD(20), DT, EPS, HEAD(20),
1  PI, RERF, RERH, RERZ, SERR, TBEGIN, THALT, TIME, TINK, TINY, TPROB
COMMON/MAINBK/IANAL, ICURV, IERR, IFAIL, IFOR, ILIN, IPAGE, IPLOT, IPRINT,
1  IREC, ISTART, ISTOP, ISTRES, ITAPE, IUNITS, IYLD, LERR, LINE, NACC, NCM,
2  NCRO, NOF, NOFD, NOFJ, NOIS, NDL, NFF, NJOR, NING, NJ, NJO, NJER, NL, NLD,
3  NLS, NLSR, NM, NMAS, NMAT, NMATD, NMD, NPLOT, NPRT, NSAVE, NTAB, NTAPE,
4  NTIMES, NVEL, IINITD
COMMON/MEMBER/AGRP(10,45), ATIES(6,45), BMEM(45), BPP(45), BOM(10,45),
1  BWF(45), D(45), DP(45), DPP(45), DWF(45), EFFL(10,45), EFLM(45),
2  HMEM(45), HTOP(45), HTWF(45), PDP(7,45), SPRING(5,20), STIES(7,45),
3  TFWF(45), TWWF(45), UDM(45), URM(45), XBEG(10,45),
4  XBEGM(45), XBEGS(6,45), XL(45), XPI(5,45), YBAR(10,45), YGP(7,45),
5  YFIBR(11,45), YLOS(45), XOM(45), PDF(7,45), DISM(45)
COMMON/SAVEBK/SAVACC(3,50), SAVAXL(2,45), SAVCRV(2,45), SAVMOM(2,45)
1  , SAVSHR(2,45), SAVSRP(3,20), SAVSRQ(3,20), SAVXDJ(3,50),
2  SAVVEL(3,50), SVSTRN(12,45), SVSTRS(12,45)
COMMON/STORE/LCURV, LFF, LFFI, LMAXI, LMAX, LP, LPI, LPSI, LTAB,
1  LTABI, NMAX, NMAXI
ADYN      0
ADYN     10
ADYN     20
ADYN     30
ADYN     40
ADYN     50
ADYN     60
ADYN     70
ADYN     80
ADYN     90
ADYN    100
ADYN    110
ADYN    120
ADYN    130
ADYN    140
ADYN    150
ADYN    160
ADYN    170
ADYN    180
ADYN    190
ADYN    200
ADYN    210
ADYN    220
ADYN    230
ADYN    240
ADYN    250
ADYN    260
ADYN    270
ADYN    280

```

```

COMMON/SEEK/DEFOR(90),STPSIZ(90),GRAD(90),GRADI(90),DELTA(90),DELTA(90),
1  DIRECT(90),DIAG(90),STEP(4),DSTEP(4),FVAL(4),VALUES(7),
2  DISACC,SSIZE,FUNACC,FUNMIN,CRITL,CRITU,NLIN
COMMON/STRNBK/SRP(4),SRQ(4),UX,UY,UZ,XLEN,AREA,ZZI,IMAT
C
C  INTEGER HEAD,DHEAD
C  DIMENSION SOLN(90)
C  DATA DTMIN/1.E-07/
C
C  THIS SUBROUTINE PERFORMS DYNAMIC ANALYSIS
C
C  INITIALIZE PROBLEM DATA WITH STATIC ANALYSIS
C  CALL ASAN(SOLN)
C
C  ADD CALCULATED INITIAL DISPLACEMENTS TO PRESCRIBED DISPLACEMENTS.
C
DO 151 I=1,NDFJ
J=IDFI(I)
K=IDFII(I)
151 DIS(K,J)=DIS(K,J)+SOLN(I)
L=NDFJ+1
DO 152 I=L,NDF
M=IDFI(I)
152 DISM(M)=DISM(M)+SOLN(I)
C
C  SET INITIAL DISPLACEMENTS FOR DYNAMIC ANALYSIS
C
DO 156 I=1,NDFJ
J=IDFI(I)
K=IDFII(I)

```

```

156      SOLN(I)=DIS(K,J)
      XDJ(K,J)=SOLN(I)
      L=NDFJ+1
      DO 157 I=L,NDF
      M=IDFI(I)
      SOLN(I)=DISM(M)
157      XDM(M)=SOLN(I)
      C
      C CALCULATE INITIAL ACCELERATIONS.
      C
      IF(NMAS.EQ.0) GO TO 170
      IF(IFOR.EQ.0.AND.NFF.EQ.0) GO TO 170
      DO 161 J=1,NJ
      DO 161 K=1,3
161      F(K,J)=0.E0
      IF(NFF.EQ.0) GO TO 162
      CALL FORS(TIME)
      DO 164 J=1,NJ
      DO 164 K=1,3
      DFOR=F(K,J)-FOR(K,J)
      IF(DAS(K,J).EQ.0.E0) GO TO 164
      DO 163 I=1,NDFJ
      IF (J.EQ.IDFI(I).AND.K.EQ.IDFII(I)) GO TO 165
163      CONTINUE
      GO TO 164
165      ACC(K,J) = DFOR/DAS(K,J) + ACC(K,J)
164      CONTINUE
      C
      C FOR MASSLESS DEGREES-OF-FREEDOM SET VELOCITY, ACCELERATION,
      C AND BETA EQUAL TO ZERO

```

```

ADYN 590
ADYN 600
ADYN 610
ADYN 620
ADYN 630
ADYN 640
ADYN 650
ADYN 660
ADYN 670
ADYN 680
ADYN 690
ADYN 700
ADYN 710
ADYN 720
ADYN 730
ADYN 740
ADYN 750
ADYN 760
ADYN 770
ADYN 780
ADYN 790
ADYN 800
ADYN 810
ADYN 820
ADYN 830
ADYN 840
ADYN 850
ADYN 860
ADYN 870
ADYN 880

```



```

C      170      DO 172 J=1,NJ
                DO 172 K=1,3
                IF(OAS(K,J).NE.0.E0) GO TO 172
                VEL(K,J)=0.E0
                ACC(K,J)=0.E0
                BET(K,J)=0.E0
                CONTINUE
C      172
C
                IFOR=0
                IF(NFF.NE.0) IFOR=1
                DO 201 J=1,NJ
                DO 201 K=1,3
                F(K,J)=0.E0
                201 FOR(K,J)=0.E0
C      BEGIN CURRENT TIME STEP AND UPDATE ERROR DATA
C
                203      RERZ=RERF
                DO 206 J=1,NJ
                DO 206 K=1,3
                206      ERJZ(K,J)=ERJF(K,J)
C      INCREMENT TIME
                209      TIME=TIME+DT
C
C      CHECK FOR COMPLETION OF INTEGRATION
C
                CALL TICS(TIMN,IGA)
                IF(IGA.EQ.2) GO TO 400
                WRITE(NPRT,971) TIME,DT
                971      FORMAT(1H1,17HSOLUTION FOR TIME,0PE13.5,23H, WITH TIME INTERVAL OF ADYN1180
ADYN 890
ADYN 900
ADYN 910
ADYN 920
ADYN 930
ADYN 940
ADYN 950
ADYN 960
ADYN 970
ADYN 980
ADYN 990
ADYN1000
ADYN1010
ADYN1020
ADYN1030
ADYN1040
ADYN1050
ADYN1060
ADYN1070
ADYN1080
ADYN1090
ADYN1100
ADYN1110
ADYN1120
ADYN1130
ADYN1140
ADYN1150
ADYN1160
ADYN1170
ADYN1180

```

```

1,E13.5//)
C
C
C PREDICT DISPLACEMENTS FOR CURRENT TIME INTERVAL AND FORM 1D
C DISPLACEMENT ARRAY
C
      IF (NMA5.EQ.0) GO TO 220
      DO 211 I=1,NDFJ
      J=IOFI(I)
      K=IOFII(I)
      211 SOLN(I)=BET(K,J)*DT**3/6.E0+ACC(K,J)*DT**2/2.E0+VEL(K,J)*DT+
          1 DIS(K,J)
          L=NDFJ+1
          DO 212 I=L,NDF
          M=IOFI(I)
          212 SOLN(I)=DISM(M)
C CALCULATE FORCING FUNCTION FOR CURRENT TIME STEP
C
      220 IF(NFF.EQ.0) GO TO 240
      CALL FORS(TIME)
      DO 221 I=1,NFF
      L=LFFI+5*I
      J=KDATA(L-4)
      K=KDATA(L-2)
      221 FOR(K,J)=F(K,J)
C
C SOLVE FOR DISPLACEMENTS BY FUNCTION MINIMIZATION PROCEDURE
C
      240 CALL SEEK(SOLN,VALUEM)
      DO 243 I=1,NDFJ

```

```

ADYN1190
ADYN1200
ADYN1210
ADYN1220
ADYN1230
ADYN1240
ADYN1250
ADYN1260
ADYN1270
ADYN1280
ADYN1290
ADYN1300
ADYN1310
ADYN1320
ADYN1330
ADYN1340
ADYN1350
ADYN1360
ADYN1370
ADYN1380
ADYN1390
ADYN1400
ADYN1410
ADYN1420
ADYN1430
ADYN1440
ADYN1450
ADYN1460
ADYN1470
ADYN1480

```

```

      J=IDFI(I)
      K=IDFII(I)
243  XDJ(K,J)=SOLN(I)
      L=NDFJ+1
      DO 244 I=L,NDF
      M=IDFI(I)
244  XDM(M)=SOLN(I)
      C
      C CHECK STATUS OF ELASTIC-PLASTIC MEMBERS.
      C IYFLAG = 0
      C IF (IYLO.LT.NM) CALL TEST (IYFLAG)
      C
      C STORE ENERGIES AND STRESS RESULTANTS, AND CHECK MEMBER FAILURE
      C CRITERIA.
      C CALL FAIL
      C
      C REPEAT DYNAMIC CALCULATION IF MEMBERS HAVE YIELDED.
      C IF (IYFLAG.EQ.1.AND.LERR.EQ.0.AND.IERR.EQ.0) GO TO 240
      C
      C CALCULATE ERROR MEASURES FOR CURRENT TIME STEP
      C
      C WRITE(NPRT,971) TIME,DT
      C CALL ERRS(SOLN,VALUEM)
      C WRITE(NPRT,972)RERZ,RERH,RERF
      C FORMAT(1H0,5X,39HTOTAL ERROR MEASURES, ZERO-TIME ERROR=,0PE13.5/
      C 11H ,28X,16HHALF-TIME ERROR=,E14.5/1H ,28X,16HFULL-TIME ERROR=,E14.
      C 25//)
      C
      C IF DATA ERRORS HAVE OCCURED, SAVE PREVIOUS SOLUTION ON TAPE FOR
      C SUBSEQUENT RESTART.

```

```

ADYN1490
ADYN1500
ADYN1510
ADYN1520
ADYN1530
ADYN1540
ADYN1550
ADYN1560
ADYN1570
ADYN1580
ADYN1590
ADYN1600
ADYN1610
ADYN1620
ADYN1630
ADYN1640
ADYN1650
ADYN1660
ADYN1670
ADYN1680
ADYN1690
ADYN1700
ADYN1710
ADYN1720
ADYN1730
ADYN1740
ADYN1750
ADYN1760
ADYN1770
ADYN1780

```

```

C      IF(IERR.NE.0.OR.LERR.NE.0) GO TO 400
C      C CHECK SOLUTION ACCURACY.  IF NECESSARY, REDUCE TIME INTERVAL
C      C AND REPEAT TIME STEP.
C
      IF (CRITU.EQ.0.E0) GO TO 289
      IF(RERF.LE.CRITU) GO TO 283
      ERRXX=RERF
      GO TO 284
283  ERRXX= RERH-(RERZ+RERF)/2.
      IF(ERRXX.LE.CRITU) GO TO 289
284  WRITE(NPRT,973) ERRXX,CRITU
973  FORMAT(1H0,5X,46H THE REQUIRED ACCURACY WAS NOT ACHIEVED (ERROR=,1P
      1E13.5,11H, REQUIRED=,E13.5,1H) )
      IF(DT.EQ.DTMIN) GO TO 288
      TIME=TIME-DT
      DT=0.6*DT
      IF (DT.LT.DTMIN) DT = DTMIN
      WRITE (NPRT,974)
974  FORMAT(1H ,5X,65H THE TIME INTERVAL IS REDUCED AND THE INTEGRATION
      1STEP IS REPEATED)
      GO TO 209
288  WRITE(NPRT,975)
975  FORMAT (1H ,80H*** WITH MINIMUM TIME INTERVAL. RESULTS ARE REPORT
      1ED AND INTEGRATION CONTINUES.//)
289  CONTINUE
C
C      C INTEGRATION FOR CURRENT TIME STEP IS COMPLETE.
C      C UPDATE RESPONSE RESULTS.
C
ADYN1790
ADYN1800
ADYN1810
ADYN1820
ADYN1830
ADYN1840
ADYN1850
ADYN1860
ADYN1870
ADYN1880
ADYN1890
ADYN1900
ADYN1910
ADYN1920
ADYN1930
ADYN1940
ADYN1950
ADYN1960
ADYN1970
ADYN1980
ADYN1990
ADYN2000
ADYN2010
ADYN2020
ADYN2030
ADYN2040
ADYN2050
ADYN2060
ADYN2070
ADYN2080

```



```

IF (NMAS.EQ.0) GO TO 295
DO 291 I=1,NDF J
J=IDFI(I)
K=IDFII(I)
IF (DAS(K,J).EQ.0.E0) GO TO 291
BET(K,J)=6.E0*((SOLN(I)-DIS(K,J))/(DT*DT))-VEL(K,J)/DT
1 -ACC(K,J)*0.5E0/DT
VEL(K,J)=VEL(K,J)+ACC(K,J)*DT+BET(K,J)*DT*0.5E0
ACC(K,J)=ACC(K,J)+BET(K,J)*DT
DIS(K,J)=SOLN(I)
GO TO 297
291
295 DO 296 I=1,NDF J
J=IDFI(I)
K=IDFII(I)
DIS(K,J)=SOLN(I)
L=NDF J+1
DO 298 I=L,NDF
M=IDFI(I)
DISM(M)=SOLN(I)
298
C
C PRINT RESPONSE RESULTS
C
CALL OUTS
IF (IPLOT.EQ.1) CALL PLOG(NPLOT)
IF (IFAIL.EQ.1) RETURN
C
C DETERMINE TIME INTERVAL FOR NEXT TIME STEP
C
IF (CRITU.EQ.0.E0) GO TO 382
IF (ERRXX.GT.CRITL) GO TO 381

```

```

ADYN2090
ADYN2100
ADYN2110
ADYN2120
ADYN2130
ADYN2140
ADYN2150
ADYN2160
ADYN2170
ADYN2180
ADYN2190
ADYN2200
ADYN2210
ADYN2220
ADYN2230
ADYN2240
ADYN2250
ADYN2260
ADYN2270
ADYN2280
ADYN2290
ADYN2300
ADYN2310
ADYN2320
ADYN2330
ADYN2340
ADYN2350
ADYN2360
ADYN2370
ADYN2380

```

```

990      WRITE(NPRT,990) ERRXX
          FORMAT(1H0,41HTIME INTERVAL IS INCREASED FOR NEXT STEP.,9H ERROR
1=0PE12.4)
          DT=1.85*DT
          GO TO 382
381      WRITE(NPRT,991)ERRXX
991      FORMAT(1H0,43HTIME INTERVAL IS NOT CHANGED FOR NEXT STEP.,9H  ERR
10R=,0PE12.3)
382      CONTINUE
C
C GO TO NEXT TIME STEP
C
C      IF(IERR.EQ.0.AND.LERR.EQ.0) GO TO 203
C
C INTEGRATION FOR PROBLEM IS COMPLETE, RETURN TO MAIN.
C
400      IF (ITAPE.NE.0) CALL REGO (-ITAPE)
          RETURN
          END
ADYN2390
ADYN2400
ADYN2410
ADYN2420
ADYN2430
ADYN2440
ADYN2450
ADYN2460
ADYN2470
ADYN2480
ADYN2490
ADYN2500
ADYN2510
ADYN2520
ADYN2530
ADYN2540
ADYN2550
ADYN2560
ADYN2570

```

```

CASAN 0 10
SUBROUTINE ASAN (SOLN)
C
C THIS SUBROUTINE DIRECTS STATIC ANALYSIS
C TO OBTAIN INITIAL PROBLEM DATA.
C
COMMON DATA(10000),KDATA(500)
COMMON/JOINTS/ACG(3,50),BET(3,50),DAS(3,50),DIS(3,50),ERJF(3,50),
1 ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
1 XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)
COMMON/LEADBK/AVDM,AVGL,CA,C8,CC,CE,DHEAD(20),DT,EPS,HEAD(20),
1 PI,REFR,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLT,IPRINT,ASAN
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,ASAN
2 NCRO,NDF,NDFD,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,
4 NTIMES,NVEL,IINITD
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BDM(10,45),
1 BWF(45),D(45),DP(45),DPP(45),DWF(45),EFFL(10,45),EFLM(45),
2 HMEM(45),HTOP(45),HTWF(45),POP(7,45),SPRING(5,20),STIES(7,45),
3 TFWF(45),THWF(45),UDM(45),URM(45),XBEG(10,45),
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),
5 YFIBR(11,45),YLDS(45),XDM(45),PDF(7,45),DISM(45)
COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB,
1 LTABI,NMAX,NMAXI
COMMON/SEEK8K/DEFOR(90),STPSIZ(90),GRAD(90),GRADI(90),DELTAG(90),
1 DIRECT(90),DIAG(90),STEP(4),DSTEP(4),FVAL(4),VALUES(7),
2 DISACC,SSIZE,FUNACC,FUNMIN,CRITL,CRITU,NLIN
C
INTEGER HEAD,DHEAD

```

C	DIMENSION SOLN(90)	ASAN 290
C	SET INITIAL VALUES.	ASAN 300
C		ASAN 310
	DT=TINK	ASAN 320
	TIME=TREGIN	ASAN 330
	ICURV=1	ASAN 340
	DO 10 J=1,NJ	ASAN 350
	DO 10 K=1,3	ASAN 360
	F(K,J) = 0.E0	ASAN 370
	XDJ(K,J)=0.E0	ASAN 380
	DER(K,J)=0.E0	ASAN 390
	RESENG(K,J)=0.E0	ASAN 400
	ERJZ(K,J)=0.E0	ASAN 410
	ERJH(K,J)=0.E0	ASAN 420
	ERJF(K,J)=0.E0	ASAN 430
10	DO 5 MM=1,NM	ASAN 440
	DISM(MM)=0.E0	ASAN 450
	XDM(MM)=0.E0	ASAN 460
5	RERZ=0.E0	ASAN 470
	RERH=0.E0	ASAN 480
	RERF=0.E0	ASAN 490
	VALUES(5)=0.E0	ASAN 500
	VALUES(6)=0.E0	ASAN 510
C		ASAN 520
C	NONDIMENSIONALIZE TRANSLATIONAL INITIAL CONDITIONS AND	ASAN 530
C	ADJUST DIMENSIONS OF TRANSLATIONAL FORCING FUNCTIONS.	ASAN 540
C		ASAN 550
	IF(ANAL.EQ.0.AND.NFF.EQ.0.AND.IF0F.EQ.0) GO TO 17	ASAN 560
	GO TO 19	ASAN 570
		ASAN 580



```

17 IERR=1
18 PRINT 18
19 FORMAT(1H,94H*** NEITHER FORCING FUNCTIONS NOR INITIAL CONDITIONS
1 SPECIFIED FOR STATIC ANALYSIS. (ASAN) ***)
RETURN
20 DO 20 J=1,NJ
DO 20 K=1,2
DIS(K,J)=DIS(K,J)/AVGL
VEL(K,J)=VEL(K,J)/AVGL
ACC(K,J)=ACC(K,J)/AVGL
BET(K,J)=BET(K,J)/AVGL
DAS(K,J)=DAS(K,J)*AVGL*AVGL
FOR(K,J)=FOR(K,J)*AVGL
IF (NFF.EQ.0) GO TO 40
DO 30 I=1,NFF
L=LFF+4*I
K=KDATA(LFFI+5*I-2)
IF (K.EQ.3) GO TO 30
DATA(L-2)=DATA(L-2)*AVGL
CONTINUE
30
C
C
C
40
PERFORM STATIC ANALYSIS, IF NECESSARY, FOR INITIAL APPLIED FORCES.
DTX=DT
DT=0.E0
IF ( IANAL.NE.0.AND.IFOR.EQ.0.AND.NFF.EQ.0) GO TO 125
DO 60 I=1,NDF
SOLN(I)=0.E0
IF (IANAL.EQ.0) GO TO 75
IF ( IFOR.EQ.0 ) GO TO 125

```

ASAN 530  
 ASAN 610  
 ASAN 610  
 ASAN 620  
 ASAN 630  
 ASAN 640  
 ASAN 650  
 ASAN 660  
 ASAN 670  
 ASAN 680  
 ASAN 690  
 ASAN 700  
 ASAN 710  
 ASAN 720  
 ASAN 730  
 ASAN 740  
 ASAN 750  
 ASAN 760  
 ASAN 770  
 ASAN 780  
 ASAN 790  
 ASAN 800  
 ASAN 810  
 ASAN 820  
 ASAN 830  
 ASAN 840  
 ASAN 850  
 ASAN 860  
 ASAN 870  
 ASAN 880

50	CALL PAGE	ASAN 890
	FORMAT (1H, 25HSOLUTION FOR INITIAL TIME, 0PE13.5//)	ASAN 900
	WRITE(NPRT, 50) TIME	ASAN 910
	DO 70 J=1, NJ	ASAN 920
	DO 70 K=1, 3	ASAN 930
70	IF (ABS(FOR(K, J)/AVGL-TINY).LT.1.E2*TINY) FOR(K, J)=0.E0	ASAN 940
	F(K, J)=FOR(K, J)	ASAN 950
	GO TO 80	ASAN 960
75	CALL PAGE	ASAN 970
	WRITE(NPRT, 77) TIME	ASAN 980
77	FORMAT (1H, 22HSOLUTION FOR LOAD STEP, 0PE13.5//)	ASAN 990
	IF(NFF.EQ.0) GO TO 82	ASAN1000
	CALL FORS (TIME)	ASAN1010
82	DO 79 J=1, NJ	ASAN1020
	DO 79 K=1, 3	ASAN1030
79	IF (ABS(FOR(K, J)/AVGL-TINY).LT.1.E2*TINY) FOR(K, J)=0.E0	ASAN1040
C	F(K, J)=F(K, J)+FOR(K, J)	ASAN1050
C		ASAN1060
C	STATIC SOLUTION BY FUNCTIONAL MINIMIZATION.	ASAN1070
80	CALL SEEK (SOLN, VALUEM)	ASAN1080
	DO 90 I=1, NDFJ	ASAN1090
	J=IDFI(I)	ASAN1100
	K=IDFI(I)	ASAN1110
90	XDJ(K, J)=SOLN(I)	ASAN1120
	L=NDFJ+1	ASAN1130
	DO 91 I=L, NDF	ASAN1140
	M=IDFI(I)	ASAN1150
91	XDM(M)=SOLN(I)	ASAN1160
C		ASAN1170
		ASAN1180

```

C      CHECK STATUS OF ELASTIC-PLASTIC MEMBERS.
      IYFLAG = 0
      IF (IYLD.LT.NM) CALL TEST (IYFLAG)
C
C      STORE ENERGIES AND STRESS RESULTANTS, AND CHECK MEMBER
C      FAILURE CRITERIA.
      CALL FAIL
C
C      REPEAT STATIC CALCULATION IF MEMBERS HAVE YIELDED.
      IF (IYFLAG.EQ.1.AND.LERR.EQ.0.AND.IERR.EQ.0) GO TO 80
C
C      CALCULATE ERROR FOR STATIC ANALYSIS.
      CALL ERRS (SOLN,VALUEM)*
      WRITE (NPRT,100) RERZ,RERH,RERF
      FORMAT (1H0,5X,39HTOTAL ERROR MEASURES,  ZERO-TIME ERROR=,0PE13.5/ASAN1340
11H ,28X,16HHALF-TIME ERROR=,E13.5/1H ,28X,16HFULL-TIME ERROR=,E13.5/ASAN1350
25//)
C
C      SOLUTION PRINTOUT AND STRESS CALCULATIONS FOR INITIAL TIME POINT.
      DO 120 J=1,NJ
      DO 120 K=1,3
      DIS(K,J)=XDJ(K,J)
      DO 121 L=1,NM
      DISM(L)=XDM(L)
      CALL OUTS
      DT = DTX
      IF (IPLOT.EQ.1) CALL PLOG(NPLOT)
      IF (IFAIL.EQ.1) RETURN
C
C
C
100
120
121
125
      ASAN1190
      ASAN1200
      ASAN1210
      ASAN1220
      ASAN1230
      ASAN1240
      ASAN1250
      ASAN1260
      ASAN1270
      ASAN1280
      ASAN1290
      ASAN1300
      ASAN1310
      ASAN1320
      ASAN1330
      ASAN1340
      ASAN1350
      ASAN1360
      ASAN1370
      ASAN1380
      ASAN1390
      ASAN1400
      ASAN1410
      ASAN1420
      ASAN1430
      ASAN1440
      ASAN1450
      ASAN1460
      ASAN1470
      ASAN1480

```

ASAN1490  
ASAN1500  
ASAN1510  
ASAN1520  
ASAN1530  
ASAN1540  
ASAN1550  
ASAN1560  
ASAN1570

IF (IANAL.NE.0) RETURN  
IF (NFF.EQ.0) GO TO 130  
TIME = TIME + DT  
IF (ISTOP.EQ.0.AND.IREC.GT.0) GO TO 130  
CALL TICS(TIMN,IGA)  
IF (IGA.EQ.1) GO TO 75  
IF (ITAPE.NE.0) CALL REGO (-ITAPE)  
RETURN  
END

130



```

CBARS      0 10
SUBROUTINE BARS (K,L,ADIM,DIAM,PERIM)
C
C THIS SUBROUTINE CALCULATES TOTAL AREA OF REBAR GROUPS, GIVEN BAR
C AND NUMBER OF BARS IN GROUP
C
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1 PI,REF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
INTEGER HEAD,DHEAD
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,BARS
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCH,BARS
2 NCRD,NDF,NDFD,NDFJ,NDIS,NOL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB3,NTAPE,
4 NTIMES,NVEL,IINITD
DIMENSION DB(12)
C
DATA DB(1),DB(2),DB(3),DB(4) / .25E0, .375E0, .5E0, .625E0 /
DATA DB(5),DB(6),DB(7),DB(8) / .75E0, .875E0, 1.E0, 1.128E0 /
DATA DB(9),DB(10),DB(11),DB(12) / 1.27E0, 1.41E0, 1.693E0, 2.257E0 /
C
IF (IUNITS.GE.2) GO TO 30
LM1=0
IF (L.GE.2.AND.L.LE.11) LM1=L-1
IF (L.EQ.14) LM1=11
IF (L.EQ.18) LM1=12
IF (LM1.EQ.0) GO TO 20
ANUM=K
ADIM=ANUM*PI*DB(LM1)*DB(LM1)/4.0E0
DIAM=DB(LM1)
PERIM=PI*DB(LM1)

```

```

10      L=LM1
        GO TO 40
        FORMAT (67H ***INVALID BAR SIZE NUMBER.AREA OF REBAR GROUP CANNOT
13E COMPUTED.,/,55H EFFECTIVE LENGTH OF REBAR CANNOT BE OBTAINED. (38ARS
2ARS)*** )
20      WRITE (NPRT,10)
        IERR=IERR+1
        LINE=LINE+2
        L=20
        GO TO 40

C      EUROPEAN (METRIC) BAR SIZES ARE INPUT IN FORM OF DIAMETER(MM)
C      AND IN INTEGER FORM(I.D. L=26 => BAR DIA.=26. MM. BAR SIZE
C      RUN FROM 5.0 TO 50.0 MM DIA. THIS SEGMENT CONVERTS BAR SIZES.
C      THE INPUT IN THIS SEGMENT ARE ASSUMED CORRECT.(I.D. IT IS ASSUMED
C      THE SPECIFIED BAR SIZES EXIST.)
C
C      DIAM=L
C      DIAM=DIAM/1000.E0
C      PERIM=PI*DIAM
C      ANUM=K
C      ADIM=ANUM*PI*DIAM*DIAM/4.E0
C      IF (LINE.GE.NL) CALL PAGE
C      L=20
C      RETURN
C      END

30
40

```

BARS 230  
 BARS 300  
 BARS 310  
 BARS 320  
 BARS 330  
 BARS 340  
 BARS 350  
 BARS 360  
 BARS 370  
 BARS 380  
 BARS 390  
 BARS 400  
 BARS 410  
 BARS 420  
 BARS 430  
 BARS 440  
 BARS 450  
 BARS 460  
 BARS 470  
 BARS 480  
 BARS 490  
 BARS 500  
 BARS 510  
 BARS 520  
 BARS 530  
 BARS 540

```

CBEAM 0 10
SUBROUTINE BEAM
C
C SUBROUTINE TO INPUT AND OUTPUT ELEMENT PROPERTIES
C
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),
1 SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),DIS(3,50),ERJF(3,50),
1 ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
1 XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1 PI,PERF,FERH,PERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
INTEGER HEAD,DHEAD
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,
1 IRFC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,
2 NCRD,NDF,NDFD,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLO,
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,
4 NTIMES,NVEL,IINITO
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BDM(10,45),
1 BWF(45),D(45),DP(45),DPP(45),DWF(45),EFFL(10,45),EFLM(45),
2 HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),
3 TFWF(45),TWWF(45),UDM(45),URM(45),X3EG(10,45),
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),
5 YFIBR(11,45),YLOS(45),XDM(45),PDF(7,45),DISM(45)
DATA J01,J02/1HH,1HS/,J03/1H1/,ID1,ID2/1HL,1HN/,ID3/4HNONE/
C
C INITIALIZE MEMBER COUNTER AND REBAR GROUP COUNTERS
C

```

```

BEAM 290
BEAM 300
BEAM 310
BEAM 320
BEAM 330
BEAM 340
BEAM 350
BEAM 360
BEAM 370
BEAM 380
BEAM 390
BEAM 400
BEAM 410
BEAM 420
BEAM 430
BEAM 440
BEAM 450
BEAM 460
BEAM 470
BEAM 480
BEAM 490
BEAM 500
BEAM 510
BEAM 520
BEAM 530
BEAM 540
BEAM 550
BEAM 560
BEAM 570
BEAM 580

```

```

IMEM=0
ITIET=0
IGRPT=0
MAXM=0
IM=0
NCM=0
NLS=0
IBA=0
NLSR=0

```

# INITIALIZE ARRAYS

```

DO 130 MEM=1,NMD
BMEM(MEM)=0.E0
BPP(MEM)=0.E0
D(MEM)=0.E0
DP(MEM)=0.E0
OPP(MEM)=0.E0
DWF(MEM)=0.E0
TFWF(MEM)=0.E0
TWTF(MEM)=0.E0
BWF(MEM)=0.E0
XL(MEM)=0.E0
EFLM(MEM)=0.E0
HMEM(MEM)=0.E0
HTOP(MEM)=0.E0
HTWF(MEM)=0.E0
XBEGM(MEM)=0.E0
YLDS(MEM)=0.E0

```



BEAM 530  
 BEAM 600  
 BEAM 610  
 BEAM 620  
 BEAM 630  
 BEAM 640  
 BEAM 650  
 BEAM 660  
 BEAM 670  
 BEAM 680  
 BEAM 690  
 BEAM 700  
 BEAM 710  
 BEAM 720  
 BEAM 730  
 BEAM 740  
 BEAM 750  
 BEAM 760  
 BEAM 770  
 BEAM 780  
 BEAM 790  
 BEAM 800  
 BEAM 810  
 BEAM 820  
 BEAM 830  
 BEAM 840  
 BEAM 850  
 BEAM 860  
 BEAM 870  
 BEAM 880

120 IP(MEM)=0  
 IQ(MEM)=0  
 MTIES(MEM)=0  
 MSHEAR(MEM)=0  
 MCODE(MEM)=0  
 MATR(MEM)=0  
 MATW(MEM)=0  
 MSTAT(MEM)=0  
 MTYPE(MEM)=0  
 NTIES(MEM)=0  
 NGRP(MEM)=0  
 DO 120 I=1,6  
 NSPAC(I, MEM)=0  
 ATIES(I, MEM)=0.E0  
 POP(I, MEM)=0.E0  
 PDF(I, MEM)=0.E0  
 STIES(I, MEM)=0.E0  
 XBEGS(I, MEM)=0.E0  
 DO 130 IGRP=1,10  
 AGRP(IGRP, MEM)=0.E0  
 EFFL(IGRP, MEM)=0.E0  
 XBEG(IGRP, MEM)=0.E0  
 YBAR(IGRP, MEM)=0.E0  
 MBAR(IGRP, MEM)=0  
 DO 140 I=1,NLD  
 IPL(I)=0  
 IQL(I)=0  
 DO 140 J=1,5  
 SPRING(J, I)=0.E0  
 C

```

C      READ A DATA CARD.
C
150    FORMAT (20A4)
      READ (NCRD,150) DHEAD
160    FORMAT (1H0,20A4,/)
      CALL PAGE
      WRITE (NPRT,160) DHEAD
      ICARD = 1
170    FORMAT (A4,1X,3I5,4A1,I1,A4,1X,5E10.0)
180    READ (NCRD,170) J1,I1,I2,I3,J2,J3,J4,J5,I4,J6,R1,R2,R3,R4,R5
      ICARD=ICARD+1
C
C      TEST FOR TYPE OF DATA BY INVESTIGATING J1.
C      CALL FORK (J1,IBRNCH)
C
C      CHECK FOR MATERIAL NAME.
      IF (IBRNCH.EQ.1) GO TO 200
      IF (IBRNCH.EQ.9) GO TO 840
      IF (IBRNCH.EQ.7.OR.IBRNCH.EQ.8) GO TO 200
      CALL MATY (J5,MATN)
      IF (MATN.NE.0) GO TO 200
190    FORMAT (1H,12H***MATERIAL ,A4,10H FOR CARD ,A4,12H OF ELEMENT ,I3BEAM1100
1,1H-,I3,48H IS NOT IN THE MATERIAL DATA BLOCK (BEAM).*** )
      LINE=LINE+1
      IF (LINE.GT.NL) CALL PAGE
      IACT=I2
      ISHEAR=I3
      IF (I1.EQ.0) IACT=IP(IMEM)
      IF (I1.EQ.0) ISHEAR=IQ(IMEM)
      PRINT 190, J6,J1,IACT,ISHEAR

```

BEAM 890  
 BEAM 900  
 BEAM 910  
 BEAM 920  
 BEAM 930  
 BEAM 940  
 BEAM 950  
 BEAM 960  
 BEAM 970  
 BEAM 980  
 BEAM 990  
 BEAM1000  
 BEAM1010  
 BEAM1020  
 BEAM1030  
 BEAM1040  
 BEAM1050  
 BEAM1060  
 BEAM1070  
 BEAM1080  
 BEAM1090  
 BEAM1100  
 BEAM1110  
 BEAM1120  
 BEAM1130  
 BEAM1140  
 BEAM1150  
 BEAM1160  
 BEAM1170  
 BEAM1180



```

240      PRINT 230, I2, I3
        IF (I2.LE.NJ.AND.I3.LE.NJ) GO TO 260
        IF (LINE.GT.NL) CALL PAGE
        IERR=IERR+1
        LINE=LINE+1
        ISK=1
250      FORMAT (1H, 11H***ELEMENT , I3, 1H~, I3, 56H HAS A JOINT WHICH IS NOT
        1IN JOINT DATA BLOCK (BEAM).*** )
        PRINT 250, I2, I3
260      IF (I2.NE.I3) GO TO 280
        IF (LINE.GT.NL) CALL PAGE
        IERR=IERR+1
        LINE=LINE+1
        ISK=1
270      FORMAT (1H, 11H***ELEMENT , I3, 1H~, I3, 46H BEGINS AND ENDS AT THE S
        1ME JOINT (BEAM).*** )
        PRINT 270, I2, I3
C
C      CHECK FOR VALID ELEMENT NUMBER.
280      IF (IM.LE.NMD) GO TO 300
        IF (LINE.GT.NL) CALL PAGE
        IERR=IERR+1
        LINE=LINE+1
290      FORMAT (1H, 11H***ELEMENT , I3, 1H~, I3, 42H REQUIRES EXCEEDING ARRAY
        1SIZE (BEAM).*** )
        PRINT 290, I2, I3
C
C      IF NO NODAL POINT ERRORS, CALCULATE GROSS AND EFFECTIVE LENGTHS.
C
300      IF (ISK.EQ.1) GO TO 330

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```

BEAM1490
BEAM1500
BEAM1510
BEAM1520
BEAM1530
BEAM1540
BEAM1550
BEAM1560
BEAM1570
BEAM1580
BEAM1590
BEAM1600
BEAM1610
BEAM1620
BEAM1630
BEAM1640
BEAM1650
BEAM1660
BEAM1670
BEAM1680
BEAM1690
BEAM1700
BEAM1710
BEAM1720
BEAM1730
BEAM1740
BEAM1750
BEAM1760
BEAM1770
BEAM1780

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AD-A038 317

VIRGINIA POLYTECHNIC INST AND STATE UNIV BLACKSBURG --ETC F/6 13/13  
RELIABILITY STUDY OF SINGER. VOLUME II. USER'S MANUAL.(U)

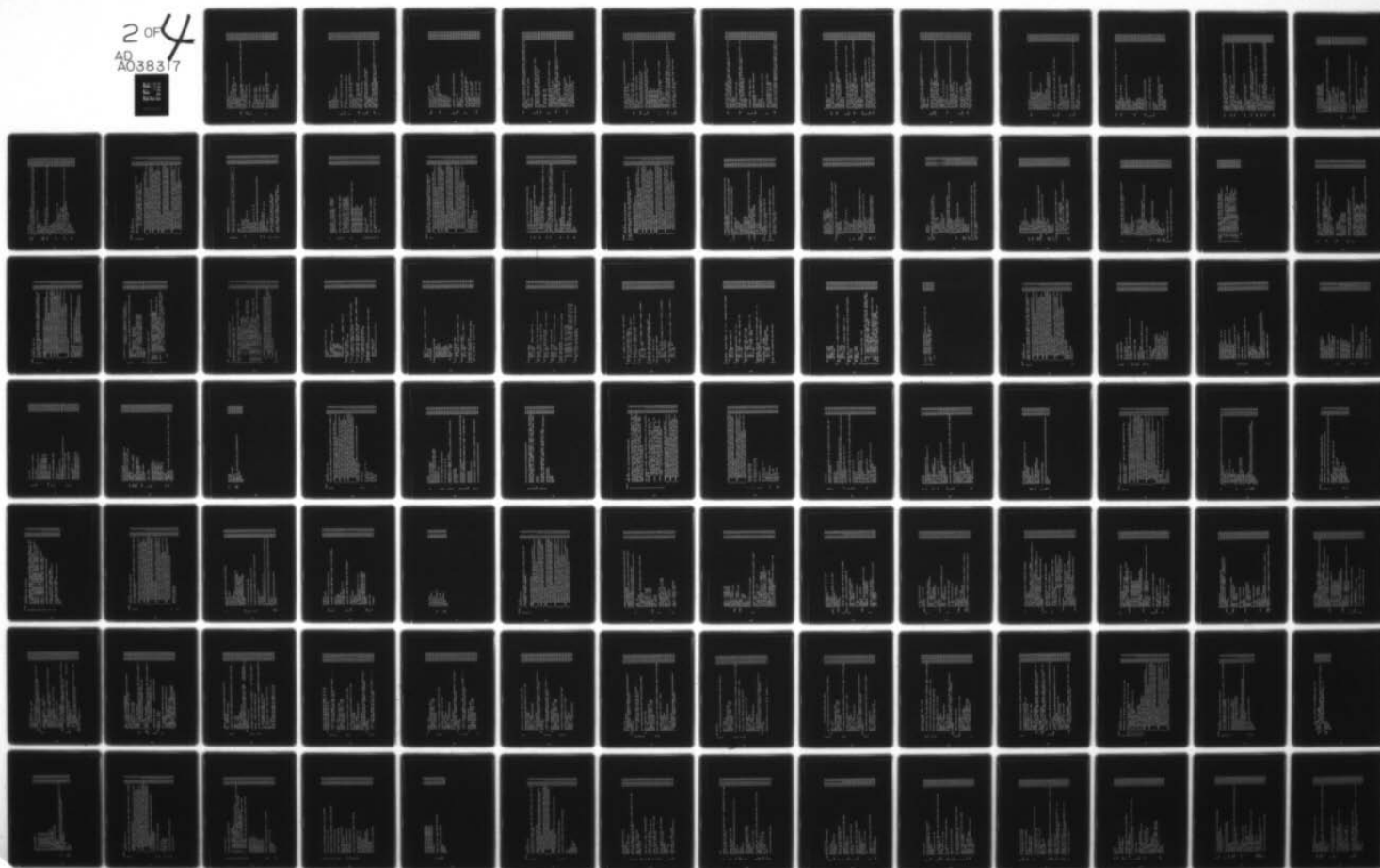
JAN 77 A E SOMERS, S M HOLZER, J C BRADSHAW F29601-75-C-0050

AFWL-TR-76-192-VOL-2

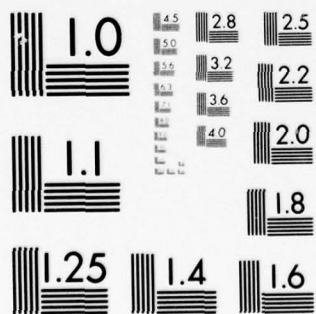
NL

UNCLASSIFIED

2 OF 4  
AD  
A038317



OF 4  
38317



MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

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320      GROS=L=SQRT((X(I2)-X(I3))**2+(Y(I2)-Y(I3))**2)
      XL(IM)=GROS
      EFLM(IM)=XL(IM)
      IF (IZZ.EQ.2) GO TO 330
      IF ((R4+R5).LE.GROS) GO TO 330
      IF (LINE.GT.NL) CALL PAGE
      IERR=IERR+1
      LINE=LINE+1
      FORMAT (1H,11H**ELEMENT ,I3,1H-,I3,52H HAS LONGER JOINT SPANS TH
1AN ITS LENGTH (BEAM).*** )
      PRINT 320, I2,I3
      IF (IM.GT.MAXM) MAXM=IM
330      INTERPRET ALPHAMERIC DATA
      C
      C
      C
      IACT=2
      IF (J2.EQ.ID1) IACT=1
      IF (J2.EQ.ID2) IACT=3
      ISHEAR=0
      IF (J3.EQ.JD2) ISHEAR=1
      IBOND=0
      IF (J4.EQ.JD1) IBOND=1
      C
      C
      ASSIGN ELEMENT PARAMETERS TO ARRAYS
      IF (IM.GT.NMD) GO TO 180
      IP(IM)=I2
      IQ(IM)=I3
      MSTAT(IM)=IACT
      MSHEAR(IM)=ISHEAR
      IF (IZZ.EQ.2) GO TO 720
      BEAM1790
      BEAM1800
      BEAM1810
      BEAM1820
      BEAM1830
      BEAM1840
      BEAM1850
      BEAM1860
      BEAM1870
      BEAM1880
      BEAM1890
      BEAM1900
      BEAM1910
      BEAM1920
      BEAM1930
      BEAM1940
      BEAM1950
      BEAM1960
      BEAM1970
      BEAM1980
      BEAM1990
      BEAM2000
      BEAM2010
      BEAM2020
      BEAM2030
      BEAM2040
      BEAM2050
      BEAM2060
      BEAM2070
      BEAM2080

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      HTOP(IM) = R1
      D(IM)=R2
      DP(IM)=R3
      XBEGM(IM)=R4
      EFLM(IM)=XL(IM)-R4-R5
      GO TO 180

C      INTERPRET CONCRETE PARAMETER CARD
C
C      IM2=IM
C      IF (IM.NE.I1.AND.I1.NE.0) IM2=I1
C
C      CHECK FOR ARRAY SPACE AVAILABILITY
C      IF (IM2.LE.NMD) GO TO 360
      IERR=IERR+1
      LINE=LINE+1
C
C      IF (LINE.GT.NL) CALL PAGE
      FORMAT (1H,11H***ELEMENT ,I3,1H-,I3,44H REQUIRES EXCEEDING ARRAY
      1SIZE (BEAM).*** )
      PRINT 350, IP(IM2),IQ(IM2)
C
C      COMPARE CONFINED AND OVERALL DIMENSIONS.
C      IF (R1.GE.R3.AND.R2.GE.R4) GO TO 380
      IREC=IREC+1
      LINE=LINE+1
C
C      IF (LINE.GT.NL) CALL PAGE
      FORMAT (1H,29H***CAGE DIMENSIONS OF ELEMENT,I3,1H-,I3,50H EXCEED
      1GROSS CROSS SECTION DIMENSIONS (BEAM).*** )
      PRINT 370, IP(IM2),IQ(IM2)
C

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```

BEAM2090
BEAM2100
BEAM2110
BEAM2120
BEAM2130
BEAM2140
BEAM2150
BEAM2160
BEAM2170
BEAM2180
BEAM2190
BEAM2200
BEAM2210
BEAM2220
BEAM2230
BEAM2240
BEAM2250
BEAM2260
BEAM2270
BEAM2280
BEAM2290
BEAM2300
BEAM2310
BEAM2320
BEAM2330
BEAM2340
BEAM2350
BEAM2360
BEAM2370
BEAM2380

```



BEAM2390  
BEAM2400  
BEAM2410  
BEAM2420  
BEAM2430  
BEAM2440  
BEAM2450  
BEAM2460  
BEAM2470  
BEAM2480  
BEAM2490  
BEAM2500  
BEAM2510  
BEAM2520  
BEAM2530  
BEAM2540  
BEAM2550  
BEAM2560  
BEAM2570  
BEAM2580  
BEAM2590  
BEAM2600  
BEAM2610  
BEAM2620  
BEAM2630  
BEAM2640  
BEAM2650  
BEAM2660  
BEAM2670  
BEAM2680

```

C      ASSIGN DATA TO ARRAYS.
380    CALL MATY (J1,M1)
      IF (M1.NE.0) GO TO 390
      LINE=LINE+1
      IF (LINE.GT.NL) CALL PAGE
      PRINT 190, J1,J1,IP(IM2),IQ(IM2)
      MATR(IM2)=MATN
      MCODE(IM2)=M1
      HMEM(IM2)=R1
      BMEM(IM2)=R2
      DPP(IM2)=R3
      BPP(IM2)=R4
      GO TO 180

C      INTERPRET LONGITUDINAL REBAR DATA.
C
C      IGRPT=IGRPT+1
C      IMR=IM
C      IGRP=IGRPT
C      IF (IGRPT.NE.I1.AND.I1.NE.0) IGRP=I1

C      CHECK ARRAY SPACE AVAILABILITY
C      IF (IMR.LE.NMD) GO TO 410
      LINE=LINE+1
      IF (LINE.GT.NL) CALL PAGE
      PRINT 350, IP(IM),IQ(IM)
      IERR=IERR+1
      IF (IGRP.LE.10) GO TO 430
      LINE=LINE+1
      IF (LINE.GT.NL) CALL PAGE
410

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420      FORMAT (1H,51H**THE NUMBER OF LONGITUDINAL REINFORCEMENT GROUPS,8EAM2690
1,I3,12H OF ELEMENT ,I3,1H-,I3,40HREQUIRES EXCEEDING ARRAY SIZE (BE3EAM2700
2AM).***)
      PRINT 420, IGRP,IP(IM),IQ(IM)
      ISK=1
      IERR=IERR+1

C
C      CALCULATE MATERIAL NUMBER FOR LONGITUDINAL REBAR
430      IF (IMR.GT.NMD.OR.IGRP.GT.10) GO TO 440
440      IF (IGRP.GT.NGRP(IMR)) NGRP(IMR)=IGRP
      M=0
      N=0
      IF (J2.EQ.JD3) M=1
      IF (J3.EQ.JD3) N=1

C
C      CALCULATE AND CHECK EFFECTIVE LENGTH OF REBAR.
      BLEN=XL(IMR)-R3-R4
      IF (BLEN.GE.0.) GO TO 460
      IF (ISK.EQ.1) GO TO 460
      FORMAT (1H,27H**LONGITUDINAL REBAR GROUP,I3,11H OF ELEMENT,I3,1HBEAM2880
1-,I3,40H IS LONGER THAN THE ELEMENT (BEAM).***)
      IF (LINE.GT.NL) CALL PAGE
      IERR=IERR+1
      LINE=LINE+1
      PRINT 450, IGRP,IP(IM),IQ(IM)
460      IF(R1.GT.0.E0) GO TO 490
      IF (I3.LE.1) GO TO 490
      CALL BARS (I2,I3,R1,DIAM,PERIM)
      IF (ISK.EQ.1) GO TO 500
      IF (IBOND.EQ.0) GO TO 490
      BEAM2690
      BEAM2700
      BEAM2710
      BEAM2720
      BEAM2730
      BEAM2740
      BEAM2750
      BEAM2760
      BEAM2770
      BEAM2780
      BEAM2790
      BEAM2800
      BEAM2810
      BEAM2820
      BEAM2830
      BEAM2840
      BEAM2850
      BEAM2860
      BEAM2870
      BEAM2880
      BEAM2890
      BEAM2900
      BEAM2910
      BEAM2920
      BEAM2930
      BEAM2940
      BEAM2950
      BEAM2960
      BEAM2970
      BEAM2980

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CALL BOND (IGRP,IMR,R2,M,N,DIAM,R3,I3,BRLEN,IN)
IF (IN.NE.0) GO TO 480
IF (IBA.EQ.IMR) GO TO 480
LINE=LINE+1
IF (LINE.GT.NL) CALL PAGE
FORMAT (1H,44H ACI 318-71 BOND CHECK WAS MADE FOR ELEMENT ,I3,1H-BEAM3040
1,I3,1H.)
WRITE (NPRT,470) IP(IMR),IQ(IMR)
IBA=IMR
IF (I3.EQ.20.OR.IBOND.EQ.0) GO TO 490
CALL ENDS(IMR,M,N,R3,R2,BRLEN,DIAM)

C
C
C
490
ASSIGN LONGITUDINAL REBAR INFORMATION TO ARRAYS.
IF (IGRP.GT.10.OR.IMR.GT.NMD) GO TO 500
AGRP(IGRP,IMR)=R1
EFL(IGRP,IMR)=BRLEN
YBAR(IGRP,IMR)=R2
MBAR(IGRP,IMR)=MATN
XBEG(IGRP,IMR)=R3
BDM(IGRP,IMR)=DIAM
CHECK FOR A NEGATIVE EFFECTIVE LENGTH OF REBAR
IF(BRLEN.GT.0.E0) GO TO 500
IERR = IERR + 1
LINE = LINE + 1
PRINT 495, IGRP,IP(IMR),IQ(IMR),BRLEN
FORMAT(1H,28H*** LONGITUDINAL REBAR GROUP ,I3,11H OF ELEMENT,I3,
1 2H -,I3,28H HAS AN EFFECTIVE LENGTH OF ,G14.7,4H ***)

C
C
C
495
CHECK VALIDITY OF LONGITUDINAL REBAR GROUP AREA.
IF (R1.GT.0.E0) GO TO 180
500

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```

BEAM2990
BEAM3000
BEAM3010
BEAM3020
BEAM3030
BEAM3040
BEAM3050
BEAM3060
BEAM3070
BEAM3080
BEAM3090
BEAM3100
BEAM3110
BEAM3120
BEAM3130
BEAM3140
BEAM3150
BEAM3160
BEAM3170
BEAM3180
BEAM3190
BEAM3200
BEAM3210
BEAM3220
BEAM3230
BEAM3240
BEAM3250
BEAM3260
BEAM3270
BEAM3280

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2) PRINT 540, IP(IM), IQ(IM)
   IERR=IERR+1
   LINE=LINE+1
550 IF (ITI.GT.0.AND.ITI.LE.6) GO TO 570
   IF (LINE.GT.NL) CALL PAGE
   ISK=1
560 FORMAT (1H, 11H***ELEMENT, I3, 1H-, I3, 5H HAS, I3, 50H TIE OR STIRRUP
1 GROUPS. SIX ARE ALLOWED (BEAM).***),
PRINT 560, IP(IM), IQ(IM), ITI
   IERR=IERR+1
   LINE=LINE+2
C
C CALCULATE LATERAL GROUP REBAR AREA AND CHECK VALIDITY OF AREA
570 IF (R1.GT.0.E0) GO TO 600
   IF (I2.NE.0.AND.I4.NE.0) GO TO 590
   IF (LINE.GT.NL) CALL PAGE
580 FORMAT (1H, 11H***ELEMENT, I3, 1H-, I3, 62H HAS A LATERAL REINFORCEME
1NT GROUP WITH ZERO AREA (BEAM).***),
PRINT 580, IP(IM), IQ(IM)
   IERR=IERR+1
   LINE=LINE+1
590 CALL 3ARS (I4, I2, R1, DIAM, PERIM)
C
C ASSIGN LATERAL GROUP REBAR INFORMATION TO ARRAYS.
C CALCULATE MATERIAL NUMBER.
600 IF (R4.NE.0.E0.OR.(I2.NE.0.AND.I4.NE.0)) GO TO 620
   IF (LINE.GT.NL) CALL PAGE
610 FORMAT (74H ***INSUFFICIENT INFORMATION PROVIDED TO DETERMINE STIR
1RUP VOLUME OF GROUP, I3, 11H IN ELEMENT, I3, 1H-, I3, /, 67H WHICH IS NEE
BEAM3590
BEAM3600
BEAM3610
BEAM3620
BEAM3630
BEAM3640
BEAM3650
BEAM3660
BEAM3670
BEAM3680
BEAM3690
BEAM3700
BEAM3710
BEAM3720
BEAM3730
BEAM3740
BEAM3750
BEAM3760
BEAM3770
BEAM3780
BEAM3790
BEAM3800
BEAM3810
BEAM3820
BEAM3830
BEAM3840
BEAM3850
BEAM3860
BEAM3870
BEAM3890

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```

20ED IN COMPUTING THE CONFINEMENT COEFFICIENT. (BEAM) ***)
PRINT 610, ITI, IP(IM), IQ(IM)
IERR=IERR+1
ISK=1
LINE=LINE+1

C
C      CALCULATE CONFINEMENT FACTOR.
620 IF (R2.GT.0.E0) GO TO 640
630 FORMAT (23H ***TIE (STIRrup) GROUP, I2, 11H OF ELEMENT, I3, 1H -, I3, 39HBEAM3970
      1 HAS ZERO OR NEGATIVE SPACING. (BEAM) ***)
      IF (LINE.GT.NL) CALL PAGE
      LINE=LINE+1
      IERR=IERR+1
      PRINT 630, ITI, IP(IM), IQ(IM)
      GO TO 650
640 IF (ISK.EQ.1) GO TO 650
      VSTIR=R4
      IF (R4.EQ.0.E0) VSTIR=R1*DPP(IMT)+8PP(IMT)*PI*DIAM*DIAM/2.E0
      ZZA=R2*8PP(IMT)*OPP(IMT)
      IF (ZZA.EQ.0.E0) GO TO 650
      PPP=VSTIR/ZZA
      PDPT=PPP*SQR(8PP(IMT)/R2)

C
C      ASSIGN DATA TO ARRAYS.
650 IF (I3.NE.0) GO TO 670
      LINE=LINE+1
      IF (LINE.GT.NL) CALL PAGE
660 FORMAT (36H **NUMBER OF TIES (STIRrupS) IN GROUP, I2, 11H OF ELEMENT,
      I3, 1H -, I3, 17H IS ZERO. (BEAM) **)
      PRINT 660, ITI, IP(IM), IQ(IM)

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```

BEAM3890
BEAM3900
BEAM3910
BEAM3920
BEAM3930
BEAM3940
BEAM3950
BEAM3960
BEAM3970
BEAM3980
BEAM3990
BEAM4000
BEAM4010
BEAM4020
BEAM4030
BEAM4040
BEAM4050
BEAM4060
BEAM4070
BEAM4080
BEAM4090
BEAM4100
BEAM4110
BEAM4120
BEAM4130
BEAM4140
BEAM4150
BEAM4160
BEAM4170
BEAM4180

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```

670      IREC=IREC+1
      IF (IMT.GT.NMD.OR.ITI.GT.6) GO TO 180
      ATIES(ITI,IMT)=R1
      STIES(ITI,IMT)=R2
      XBEGS(ITI,IMT)=R3
      MTYPE(IMT)=IBRNCH-3
      POP(ITI,IMT)=PDPT
      PDF(ITI,IMT)=PPP*FCFY(MATN)
      NSPAC(ITI,IMT)=I3
      MTIES(IMT)=MATN
      VLDS(IMT)=FCFY(MATN)
      IF (ITI.GT.MTIES(IMT)) MTIES(IMT)=ITI
      IF (MTYPE(IMT).EQ.2) NSPAC(6,IMT)=-1
      GO TO 180

C      INTERPRET AND STORE DATA ON WIDE FLANGE TYPE BEAMS.
C
C      IMW=IM
      IF (IMW.NE.I1.AND.I1.NE.0) IMW=I1
      IF (IMW.LE.NMD) GO TO 690
      LINE=LINE+1
      IF (LINE.GT.NL) CALL PAGE
      PRINT 290, IP(IMW), IQ(IMW)
      IERR=IERR+1

C      CHECK FOR VALIDITY OF DIMENSIONS
C      IF (R5.GT.0.E0.AND.R2.GT.0.E0.AND.R3.GT.0.E0.AND.R4.GT.0.E0) GO TO 690
      1 710
      LINE=LINE+1
      IF (LINE.GT.NL) CALL PAGE

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```

BEAM4190
BEAM4200
BEAM4210
BEAM4220
BEAM4230
BEAM4240
BEAM4250
BEAM4260
BEAM4270
BEAM4280
BEAM4290
BEAM4300
BEAM4310
BEAM4320
BEAM4330
BEAM4340
BEAM4350
BEAM4360
BEAM4370
BEAM4390
BEAM4390
BEAM4400
BEAM4410
BEAM4420
BEAM4430
BEAM4440
BEAM4450
BEAM4460
BEAM4470
BEAM4480

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700	FORMAT (49H **A DIMENSION OF THE STEEL BEAM IS ZERO.(BEAM)**)	BEAM4490
	PRINT 700	BEAM4500
710	IREC=IREC+1	BEAM4510
	IF (IMW.GT.NMD) GO TO 730	BEAM4520
	MTYPE(IMW)=3	BEAM4530
	NCM=NCM+1	BEAM4540
	IF (I2.EQ.0.AND.I3.EQ.0) GO TO 720	BEAM4550
	MTYPE(IMW)=4	BEAM4560
	NAME(9)=I03	BEAM4570
	IZZ=2	BEAM4580
	GO TO 220	BEAM4590
720	CONTINUE	BEAM4600
	OWF(IMW)=R2	BEAM4610
	TFWF(IMW)=R5	BEAM4620
	THWF(IMW)=R3	BEAM4630
	BWF(IMW)=R4	BEAM4640
	HTWF(IMW)=R1	BEAM4650
730	IF (IMW.LE.NMD) MATW(IMW)=MATN	BEAM4660
	GO TO 180	BEAM4670
C		BEAM4680
C	INTERPRET LEAF SPRING DATA CARD.	BEAM4690
C		BEAM4700
740	NLS=NLS+1	BEAM4710
	ILS=NLS	BEAM4720
	ISK=0	BEAM4730
	IF (ILS.NE.I1.AND.I1.NE.0) ILS=I1	BEAM4740
	IF (ILS.LE.NLD) GO TO 760	BEAM4750
	IF (LINE.GT.NL) CALL PAGE	BEAM4760
	LINE=LINE+1	BEAM4770
	IERR=IERR+1	BEAM4780



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750  FORMAT (1H ,23H**LEAF SPRING ELEMENT ,I3,1H-,I3,52H REQUIRES EXCEBEAM4790
      1EDING *SPRING* ARRAY SIZE (BEAM).*** )
      PRINT 750, I2,I3
      ISK=1
760  IF (I2.NE.0.AND.I3.NE.0) GO TO 780
      IF (LINE.GT.NL) CALL PAGE
770  FORMAT (15H ***LEAF SPRING,I3,1H-,I3,38H HAS AN UNSPECIFIED JOINT
      1(BEAM).*** )
      PRINT 770, I2,I3
      LINE=LINE+1
      IERR=IERR+1
      ISK=1
780  IF (I2.LE.NJ.AND.I3.LE.NJ) GO TO 800
      IF (LINE.GT.NL) CALL PAGE
      LINE=LINE+1
      IERR=IERR+1
790  FORMAT (15H ***LEAF SPRING,I3,1H-,I3,65H HAS A NODE WHICH WAS NOT
      1DESCRIBED BY NODAL POINT DATA.(BEAM)*** )
      PRINT 790, I2,I3
800  IF (R1.LT.0.E0.OR.R3.LT.0.E0.OR.R4.LT.0.E0) GO TO 810
      DET=R1*R3-R2*R2
      IF (DET.GE.0.E0) GO TO 830
      IREC=IREC+1
810  IF (LINE.GT.NL) CALL PAGE
820  FORMAT (1H ,23H**LEAF SPRING ELEMENT ,I3,1H-,I3,79H HAS AN UNACCEBEAM5030
      1PTABLE FLEXIBILITY MATRIX. IT IS NOT POSITIVE DEFINITE (BEAM).*** )BEAM5040
      IERR=IERR+1
      PRINT 820, I2,I3
      LINE=LINE+1
830  IF (ISK.EQ.1) GO TO 180

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IF (R1.EQ.0.E0) NLSR=NLSR+1
IF (R3.EQ.0.E0) NLSR=NLSR+1
IF (R4.EQ.0.E0) NLSR=NLSR+1
IF (R4.EQ.0.E0) R4=TINY*1.E04
IPL(ILS)=I2
IQL(ILS)=I3
C INVERT FLEXIBILITY MATRIX TO OBTAIN STIFFNESS MATRIX.
SPRING(4,ILS)=1.E0/R4
SPRING(5,ILS)=R5
IF (DET.GT.0.E0) GO TO 834
SPRING(1,ILS)=1.E-04/TINY
SPRING(2,ILS)=0.E0
SPRING(3,ILS)=1.E-04/TINY
GO TO 180
SPRING(1,ILS)=R3/DET
SPRING(2,ILS)=-R2/DET
SPRING(3,ILS)=R1/DET
GO TO 180
834
C
C IF END OF DATA, SET NM EQUAL TO THE MAXIMUM COUNTER VALUE
C
NM=IMEM
840
C
C CONDUCT ADDITIONAL CHECKS ON NATURE OF INPUT DATA.
DO 880 I=1,NM
NGP=NGRP(I)
IF (NGP.EQ.0) GO TO 880
DO 870 J=1,NGP
IF (YBAR(J,I).GT.FTOP(I)) GO TO 850
IF (YBAR(J,I).LT.(HTOP(I)-HMEM(I))) GO TO 850

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```

BEAM5090
BEAM5100
BEAM5110
BEAM5120
BEAM5130
BEAM5140
BEAM5150
BEAM5160
BEAM5170
BEAM5180
BEAM5190
BEAM5200
BEAM5210
BEAM5220
BEAM5230
BEAM5240
BEAM5250
BEAM5260
BEAM5270
BEAM5280
BEAM5290
BEAM5300
BEAM5310
BEAM5320
BEAM5330
BEAM5340
BEAM5350
BEAM5360
BEAM5370
BEAM5380

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850	GO TO 870	BEAM5390
860	IF (LINE.GT.NL) CALL PAGE	BEAM5400
	FORMAT (23H ***REINFORCEMENT GROUP,I3,12H OF ELEMENT ,I3,1H-,I3,68BEAM5410	
	1H IS NOT CONTAINED IN THE CONCRETE PORTION OF THE ELEMENT (BEAM).*BEAM5420	
	2** )	BEAM5430
	PRINT 860, J,IP(I),IQ(I)	BEAM5440
	IERR=IERR+1	BEAM5450
	LINE=LINE+1	BEAM5460
870	CONTINUE	BEAM5470
880	CONTINUE	BEAM5480
	IF (MAXM.EQ.NM) GO TO 900	BEAM5490
890	FORMAT (62H ***ELEMENTS WERE NOT INPUT WITH CONSECUTIVE NUMBERS.(9BEAM5500	
	1EAM)***)	BEAM5510
	PRINT 890	BEAM5520
	IERR=IERR+1	BEAM5530
	LINE=LINE+1	BEAM5540
900	DO 920 I=1,NM	BEAM5550
	IF (EFLM(I).EQ.0.E0) GO TO 920	BEAM5560
	RATIO=HMEM(I)/EFLM(I)	BEAM5570
	IF (RATIO.LT..4) GO TO 920	BEAM5580
	IF (LINE.GT.NL) CALL PAGE	BEAM5590
910	FORMAT (48H **USING CRITERION OF 10.7, ACI 318-71, ELEMENT ,I3,1H-8BEAM5600	
	1,I3,24H IS A DEEP BEAM(BEAM).**)	BEAM5610
	PRINT 910, IP(I),IQ(I)	BEAM5620
	LINE=LINE+1	BEAM5630
920	CONTINUE	BEAM5640
	RETURN	BEAM5650
	END	BEAM5660

```

C800Y 0 10
SUBROUTINE BODY
C
C THIS SUBROUTINE CALCULATES BODY FORCES AND MEMBER MASSES
C FROM MEMBER WEIGHTS AND LUMPS THEM AT THE JOINTS.
C L=0, DENSITY OF MEMBER EQUALS ZERO.
C L=1, DATA INCLUDES CALCULATED MEMBER MASSES.
C
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATH(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),
1 SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),DIS(3,50),ERJF(3,50),
1 ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
1 XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CE,DHEAD(20),DT,EPS,HEAD(20),
1 PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
INTEGER HEAD,DHEAD
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLT,IPRINT,
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,
2 NCRO,NDF,NDFD,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLO,
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,
4 NTIMES,NVEL,IINITO
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BOM(10,45),
1 BWF(45),D(45),DP(45),OPP(45),OWF(45),EFFL(10,45),EFLM(45),
2 HMEM(45),HTOP(45),HTWF(45),POP(7,45),SPRING(5,20),STIES(7,45),
3 TFWF(45),TWWF(45),UDM(45),URM(45),XBEG(10,45),
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),
5 YFIBR(11,45),YLOS(45),XOM(45),PDF(7,45),DISM(45)
BODY 0
BODY 10
BODY 20
BODY 30
BODY 40
BODY 50
BODY 60
BODY 70
BODY 80
BODY 90
BODY 100
BODY 110
BODY 120
BODY 130
BODY 140
BODY 150
BODY 160
BODY 170
BODY 180
BODY 190
BODY 200
BODY 210
BODY 220
BODY 230
BODY 240
BODY 250
BODY 260
BODY 270
BODY 280

```







```

CBOND      0 10
SUBROUTINE BOND (IGRP,IMR,ROIM1,M,N,DIAM,XOIM,L,ROIM2,IN)
C          SUBROUTINE TO CHECK BOND REQUIREMENTS USING ACI 310-71.
C
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1  MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),BOND 0
2  MTYPE(45),NGRF(45),NSPAC(6,45),NTIES(45)BOND 10
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),BOND 20
1  SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)BOND 30
COMMON/LEADBK/AVDM,AVGL,CA,C8,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),BOND 40
1  PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB 50
INTEGER HEAD,DHEADBOND 60
COMMON/MAINBK/IANAL,ICUFV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,BOND 70
1  IREG,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,BOND 80
2  NCRO,NDF,NDFD,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,BOND 90
3  NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,BOND 100
4  NTIMES,NVEL,IINITOBOND 110
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BOM(10,45),BOND 120
1  BWF(45),D(45),DP(45),DPP(45),DWF(45),EFFL(10,45),EFLM(45),BOND 130
2  HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),BOND 140
3  TFWF(45),TWWF(45),UOM(45),URM(45),XBEG(10,45),BOND 150
4  XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),BOND 160
5  YFIBR(11,45),YLDS(45),XDM(45),PDF(7,45),DISM(45)BOND 170
IN=0BOND 180
IF ((L.EQ.20).OR.(M.EQ.1.AND.N.EQ.1)) GO TO 80BOND 190
MC=MCODE(IMR)BOND 200
MS=MBAR(IGRP,IMR)BOND 210
IF (MS.EQ.0.OR.MC.EQ.0) GO TO 80BOND 220
IF (L.LE.10) GO TO 20BOND 230
IF (L.EQ.11) GO TO 10BOND 240
BOND 250
BOND 260
BOND 270
BOND 280

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10      IF (L.EQ.12) DL=.11E0*FCFY(MS)/SQRT(FCFY(MC))
      GO TO 30
      DL=.085E0*FCFY(MS)/SQRT(FCFY(MC))
20      GO TO 30
      DL=.01E0*(DIAM*DIAM)*PI*FCFY(MS)/SQRT(FCFY(MC))
      TEMP=.0004E0*DIAM*FCFY(MS)
      IF (DL.LE.TEMP) DL=TEMP
30      IF (DL.LE.12.E0) DL=12.E0
      IF (RDIM1.GE.0.E0) DL=1.4E0*DL
      IF ((M.EQ.1).AND.(XDIM.LE.XBEGH(IMR)).AND.(DL.GE.RDIM2)) GO TO 40
      GO TO 60
40      LINE=LINE+1
      IF (LINE.GT.NL) CALL PAGE
50      FORMAT(27H **LONGITUDINAL REBAR GROUP,I3,12H OF ELEMENT ,I3,1H-,I3BOND 420
      1,47H HAS INSUFFICIENT DEVELOPMENT LENGTH FROM JOINT,I4,9H(BOND) .**BOND 430
      2)
      PRINT 50, IGRP,IP(IMR),IQ(IMR),IP(IMR)
      IREC=IREC+1
      IN=1
60      XEN=XDIM+RDIM2
      XCOMP=XBEGH(IMR)+EFLM(IMR)
      IF ((N.EQ.1).AND.(XEN.GE.XCOMP).AND.(DL.GE.RDIM2)) GO TO 70
      GO TO 80
70      LINE=LINE+1
      IF (LINE.GT.NL) CALL PAGE
      WRITE(NPRT,50) IGRP,IP(IMR),IQ(IMR),IQ(IMR)
      IN=1
80      RETURN
      END

```



```

CCOEN      0 10
C          SUBROUTINE COEN(M,UR,UD,IFLAG)
C          C THIS SUBROUTINE CALCULATES THE CONTRIBUTION OF CONFINED AND
C          C UNCONFINED CONCRETE TO THE TOTAL MEMBER ENERGY.
C
COMMON DATA(10000),KDATA(500)
COMMON/CONBK/COAREA(4,45),SIGMA(5,45)
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),
1 SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),DIS(3,50),ERJF(3,50),
1 ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
2 XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)
COMMON/LEAD8K/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1 PI,REF,REH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
INTEGER HEAD,DHEAD
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLT,IPRINT,COEN 180
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCH,COEN 190
2 NCRD,NDF,NDFD,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,COEN 200
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRI,NSAVE,NTAB,NTAPE,COEN 210
4 NTIMES,NVEL,IINITO
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BDM(10,45),COEN 220
1 BWF(45),D(45),DP(45),DPP(45),DWF(45),EFL(10,45),EFLM(45),COEN 230
2 HMEM(45),HTOP(45),HTWF(45),POP(7,45),SPRING(5,20),STIES(7,45),COEN 240
3 TFWF(45),TWWF(45),UDM(45),URM(45),X8EG(10,45),COEN 250
4 XBEGM(45),X8EGS(6,45),XL(45),XPI(5,45),Y3AR(10,45),YGP(7,45),COEN 260
5 YFIBR(11,45),YLDS(45),XDM(45),PDF(7,45),DISM(45)
COEN 270
COEN 280

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COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB,
1  LTABI,NMAX,NMAXI
COMMON/STRNBK/SRP(4),SRQ(4),UX,UY,UZ,XLEN,AREA,ZZI,IMAT
C
DIMENSION GPS(7,3),URMP(7,3),UDMP(7,3),GAUSS(3)
C INITIALIZE
CON = COAREA(1,M)
ISTAT=MSTAT(M)
MTN = MATR(M)
NG=NGRP(M)
NT=NTIES(M)
GAUSS(1)=5.E0/9.E0
GAUSS(2)=8.E0/9.E0
GAUSS(3)=GAUSS(1)
C RETRIEVE BEGINNING (ZERO) INDEXES FOR STRAIN AND STRESS HISTORIES.
KRAIN=KOATA(LPI+M)+5*NG-1
KRESS=KOATA(LPSI+M)+40*NG-1
C DETERMINE STRAINS AT GAUSS POINTS
DO 20 I=1,7
DO 20 J=1,3
CALL STRN(M,XPI(J,M),YGP(I,M),GPS(I,J))
IF (ABS(GPS(I,J)).LT.TINY) GPS(I,J) = SIGN(TINY,GPS(I,J))
20 CONTINUE
C IF NO STIRRUPS GO TO UNCONFINED SECTION.
IF(NT.EQ.0) GO TO 190
C
C CALCULATE ENERGIES FOR CONFINED CONCRETE SECTION.
C
C ESTABLISH POINTS 5 AND 6 OF STRESS-STRAIN CURVE.
STS(5,MTN) = SIGMA(1,M)
COEN 290
COEN 300
COEN 310
COEN 320
COEN 330
COEN 340
COEN 350
COEN 360
COEN 370
COEN 380
COEN 390
COEN 400
COEN 410
COEN 420
COEN 430
COEN 440
COEN 450
COEN 460
COEN 470
COEN 480
COEN 490
COEN 500
COEN 510
COEN 520
COEN 530
COEN 540
COEN 550
COEN 560
COEN 570
COEN 580

```

```

70 STN(5,MTN) = SIGMA(2,M)
80 STN(6,MTN) = SIGMA(3,M)
90 SLOPE(4,MTN) = SIGMA(4,M)
100 SLOPE(5,MTN) = SIGMA(5,P)
110 EPSU(MTN) = STN(4,MTN)
120 IF(STS(5,MTN).LT.STS(4,MTN)) EPSU(MTN) = STN(5,MTN)
130
140 C EVALUATE STRESSES AND ENERGY DENSITIES AT GAUSS POINTS.
150 KR=KRAIN+31
160 KS=KRESS+248
170 DO 150 I=1,3
180 K=I+2
190 DO 140 J=1,3
200 IF(ISTAT.EQ.3) GO TO 80
210 DO 70 L=1,5
220 S(L)=0.E0
230 GO TO 100
240 S(9)=DATA(KR+J)
250 LS=KS+8*(J-1)
260 DO 90 L=1,8
270 S(L)=DATA(LS+L)
280 CALL CRET(MTN,GPS(K,J),URMP(K,J),UDMP(K,J))
290 C UPDATE IF IFLAG=3
300 IF(IFLAG.NE.3.OR.ISTAT.NE.3) GO TO 120
310 DATA(KR+J)=S(9)
320 DO 110 L=1,8
330 DATA(LS+L)=S(L)
340 UR=UR+CON*GAUSS(I)*GAUSS(J)*URMP(K,J)
350 UD=UD+CON*GAUSS(I)*GAUSS(J)*UDMP(K,J)
360 CONTINUE
370
380 COEN 590
390 COEN 600
400 COEN 610
410 COEN 620
420 COEN 630
430 COEN 640
440 COEN 650
450 COEN 660
460 COEN 670
470 COEN 690
480 COEN 690
490 COEN 700
500 COEN 710
510 COEN 720
520 COEN 730
530 COEN 740
540 COEN 750
550 COEN 760
560 COEN 770
570 COEN 780
580 COEN 790
590 COEN 800
600 COEN 810
610 COEN 820
620 COEN 830
630 COEN 840
640 COEN 850
650 COEN 860
660 COEN 870
670 COEN 880

```

```

150 KR=KR+3
    KS=KS+24
C
C STORE MEMBER END STATE DATA IF IFLAG=3.
190 IF(IFLAG.NE.3.OR.ISTAT.NE.3) GO TO 200
    KR = KRAIN + 40
    KS = KRESS + 320
    XLOC=0.E0
    DO 180 I=1,2
    IF(I.EQ.2) XLOC=XLEN
    DO 170 KK=2,10
    K=KK-1
    CALL STRN(M,XLOC,YFIBR(KK,M),STRAIN)
    IF (ABS(STRAIN).LT.TINY) STRAIN = SIGN(TINY,STRAIN)
    S(9)=DATA(KR+K)
    LS=KS+8*(K-1)
    DO 155 L=1,8
    S(L)=DATA(LS+L)
    CALL CRET(MTN,STRAIN,URE,UDE)
    DATA(KR+K)=S(9)
    DO 160 L=1,8
    DATA(LS+L)=S(L)
    CONTINUE
    KR=KR+9
    KS=KS+72
180
C
C CALCULATE ENERGIES FOR UNCONFINED CONCRETE PORTION.
C
C EVALUATE STRESSES AND ENERGY DENSITIES AT GAUSS POINTS.
200 KR = KRAIN

```

```

COEN 890
COEN 900
COEN 910
COEN 920
COEN 930
COEN 940
COEN 950
COEN 960
COEN 970
COEN 980
COEN 990
COEN1000
COEN1010
COEN1020
COEN1030
COEN1040
COEN1050
COEN1060
COEN1070
COEN1080
COEN1090
COEN1100
COEN1110
COEN1120
COEN1130
COEN1140
COEN1150
COEN1160
COEN1170
COEN1180

```



COEN1190  
COEN1200  
COEN1210  
COEN1220  
COEN1230  
COEN1240  
COEN1250  
COEN1260  
COEN1270  
COEN1280  
COEN1290  
COEN1300  
COEN1310  
COEN1320  
COEN1330  
COEN1340  
COEN1350  
COEN1360  
COEN1370  
COEN1380  
COEN1390  
COEN1400  
COEN1410  
COEN1420  
COEN1430  
COEN1440  
COEN1450  
COEN1460  
COEN1470  
COEN1480

```

210      KS=KRESS
      DO 270 I=1,7
      DO 260 J=1,3
      IF (ISTAT.EQ.3) GO TO 220
      DO 210 L=1,9
      S(L)=0.E0
      GO TO 240
220      S(9)=DATA(KR+J)
      LS=KS+8*(J-1)
      DO 230 L=1,8
      S(L)=DATA(LS+L)
230      S(L)=DATA(LS+L)
240      CALL CRET(MCODE(M),GPS(I,J),URMP(I,J),UDMP(I,J))
      C UPDATE IF IFLAG=3.
      IF (IFLAG.NE.3.OR.ISTAT.NE.3) GO TO 260
      DATA(KR+J)=S(9)
      DO 250 L=1,8
      DATA(LS+L)=S(L)
250      DATA(LS+L)=S(L)
260      CONTINUE
      KR=KR+3
270      KS=KS+24
      C
      C OBTAIN ENERGY CONTRIBUTIONS OF COVER AND SIDES.
      DO 300 I=1,7
      IF (I.LE.2) CONST = COAREA(3,M)
      IF (I.GE.6) CONST = COAPEA(4,M)
      IF (I.GE.3.AND.I.LE.5) CONST = COAREA(2,M)*GAUSS(I-2)
      DO 300 J=1,3
      UR = UR + CONST*GAUSS(J)*URMP(I,J)
      UD = UD + CONST*GAUSS(J)*UDMP(I,J)
300      C

```

```

C      UPDATE MEMBER END STATE DATA FOR UNCONFINED CONCRETE.
      IF (IFLAG.NE.3.OR.ISTAT.NE.3) GO TO 360
      KR=KRAIN+21
      KS=KRESS+168
      XLOC=0.E0
      DO 350 I=1,2
      IF (I.EQ.2) XLOC=XLEN
      DO 340 KK=1,5
      K=KK
      IF (KK.EQ.3) K=6
      IF (KK.EQ.4) K=10
      IF (KK.EQ.5) K=11
      CALL STRN(M,XLOC,YFIBR(K,M),STRAIN)
      IF (ABS(STRAIN).LT.TINY) STRAIN = SIGN(TINY,STRAIN)
      S(9)=DATA(KR+KK)
      LS=KS+8*(KK-1)
      DO 325 L=1,8
      S(L)=DATA(LS+L)
      CALL CRET(MCODE(M),STRAIN,URE,UDE)
      DATA(KR+KK)=S(9)
      DO 330 L=1,8
      DATA(LS+L)=S(L)
      CONTINUE
      KR=KR+5
      KS = KS + 40
      RETURN
325
330
340
350
360
C
C ***** GLOSSARY FOR COEN *****
C
C      KR = STRAIN INDEX FOR EACH INTEGRATION SECTION.
COEN1490
COEN1500
COEN1510
COEN1520
COEN1530
COEN1540
COEN1550
COEN1560
COEN1570
COEN1580
COEN1590
COEN1600
COEN1610
COEN1620
COEN1630
COEN1640
COEN1650
COEN1660
COEN1670
COEN1680
COEN1690
COEN1700
COEN1710
COEN1720
COEN1730
COEN1740
COEN1750
COEN1760
COEN1770
COEN1780

```

C KRAIN = ZERO INDEX FOR STRAIN HISTORY STORAGE.  
 C KRESS = ZERO INDEX FOR STRESS HISTORY STORAGE.  
 C KS = STRESS INDEX FOR EACH INTEGRATION SECTION.  
 C M = MEMBER NUMBER.  
 C MTN = MATERIAL NUMBER OF CONFINED CONCRETE.  
 C NG = NUMBER OF LONGITUDINAL STEEL GROUPS IN MEMBER.  
 C NT = NUMBER OF STIRRUP GROUPS IN MEMBER.  
 C UD = DISSIPATIVE ENERGY DENSITY FOR MEMBER.  
 C UDMP = DISSIPATIVE ENERGY DENSITY AT MESH POINTS.  
 C UR = RECOVERABLE ENERGY DENSITY FOR MEMBER.  
 C URMP = RECOVERABLE ENERGY DENSITY AT MESH POINTS.  
 C XLEN = LENGTH OF MEMBER.  
 C  
 END

COEN1790  
 COEN1800  
 COEN1810  
 COEN1820  
 COEN1830  
 COEN1840  
 COEN1850  
 COEN1860  
 COEN1870  
 COEN1880  
 COEN1890  
 COEN1900  
 COEN1910  
 COEN1920

```

C
C      REMOVE CONCRETE AREA DISPLACED BY LONGITUDINAL STEEL.
DO 20 N=1,NG
  NLOC = 1
  IF (YBAR(N,M).GT.YFIBR(2,M)) NLOC = 3
  IF (YBAR(N,M).LT.YFIBR(10,M)) NLOC = 4
  COAREA(NLOC,M) = COAREA(NLOC,M) - AGRP(N,M)*XL(M)/4.E0
  IF (NTIES(M).NE.0) GO TO 30
  COAREA(2,M) = COAREA(2,M) + COAREA(1,M)
  COAREA(1,M) = 0.E0
  GO TO 70
C
C      30
  MTN = MATR(M)
  MTS = MTIES(M)
  FCP = ABS(FCFY(MTN))
  SIGMA(1,M) = STS(5,MTN)
  SIGMA(2,M) = STN(5,MTN)
  SIGMA(3,M) = STN(6,MTN)
C
C      CHECK FOR INTERNALLY GENERATED CURVE.
  IF (STS(5,MTN).NE.0.E0) GO TO 40
C
C      ALTER POINTS 5 AND 6 ON THE STRESS-STRAIN CURVE.
  DSTS = ABS(0.75E0*PDF(7,MTS))
  IF (DSTS.GT.2.E3) DSTS = 2.E+03
  SIGMA(1,M) = STS(4,MTN) - DSTS
  DSTN = ABS(0.17E0*POP(7,MTS))
  IF (DSTN.GT.8.E-3) DSTN = 8.E-03
  SIGMA(2,M) = STN(4,MTN) - DSTN
  S50 = (3.E0-2.E-3*FCP)/(FCP+1.E3) - ABS(0.75E0*POP(7,MTS))
CONC 290
CONC 300
CONC 310
CONC 320
CONC 330
CONC 340
CONC 350
CONC 360
CONC 370
CONC 380
CONC 390
CONC 400
CONC 410
CONC 420
CONC 430
CONC 440
CONC 450
CONC 460
CONC 470
CONC 480
CONC 490
CONC 500
CONC 510
CONC 520
CONC 530
CONC 540
CONC 550
CONC 560
CONC 570
CONC 580

```





```

C      SIGMA(3,M) = SIGMA(2,M) + (SIGMA(1,M)-STS(6,MTN))/
1      (SIGMA(1,M)-0.5E0*FCP) * (S50-SIGMA(2,M))
C
C      CALCULATE SLOPES OF ALTERED SEGMENTS OF STRESS-STRAIN CURVE.
C      CONTINUE
40    CON4 = SIGMA(2,M) - STN(4,MTN)
      CON5 = SIGMA(3,M) - SIGMA(2,M)
      IF(ABS(CON4).LT.EPS) CON4 = SIGN(EPS,CON4)
      IF(ABS(CON5).LT.EPS) CON5 = SIGN(EPS,CON5)
      SIGMA(4,M) = (SIGMA(1,M)-STS(4,MTN))/CON4
      SIGMA(5,M) = (STS(6,MTN)-SIGMA(1,M))/CON5
70    CONTINUE
      RETURN
C
C      ***** GLOSSARY FOR CONC *****
C
C      COAREA = INTEGRATION CONSTANT OF CONCRETE CROSS-SECTION AREA.
C      CON4 = TEMPORARY CONSTANT OF STRESS DIFFERENCE.
C      CON5 = TEMPORARY CONSTANT OF STRESS DIFFERENCE.
C      NLOC = LOCATION OF COAREA (1=CONFINED CONCRETE,2=COVER ON THE
C      SIDES,3=TOP COVER,4=BOTTOM COVER).
C      SIGMA = ALTERED STRESS, STRAINS, AND SLOPES DUE TO STIRRUPS IN EACH
C      MEMBER (1 = STRESS AT POINT 5 - 2,3 = STRAINS AT POINTS 5
C      AND 6 - 4,5 = SLOPES OF SEGMENTS 4 AND 5).
C
C      END

```

```

CONC 590
CONC 600
CONC 610
CONC 620
CONC 630
CONC 640
CONC 650
CONC 660
CONC 670
CONC 680
CONC 690
CONC 700
CONC 710
CONC 720
CONC 730
CONC 740
CONC 750
CONC 760
CONC 770
CONC 780
CONC 790
CONC 800
CONC 810
CONC 820
CONC 830
CONC 840

```

```

CCRET 0 10
C      SUBROUTINE CRET (MATL, RAINX, URC, UDC)
C
C      DEFINITION OF STRESS HISTORY CURVE PARAMETERS
C      TRANSMITTED VIA COMMON ARRAY S(9)
C
C      S(1) = XFAIL = FIBER FAILURE CODE; 0 = NOT RUPTURED, 1 = RUPTURED
C      S(2) = SDIRCD = LOAD DIRECTION CODE
C      0 = LOADING WITH STRAIN LT ULTIMATE
C      1 = UNLOADING WITH STRAIN LT ULTIMATE
C      2 = LOADING WITH STRAIN GT ULTIMATE
C      3 = UNLOADING WITH STRAIN GT ULTIMATE (DROP-ELASTIC)
C      4 = RELOADING WITH STRAIN GT ULTIMATE (DROP-ELASTIC)
C
C      S(3) = RAINM = MAX STRAIN ENCOUNTERED
C      S(4) = RESM = STRESS ASSOCIATED WITH RAINM
C      S(5) = RAINL = STRAIN FROM LAST TIME STEP (LT PLASTIC OFFSET)
C      S(6) = RESL = STRESS ASSOCIATED WITH RAINL
C      S(7) = SSEGM = STRESS-STRAIN CURVE LINE SEGMENT CONTAINING (RAINM, RESM)
C      S(8) = PLAS = EFFECTIVE PLASTIC OFFSET STRAIN
C      S(9) = RAIN = LAST STRAIN
C
C      COMMON/FIBER/DENS(9), EC(9), EPSU(9), ET(9), FCFY(9), G(9), PR(9),
C      $      XFAIL, SDIRCD, RAINM, RESM, RAINL, RESL, SSEGM, PLAS, RAIN,
C      1      SLOPE(8,9), ST(17,6), STN(8,9), STS(8,9), UNLK(9), ICODE(9), NAME(9)
C      COMMON/LEADBK/AVDM, AVGL, CA, CB, CC, CD, CE, DHEAD(20), DT, EPS, HEAD(20),
C      1      PI, PERP, PERZ, SERR, TBEGIN, THALT, TIME, TINK, TINY, TPROB
C      INTEGER HEAD, DHEAD
C
C      INITIALIZE.
C
C

```

```

CRET 0
CRET 10
CRET 20
CRET 30
CRET 40
CRET 50
CRET 60
CRET 70
CRET 80
CRET 90
CRET 100
CRET 110
CRET 120
CRET 130
CRET 140
CRET 150
CRET 160
CRET 170
CRET 180
CRET 190
CRET 200
CRET 210
CRET 220
CRET 230
CRET 240
CRET 250
CRET 260
CRET 270
CRET 280

```

```

IF(XFAIL.GT.0.E0) GO TO 500
J=MATL
N=7
YC = SLOPE(1,J)
IF (SSEGM.LT. 1.E0) SSEGM= 1.E0
SRAINM =RAINM
SRESM = RESM
DIRCD = SDIRCD
SEGM = SSEGM
RESX = RESL
IF(SRAINM.EQ. 0.E0 )SRAINM = STN(1,J)

C DEFINE STRAIN ORIGIN
ZERN = STN(1,J)+ PLAS

C TEST FOR TENSILE STRAIN OR STRAIN GT LAST PLASTIC OFFSET
IF (RAINX.GT. ZERN) GO TO 450

C IF LAST STRAIN AND PRESENT STRAIN ARE EQUAL, COMPUTE ENERGIES.
IF (RAINX.EQ. RAINL) GO TO 300

C TEST FOR UNLOADING OR RELOADING
IF (RAINX.GE.RAINM) GO TO 200

C INCREASING STRAIN
C INCREMENT THRU STRESS-STRAIN CURVE TO LOCATE STRESS
C
IPT= SSEGM +1.1E0
DO 50 I=IPT,N
IF(RAINX.LT. STN(I,J)) GO TO 50

```

```

CRET 290
CRET 300
CRET 310
CRET 320
CRET 330
CRET 340
CRET 350
CRET 360
CRET 370
CRET 380
CRET 390
CRET 400
CRET 410
CRET 420
CRET 430
CRET 440
CRET 450
CRET 460
CRET 470
CRET 480
CRET 490
CRET 500
CRET 510
CRET 520
CRET 530
CRET 540
CRET 550
CRET 560
CRET 570
CRET 580

```



CRET 590  
 CRET 600  
 CRET 610  
 CRET 620  
 CRET 630  
 CRET 640  
 CRET 650  
 CRET 660  
 CRET 670  
 CRET 680  
 CRET 690  
 CRET 700  
 CRET 710  
 CRET 720  
 CRET 730  
 CRET 740  
 CRET 750  
 CRET 760  
 CRET 770  
 CRET 780  
 CRET 790  
 CRET 800  
 CRET 810  
 CRET 820  
 CRET 830  
 CRET 840  
 CRET 850  
 CRET 860  
 CRET 870  
 CRET 880

```

M= I-1
RESX = STS(M,J) + (RAINX - STN(M,J)) * SLOPE(M,J)
SEGM = M
GO TO 60
50 CONTINUE
C STRAIN EXCEEDS RUPTURE
XFAIL =1.E0
RESM=STS(N,J)
RAINM=STN(N,J)
SSEGM=N-1
RESL=0.E0
RAINL=RAINX
SDIRCD=DIRCD
GO TO 500
60 RAINM = RAINX
RESM = RESX
C SET LOAD DIRECTION CODE
DIRCD = 0.E0
IF (RAINX .LT. EPSU(J)-EPS) DIRCD = 2.E0
C CALCULATE PLASTIC OFFSET
PLAS = RAINX - STN(1,J) - RESX/ YC
GO TO 300
C UNLOADING OR RELOADING
C TEST FOR ASCENDING OR DESCENDING BRANCH
200 IF (SDIRCD .GT. 1.E0) GO TO 210
  
```

```

C ASCENDING BRANCH
DIRCD = 1.E0
RESX = RESM - (RAINM - RAINX)* YC
GO TO 300

C DESCENDING BRANCH TEST FOR UNLOADING OR RELOADING
210 DIRCD = 3.E0
IF ( RAINX .LT. RAINL) GO TO 220

C UNLOADING ON DROP-ELASTIC LOOP
RESX = UNLK(J)* YC * (RAINX - PLAS -STN(1,J))
GO TO 300

C RELOADING ON DROP- ELASTIC LOOP
220 DIRCD = 4.E0
RESX = RESM - UNLK(J) * YC *(RAINM -RAINX)
GO TO 300

C ENERGY CALCULATIONS
C CHECK FOR UNLOADING ,RELOADING OR LOOP LOADING
C
300 IF ( SEGM .EQ. 1.E0 ) GO TO 350
IF (DIRCD .EQ. 1.E0 ) GO TO 350
IF( SDIRCD .EQ. 2.E0 .AND. DIRCD .EQ.3.E0) GO TO 360
IF( SDIRCD .EQ. 3.E0.AND. DIRCD .EQ.4.E0) GO TO 370
IF( SDIRCD .GE. 3.E0.AND. DIRCD .EQ.2.E0 ) GO TO 380

C DEFINE PREVIOUS UR FOR ASCENDING ^ DESCENDING BRANCHES
UDC = 0.5E0 *SRESM*SRESM/ YC

```

```

CRET 890
CRET 900
CRET 910
CRET 920
CRET 930
CRET 940
CRET 950
CRET 960
CRET 970
CRET 980
CRET 990
CRET1000
CRET1010
CRET1020
CRET1030
CRET1040
CRET1050
CRET1060
CRET1070
CRET1080
CRET1090
CRET1100
CRET1110
CRET1120
CRET1130
CRET1140
CRET1150
CRET1160
CRET1170
CRET1180

```

```

C
C IF ( SOIRCO .GE. 2.E0 ) UDC = UDC* UNLK(J)
C
C LOADING WITH INCREASING STRAIN
305 URC = 0.5E0 * RESM * RESM/ YC
C IF (DIRCO .GT. 1.E0 ) URC= URC* UNLK(J)
C
C ARE PRESENT A LAST STRAINS ON SAME LINE SEGMENT
C IF (SSEGM .LT. SEGM) GO TO 310
C
C SAME SEGMENT
UDC = UDC + 0.5E0 * ((SRESM + RESX) * ( RAINX - SRAINM))
UDC = UDC - URC
GO TO 400
C
C ACCUMULATE AREA UNDER STRESS-STRAIN CURVE
C LOCATE END OF LINE SEGMENT FOR PREVIOUS LOADING
C
310 IPT = SSEGM +1.1E0
C
C USE NO OF PRESENT SEGMENT
N= SEGM
DO 330 I= IPT,N
UDC = UDC+ 0.5E0* ((SRESM+ STS(I,J)) *(STN(I,J)-SRAINM))
SRESM = STS(I,J)
330 SRAINM = STN(I,J)
C
C ADD IN LAST SEGMENT
UDC= UDC + 0.5E0*(( STS(N,J)+ RESX) * ( RAINX - STN(N,J)))
UDC = UDC -URC
GO TO 400

```

```

CRET1190
CRET1200
CRET1210
CRET1220
CRET1230
CRET1240
CRET1250
CRET1260
CRET1270
CRET1280
CRET1290
CRET1300
CRET1310
CRET1320
CRET1330
CRET1340
CRET1350
CRET1360
CRET1370
CRET1380
CRET1390
CRET1400
CRET1410
CRET1420
CRET1430
CRET1440
CRET1450
CRET1460
CRET1470
CRET1480

```

```

C UNLOADING (ELASTIC RANGE) 0,1 ^ 1,1 LOADING ON FIRST SEGMENT
C
C 350 UDC=0.E0
    URC= 0.5E0* RESX* RESX/ YC
    GO TO 400
C
C UNLOADING ON DROP-ELASTIC 2,3 ^ 3,3
C 360 UDC = 0.E0
    URC = 0.5E0 * RESX * RESX / (UNLK(J)* YC)
    GO TO 400
C
C RELOADING WITHIN LOOP 3,4 ^ 4,4
C 370 HT = (1.E0 - UNLK(J)) * RESM
    URC = RESX - HT
    URC = 0.5E0 * URC * URC / (UNLK(J) * YC)
    UDC = HT * (RAINX - RAINL)
    GO TO 400
C
C RELOADING FROM LOOP BACK ON TO VIRGIN CURVE 3,2 ^ 4,2
C OLD ELASTIC ENERGY
C 380 UDC= 0.5E0 * UNLK(J)*SRESM*SRESM /YC
C
C ADDITIONAL LOOP ENERGY
    HT= (1.E0 - UNLK(J))*SRESM
    UDC = UDC+ HT * (SRAINM - RAINL)
    GO TO 305
C
C SAVE CURVE PARAMETERS FOR NEXT CYCLE
C

```

```

CRET1490
CRET1500
CRET1510
CRET1520
CRET1530
CRET1540
CRET1550
CRET1560
CRET1570
CRET1580
CRET1590
CRET1600
CRET1610
CRET1620
CRET1630
CRET1640
CRET1650
CRET1660
CRET1670
CRET1680
CRET1690
CRET1700
CRET1710
CRET1720
CRET1730
CRET1740
CRET1750
CRET1760
CRET1770
CRET1780

```



```

400 SSEGM = SEGM
    RESL = RESX
    RAINL = RAINX
    SDIRCD = DIRCD
    GO TO 600

C
C SET DIRECTION CODE A STRESS FOR STRAIN GT PLASTIC OFFSET
450 RESL = 0.E0
    RAINL = ZERON
    SDIRCD = 1.E0
    IF ( SRAINM .LT. EPSU(J) ) SDIRCD = 3.E0

C
C RETURN URC A UDC AS ZERO FOR TENSILE STRAIN OR CRUSHED CONCRETE.
500 UDC = 0.E0
    URC = 0.E0

C
C REMEMBER STRAIN
600 RAIN = RAINX
    RETURN

C ***** GLOSSARY FOR CRET *****
C
C DIRCD = LOAD DIRECTION CODE FOR THIS LOAD STEP (SEE SDIRCD ABOVE).
C HT = LENGTH OF VERTICAL SEGMENT OF DROP-ELASTIC UNLOADING CURVE.
C IPT = STRESS-STRAIN CURVE POINT NUMBER.
C J = MATERIAL NUMBER.
C N = NUMBER OF POINTS USED TO DESCRIBE STRESS-STRAIN CURVE.
C RESX = STRESS AT THIS LOAD STEP STRAIN (RAINX).
C SEGM = STRESS-STRAIN CURVE LINE SEGMENT NUMBER.
C SRAINM = MAXIMUM STRAIN OF PREVIOUS LOAD STEP SAVED FOR

```

```

CRET1790
CRET1800
CRET1810
CRET1820
CRET1830
CRET1840
CRET1850
CRET1860
CRET1870
CRET1880
CRET1890
CRET1900
CRET1910
CRET1920
CRET1930
CRET1940
CRET1950
CRET1960
CRET1970
CRET1980
CRET1990
CRET2000
CRET2010
CRET2020
CRET2030
CRET2040
CRET2050
CRET2060
CRET2070
CRET2080

```



```

CCUTS      0 10
C          SUBROUTINE CUTS
C          SUBROUTINE TO INCREASE THE NUMBER OF FINITE ELEMENTS DESCRIBED BY
C          INPUT DATA BY BISECTING ELEMENTS, DRAWN FROM COMMON BLOCKS.
C
COMMON/ELEMENT/ICARD,IP(45),IPL(20),IQ (45),IQL(20),MATR(45),
1  MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2  MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),DIS(3,50),ERJF(3,50),
1  ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
2  XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IOFI(90),IOFII(90)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1  PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,CUTS
1  IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,CUTS
2  NCRO,NDF,NDFD,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJO,NJER,NL,NLO,CUTS
3  NLS,NLSR,NM,NMAS,NMAT,NMATO,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE, CUTS
4  NTIMES,NVEL,IINITD CUTS
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BDM(10,45),CUTS
1  BWF(45),D(45),DP(45),DPP(45),DMF(45),EFFL(10,45),EFLM(45), CUTS
2  HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),CUTS
3  TWF(45),TWFF(45),UOM(45),URM(45),XBEG(10,45), CUTS
4  XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45), CUTS
5  YFIBR(11,45),YLOS(45),XDM(45),PDF(7,45),DISM(45)
INTEGER HEAD, DHEAD
DIMENSION KIND(45)
LDNM= NM
DO 12 IT=1,NM
12  KIND(IT)=0

```

	EP=10.*SQRT(EPS)	CUTS 290
C		CUTS 300
C	JOINT SEARCH LOOP	CUTS 310
C		CUTS 320
	DO 40 I=1,NJ	CUTS 330
	IF(NLS.EQ.0) GO TO 19	CUTS 340
	DO 13 L=1,NLS	CUTS 350
	IF(IPL(L).EQ.I.OR.IQL(L).EQ.I) GO TO 40	CUTS 360
13	CONTINUE	CUTS 370
C		CUTS 380
C	ELEMENT SEARCH LOOP	CUTS 390
C		CUTS 400
19	NM=LDNM	CUTS 410
	DO 20 J=1,NM	CUTS 420
	IF(IP(J).EQ.I.OR.IQ(J).EQ.I) GO TO 40	CUTS 430
20	CONTINUE	CUTS 440
C		CUTS 450
C	NEW JOINT, FIND BISECTED ELEMENT	CUTS 460
C		CUTS 470
	DO 30 J=1,NM	CUTS 480
	I1=IP(J)	CUTS 490
	I2=IQ(J)	CUTS 500
	XLL = AMIN1(X(I1),X(I2))	CUTS 510
	IF(X(I1).LT.XLL) GO TO 30	CUTS 520
	XR=AMAX1(X(I1),X(I2))	CUTS 530
	IF(X(I1).GT.XR) GO TO 30	CUTS 540
	YB = AMIN1(Y(I1),Y(I2))	CUTS 550
	IF(Y(I1)+EP.LT.YB) GO TO 30	CUTS 560
	YT=AMAX1(Y(I1),Y(I2))	CUTS 570
	IF(Y(I1)-EP.GT.YT) GO TO 30	CUTS 580



CUTS 590  
CUTS 600  
CUTS 610  
CUTS 620  
CUTS 630  
CUTS 640  
CUTS 650  
CUTS 660  
CUTS 670  
CUTS 680  
CUTS 690  
CUTS 700  
CUTS 710  
CUTS 720  
CUTS 730  
CUTS 740  
CUTS 750  
CUTS 760  
CUTS 770  
CUTS 780  
CUTS 790  
CUTS 800  
CUTS 810  
CUTS 820  
CUTS 830  
CUTS 840  
CUTS 850  
CUTS 860  
CUTS 870  
CUTS 880

```

XDIF=X(I1)-X(I2)
IF(ABS(XDIF).LE.EP) GO TO 21
YDIF=Y(I1)-Y(I2)
IF(ABS(YDIF).LE.EP) GO TO 21
SLOP=YDIF/XDIF
XDIF=X(I1)-X(I)
IF(ABS(XDIF).LE.EP) GO TO 30
YDIF=Y(I1)-Y(I)
SNEW=YDIF/XDIF
IF(ABS(SLOP-SNEW).GT.EP) GO TO 30

JOINT IS WITHIN ELEMENT J

LDNM=LDNM+1

CHECK FOR NEED FOR EXCEEDING ARRAY SIZE

IF(LDNM.GT.NMD) GO TO 100
  KIND(J)=1
  KIND(LDNM)=1
  IQ(LDNM)=IQ(J)
  IP(LDNM)=I
  IQ(J)=I
  XLEN=XL(J)
  XL(J)=SQRT((X(I1)-X(I))**2+(Y(I1)-Y(I))**2)
  XL(LDNM)=SQRT((X(I2)-X(I))**2+(Y(I2)-Y(I))**2)
  IF(MTYPE(J).EQ.4) GO TO 90

ELEMENTS PARAMETER CARD

```

C  
C  
C  
21  
C  
C  
C

C  
C  
C

```

MSTAT(LDNM)=MSTAT(J)
MSHEAR(LDNM)=MSHEAR(J)
HTOP(LDNM)=HTOP(J)
D(LDNM)=D(J)
DP(LDNM)=DP(J)
R5=XLEN-EFLM(J)-XBEGM(J)
XBEGM(LDNM)=0.E0
EFLM(LDNM)=XL(LDNM)-R5
EFLM(J)=XL(J)-XBEGM(J)

CONCRETE DATA CARD

MCODE(LDNM)=MCODE(J)
MATR(LDNM)=MATR(J)
HMEM(LDNM)=HMEM(J)
BMEM(LDNM)=BMEM(J)
DPP(LDNM)=DPP(J)
BPP(LDNM)=BPP(J)

LONGITUDINAL REINFORCEMENT CARD

ICNT=0
KK=NGRP(J)
DO 200 L=1, KK
XEND=XLEN-EFFL(L,J)+X(I1)
IF(X(I1).LT.XEND) GO TO 80

REINFORCEMENT IS IN ONE SECTION

EFFL(L,J)=X(I1)-XEND

```

C C C

C C C

C C C

CUTS 890  
CUTS 900  
CUTS 910  
CUTS 920  
CUTS 930  
CUTS 940  
CUTS 950  
CUTS 960  
CUTS 970  
CUTS 980  
CUTS 990  
CUTS1000  
CUTS1010  
CUTS1020  
CUTS1030  
CUTS1040  
CUTS1050  
CUTS1060  
CUTS1070  
CUTS1080  
CUTS1090  
CUTS1100  
CUTS1110  
CUTS1120  
CUTS1130  
CUTS1140  
CUTS1150  
CUTS1160  
CUTS1170  
CUTS1180



```

DO 322 II=1,KKK
XB=X(II)+XBEGS(L,J)+II*STIES(L,J)
IF(X9-EP.GT.X(II)) GO TO 323
IF(ABS(X8-X(II)).LT.EP) GO TO 324
CONTINUE
PRINT 325
FORMAT(1H ,11HCUTS BOMBED)
II=II+1
XBEGS(ICNT,LDNM)=XB-X(II)
NSPAC(ICNT,LDNM)=KKK-II
NSPAC(L,J)=II-1
CONTINUE
NTIES(LDNM)=ICNT
GO TO 40

C
C
C
90
WIDE FLANGE

MATW(LDNM)=MATW(J)
MTYPE(LDNM)=MTYPE(J)
HTWF(LDNM)=HTWF(J)
DWF(LDNM)=DWF(J)
TWWF(LDNM)=TWWF(J)
BWF(LDNM)=BWF(J)
TFWF(LDNM)=TFWF(J)
GO TO 40
CONTINUE
PRINT 35,I
FORMAT(1H ,9H***JOINT ,I3,45H IS NOT WITHIN ANY DEFINED ELEMENT
1(CUTS)***
IERR=IERR+1

```



CUTS1790  
CUTS1800  
CUTS1810  
CUTS1820  
CUTS1830  
CUTS1840  
CUTS1850  
CUTS1860  
CUTS1870

```
40  CONTINUE
    NM=LDNM
    CALL ELIN(KIND)
    RETURN
100  PRINT 101
101  FORMAT(1H ,32H***SPACE LIMIT EXCEEDED (CUTS)***)
     IERR=IERR+1
     RETURN
     END
```

```

CDEFO 0 10
SUBROUTINE DEFO (M)
C
C THIS SUBROUTINE COMPUTES THE LOCAL DISTORTION VECTOR OF ELEMENT M
C
COMMON/ELEMET/I CARD, IP(45), IPL(20), IQ(45), IQL(20), MATR(45),
1 MATW(45), MBAR(10,45), MCODE(45), MSHEAR(45), MSTAT(45), MTIES(45),
2 MTYPE(45), NGRF(45), NSPAC(6,45), NTIES(45)
COMMON/JOINTS/ACC(3,50), BET(3,50), DAS(3,50), DIS(3,50), ERJF(3,50),
1 ERJH(3,50), ERJZ(3,50), F(3,50), FOR(3,50), VEL(3,50), X(50),
1 XDJ(3,50), Y(50), DER(3,50), RESENG(3,50), IDFI(90), IDFII(90)
COMMON/LEADBK/AVDM, AVGL, CA, CB, CC, CD, CE, DHEAD(20), DT, EPS, HEAD(20),
1 PI, RERF, RERH, RERZ, SERR, TBEGIN, THALT, TIME, TINK, TINY, TPROB
COMMON/MAINBK/IANAL, ICURV, IERR, IFAIL, IFOR, ILIN, IPAGE, IPLOT, IPRINT,
1 IREG, ISTART, ISTOP, ISTRES, ITAPE, IUNITS, IYLO, LERR, LINE, NACC, NCM,
2 NCRD, NDF, NDFD, NDFJ, NOIS, NDL, NFF, NJOR, NINC, NJ, NJD, NJER, NL, NLD,
3 NLS, NLSR, NM, NMAS, NMAT, NMATD, NMD, NPLOT, NPRT, NSAVE, NTAB, NTAPE,
4 NTIMES, NVEL, IINITD
COMMON/STRNBK/SRP(4), SRQ(4), UX, UY, UZ, XLEN, AREA, ZZI, IMAT
INTEGER HEAD, DHEAD
C
C INITIALIZE
C
IF (M.GT.0) GO TO 6
ILS=IABS(M)
I=IPL(ILS)
J=IQL(ILS)
XLEN=1.E0
GO TO 8
I=IP(M)
6

```

8	J=IQ(M)	DEFO 290
	DX1=(X(J)-X(I))/XLEN	DEFO 300
	DX2=(Y(J)-Y(I))/XLEN	DEFO 310
	DU1=(XDJ(1,J)-XDJ(1,I))*AVGL/XLEN	DEFO 320
	DU2=(XDJ(2,J)-XDJ(2,I))*AVGL/XLEN	DEFO 330
	UI3=XDJ(3,I)	DEFO 340
	DU3=XDJ(3,J)-UI3	DEFO 350
C	TEST FOR GEOMETRIC NONLINEARITY	DEFO 360
C		DEFO 370
C	IF (ILIN.GT.0) GO TO 10	DEFO 380
		DEFO 390
C	GEOMETRICALLY LINEAR (ILIN=0)	DEFO 400
C	DISTORTIONS OF MEMBER M IN GLOBAL COORDINATES (TRANSLATIONAL)	DEFO 410
C		DEFO 420
C	O1=UI3*OX2+DU1	DEFO 430
	O2=-UI3*OX1+DU2	DEFO 440
	GO TO 20	DEFO 450
		DEFO 460
C	GEOMETRICALLY NONLINEAR: UNLIMITED RIGID-BODY MOTIONS, BEAM-COLUMN	DEFO 470
C	DISTORTIONS (ILIN=1)	DEFO 480
C	ROTATIONAL TRANSFORMATION PARAMETERS: GLOBAL TO DEFORMED JOINT I	DEFO 490
C		DEFO 500
C	SI3=SIN(UI3)	DEFO 510
10	CI3=COS(UI3)	DEFO 520
	SI32=SIN(UI3/2.E0)**2	DEFO 530
		DEFO 540
C	DISTORTIONS OF MEMBER M IN JOINT-I COORDINATES (TRANSLATIONAL)	DEFO 550
C		DEFO 560
C	O1=-2.E0*SI32*OX1+SI3*(OX2+DU2)+CI3*DU1	DEFO 570
		DEFO 580

C	D2=-SI3*(OX1+DU1)-2.E0*SI32*OX2+CI3*DU2	DEFO 590
C	ROTATIONAL TRANSFORMATION PARAMETERS: GLOBAL TO LOCAL (UNDEFORMED	DEFO 600
C	MEMBER) CONVENTION FOR MEMBER AXES: 1-AXIS FROM JOINT I TO J, 3-AXIS	DEFO 610
C	WITH SAME SENSE AS 3-GLOBAL, 2-AXIS TO FORM A RIGHT-HANDED TRIAD.	DEFO 620
C		DEFO 630
C		DEFO 640
20	C3=DX1	DEFO 650
	S3=DX2	DEFO 660
C		DEFO 670
C	ROTATIONAL TRANSFORMATION : GLOBAL TO INITIAL LOCAL.	DEFO 680
C	DISTORTIONS ARE PER UNIT LENGTH OF MEMBER M IN LOCAL COORDINATES.	DEFO 690
C		DEFO 700
	UX=C3*O1+S3*O2	DEFO 710
	UY=-S3*O1+C3*O2	DEFO 720
	UZ=DU3	DEFO 730
	RETURN	DEFO 740
	END	DEFO 750



```

CDELT      0  10
SUBROUTINE DELT (SOLN,DELTA,I,OVALUE,ISEQ)
C
C      THIS SUBROUTINE CALCULATES THE DERIVATIVE OF THE POTENTIAL FUNCTION DELT
C      (OVALUE) FOR A SMALL CHANGE (DELTA) IN THE I-TH VARIABLE OF THE
C      SOLUTION ARRAY.  FOR MOST STRUCTURAL MODELS A CHANGE IN A SINGLE
C      DEGREE-OF-FREEDOM CAUSES ONLY A FEW OF THE MANY TERMS CONTRIBUTING DELT
C      TO THE POTENTIAL FUNCTION TO CHANGE IN VALUE.  THE CODING TAKES
C      ADVANTAGE OF THIS BY IDENTIFYING AND THEN EVALUATING ONLY THOSE
C      TERMS AFFECTED BY THE I-TH VARIABLE.
C
C      THE PARAMETER (ISEQ) CONTROLS INITIALIZATION OF THE CALCULATIONS
C      AS FOLLOWS
C      ISEQ=0, IT IS ASSUMED THAT THE SUBROUTINE IS BEING CALLED FOR
C      SEQUENTIAL VALUES OF I FROM 1 TO NDFJ.  THUS THE 2-0
C      DISPLACEMENT ARRAYS ARE FORMED FOR I=1 ONLY.
C      ISEQ=1, INDICATES THAT THE SUBROUTINE IS BEING CALLED WITH THE
C      PREVIOUS VALUE FOR I BUT A NEW STEP SIZE (DELTA).  IN
C      THIS CASE CERTAIN CALCULATIONS ARE NOT REPEATED.
C      ISEQ=2, INDICATES THAT THE 2-0 DISPLACEMENT ARRAYS HAVE BEEN
C      FORMED.  THUS THIS CALCULATION MAY BE SKIPPED.
C
COMMON/ELEMENT/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1  MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),DELTA 210
2  MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)  DELT 220
COMMON/JOINTS/ACC(3,50),BET(3,50),OAS(3,50),DIS(3,50),ERJF(3,50),  DELT 230
1  ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),  DELT 240
1  XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)  DELT 250
COMMON/LEAD8K/AVDM,AVGL,CA,C8,CC,CD,CE,OHEAD(20),DT,EPS,HEAD(20),  DELT 260
1  PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB  DELT 270
1  DELT 280

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```

COMMON/MAINBK/IANAL, ICURV, IERR, IFAIL, IFOR, ILIN, IPAGE, IPLOT, IPRINT, DELT 290
1 IREC, ISTART, ISTOP, ISTRES, ITAPE, IUNITS, IYLO, LERR, LINE, NACC, NCM, DELT 300
2 NCRD, NDF, NDFD, NDFJ, NDIS, NDL, NFF, NJOR, NINC, NJ, NJD, NJER, NL, NLD, DELT 310
3 NLS, NLSR, NM, NMAS, NMAT, NMATD, NMD, NPLOT, NPRT, NSAVE, NTAB, NTAPE, DELT 320
4 NTIMES, NVEL, IINITD DELT 330
COMMON/MEMBER/AGRP(10,45), ATIES(6,45), BMEM(45), BPP(45), BDM(10,45), DELT 340
1 BWF(45), D(45), DP(45), DPP(45), DMF(45), EFFL(10,45), EFLM(45), DELT 350
2 HMEM(45), HTOP(45), HTWF(45), PDP(7,45), SPRING(5,20), STIES(7,45), DELT 360
3 TFWF(45), TWWF(45), UDM(45), URM(45), XBEG(10,45), DELT 370
4 XBEGM(45), XBEGS(6,45), XL(45), XPI(5,45), YBAR(10,45), YGP(7,45), DELT 380
5 YFIBR(11,45), YLOS(45), XDM(45), PDF(7,45), DISM(45) DELT 390
DELT 400
DELT 410
DELT 420
DELT 430
DELT 440
DELT 450
DELT 460
DELT 470
DELT 480
DELT 490
DELT 500
DELT 510
DELT 520
DELT 530
DELT 540
DELT 550
DELT 560
DELT 570
DELT 580

C
INTEGER HEAD, DHEAD
DIMENSION SOLN(90)

C
IF(ISEQ.EQ.1) GO TO 50
IF(ISEQ.EQ.2) GO TO 30

C
INITIALIZE.

C
IF(I.NE.1) GO TO 30
DO 20 N=1, NDFJ
J=IOFI(N)
K=IDFII(N)
XDJ(K,J)=SOLN(N)
L=NDFJ+1
DO 16 N=L, NDF
M=IOFI(N)
XDM(M)=SOLN(N)
J=IOFI(I)

```



70	CONTINUE	DELT 890
	GO TO 73	DELT 900
71	IF(XDM(J).EQ.0.E0)GO TO 72	DELT 910
	IF(ABS(DELT I/XDM(J)).GT.EPS)GO TO 72	DELT 920
	DVALUE=0.E0	DELT 930
	GO TO 90	DELT 940
72	XDM(J)=XDM(J)-DELTA	DELT 950
	CALL ENGY(J,VALUE3,VALUE4)	DELT 960
	GO TO 76	DELT 970
73	IF (NLS.LE.0) GO TO 76	DELT 980
	DO 74 M=1,NLS	DELT 990
	IF(IPL(M).NE.J.AND.IQL(M).NE.J) GO TO 74	DELT1000
	CALL LEAF(-M,UR,1)	DELT1010
	VALUE3=VALUE3+UR	DELT1020
74	CONTINUE	DELT1030
C		DELT1040
C	CALCULATE MEMBER ENERGY FOR THE I-TH VARIABLE WITH POSITIVE INCREMENT	DELT1050
C		DELT1060
76	DELTA2=DELTA+DELTA	DELT1070
	IF(I.GT.NDFJ) GO TO 87	DELT1080
	VALUE5=0.E0	DELT1090
	VALUE6=0.E0	DELT1100
	XOJ(K,J)=XOJ(K,J)+DELTA2	DELT1110
	DO 80 L=1,NM	DELT1120
	IF (IP(L).NE.J.AND.IQ(L).NE.J) GO TO 80	DELT1130
	CALL ENGY (L,UR,UD)	DELT1140
	VALUE5=VALUE5+UR	DELT1150
	VALUE6=VALUE6+UD	DELT1160
80	CONTINUE	DELT1170
	IF (NLS.EQ.0) GO TO 86	DELT1180



DELT11190  
 DELT11200  
 DELT11210  
 DELT11220  
 DELT11230  
 DELT11240  
 DELT11250  
 DELT11260  
 DELT11270  
 DELT11280  
 DELT11290  
 DELT11300  
 DELT11310  
 DELT11320  
 DELT11330  
 DELT11340

DO 84 M=1,NLS  
 IF (IPL(M).NE.J.AND.IQL(M).NE.J) GO TO 84  
 CALL LEAF1(-M,JR,1)  
 VALUE5=VALUE5+UR  
 CONTINUE  
 XDJ(K,J)=SOLN(I)  
 GO TO 89  
 XDM(J)=XDM(J)+DELTA2  
 CALL ENGY(J,VALUE5,VALUE6)  
 XDM(J)=SOLN(I)  
 CALCULATE DERIVATIVE.  
 DVALUE=(VALUE1+VALUE2+(VALUE5+VALUE6-VALUE3-VALUE4)/DELTA2)/AVDM  
 RETURN  
 END

84  
 86  
 87  
 C  
 C  
 C  
 89  
 90

```

CELIN 0 10
SUBROUTINE ELIN(KIND)
C
C SUBROUTINE TO PRINT A TABLE OF ELEMENT CHARACTERISTICS TAKEN
C FROM COMMON BLOCKS.
C
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),
1 SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,ELIN
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,ELIN
2 NCRD,NDF,NDFD,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,
4 NTIMES,NVEL,IINITD
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),8MEM(45),8PP(45),80M(10,45),
1 8WF(45),D(45),OP(45),OPP(45),OWF(45),EFFL(10,45),EFLM(45),
2 HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),
3 TFWF(45),TWWF(45),UDM(45),URM(45),XBEG(10,45),
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),
5 YFIBR(11,45),YLOS(45),XOM(45),PDF(7,45),DISM(45)
DIMENSION KIND(45)
DATA RC/3HR/C/,WF/3HW/F/,DET/6HDETAIL/,8IS/6H8ISECT/,ED/2HED/
CALL PAGE
WRITE(NPRT,30)
FORMAT(1H0,18X,51HSUMMARY DATA FOR FINITE ELEMENTS USED IN SIMULAT
ION)
LINE=LINE+2
WRITE(NPRT,40)
30

```

```

40      FORMAT(1H0,6X,7HELEMENT,6X,6HJOINTS,9X,4HKIND,8X,4HTYPE,12X,6HLENGELIN 290
      1TH,12X,8HMATERIAL/)      ELIN 300
      LINE=LINE+3      ELIN 310
      DO 100 I=1,NH      ELIN 320
      LINE=LINE+1      ELIN 330
      IF(LINE.LE.NL) GO TO 50      ELIN 340
      CALL PAGE      ELIN 350
      WRITE(NPRT,40)      ELIN 360
      LINE=LINE+3      ELIN 370
      TTYPE=RC      ELIN 380
      AKIND=DET      ELIN 390
      IF(KIND(I).EQ.1) AKIND=BIS      ELIN 400
      IF(MTYPE(I).EQ.4) GO TO 70      ELIN 410
      MATL=MCODE(I)      ELIN 420
      GO TO 80      ELIN 430
      TTYPE=WF      ELIN 440
      MATL=MATW(I)      ELIN 450
      WRITE(NPRT,90) I,IP(I),IG(I),AKIND,ED,TTYPE,XL(I),NAME(MATL)      ELIN 460
      FORMAT(1H ,8X,I3,6X,I3,1H-,I3,8X,A6,A2,7X,A3,8X,E14.7,10X,A4)      ELIN 470
      CONTINUE      ELIN 480
      RETURN      ELIN 490
      END      ELIN 500

```





```

CENGY      0  10
C          SUBROUTINE ENGY (M,UR,UD)
C
C          THIS SUBROUTINE MANAGES THE RECOVERABLE STRAIN ENERGY (UR) AND
C          THE DISSIPATIVE STRAIN ENERGY (UD) CALCULATION FOR MEMBER (M).
C          THE TYPE OF MEMBER IS INDICATED BY MTYPE(M), WHERE
C          MTYPE=1, INDICATES A REINFORCED CONCRETE MEMBER WITH STIRRUPS.
C          MTYPE=2, INDICATES A REINFORCED CONCRETE MEMBER WITH TIES.
C          MTYPE=3, INDICATES A REINFORCED CONCRETE MEMBER WITH AN
C                   EMBEDDED WIDE FLANGE.
C          MTYPE=4, INDICATES A NONCOMPOSITE WIDE FLANGE MEMBER.
C          MTYPE=5, INDICATES A LINEAR LEAF SPRING MEMBER.
C
C          COMMON/ELEMENT/IDUM1(851),MTYPE(45),IDUM2(360)
C
C          GENERAL REINFORCED CONCRETE MEMBER.
C          IF (MTYPE(M).LT.4) CALL MEMB (M,UR,UD,1)
C
C          STEEL WIDE FLANGE MEMBER.
C          IF (MTYPE(M).EQ.4) CALL WIDE (M,UR,UD,1)
C          RETURN
C          END

```

```

ENG Y      0
ENG Y     10
ENG Y     20
ENG Y     30
ENG Y     40
ENG Y     50
ENG Y     60
ENG Y     70
ENG Y     80
ENG Y     90
ENG Y    100
ENG Y    110
ENG Y    120
ENG Y    130
ENG Y    140
ENG Y    150
ENG Y    160
ENG Y    170
ENG Y    180
ENG Y    190
ENG Y    200

```

```

CERRS      0 10
SUBROUTINE ERRS (SOLN,VALUEM)
C
C      THIS SUBROUTINE CALCULATES THE ERROR MEASURES AT THE MIDDLE AND ENDS
C      OF THE TIME INTERVAL.
C
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),DIS(3,50),ERJF(3,50),
1  ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
1  XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1  PI,PERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,ERRS
1  IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LEERR,LINE,NACC,NCM,ERRS
2  NCRD,NDF,NDFD,NDFJ,NDIS,NDL,NFF,NJOR,NING,NJ,NJD,NJER,NL,NLD,ERRS
3  NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,ERRS
4  NTIMES,NVEL,IINITD
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BDM(10,45),ERRS
1  BWF(45),D(45),DP(45),OPP(45),DMF(45),EFFL(10,45),EFLM(45),ERRS
2  HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),ERRS
3  TFWF(45),TWWF(45),UDM(45),URM(45),XBEG(10,45),ERRS
4  XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),ERRS
5  YFIBR(11,45),YLDOS(45),XDM(45),PDF(7,45),DISM(45)
COMMON/SEEK8K/DEFOR(90),STPSIZ(90),GRAD(90),GRADI(90),DELTAG(90),ERRS
1  DIRECT(90),DIAG(90),STEP(4),DSTEP(4),FVAL(4),VALUES(7),ERRS
2  DISACC,SSIZE,FUNACC,FUNMIN,CRITL,CRITU,NLIN
C
C      DIMENSION SOLN(90)
C      INTEGER HEAD,DHEAD
C
ERRS      0
ERRS      10
ERRS      20
ERRS      30
ERRS      40
ERRS      50
ERRS      60
ERRS      70
ERRS      80
ERRS      90
ERRS     100
ERRS     110
ERRS     120
ERRS     130
ERRS     140
ERRS     150
ERRS     160
ERRS     170
ERRS     180
ERRS     190
ERRS     200
ERRS     210
ERRS     220
ERRS     230
ERRS     240
ERRS     250
ERRS     260
ERRS     270
ERRS     280

```

```

C          CALCULATE ERROR AT END OF TIME INTERVAL.
RERF=0.E0
DO 10 I=1,NDFJ
  J=IDFI(I)
  K=IDFII(I)
  DELTA=STPSIZ(I)
  CALL DELT (SOLN,DELTA,I,DER(K,J),2)
  IF (VALUEM.EQ.0.E0) VALUEM=TINY
  RESENG(K,J)=DER(K,J)*SOLN(I)
  ERJF(K,J)=RESENG(K,J)/VALUEM
  RERF=AMAX1(ABS(ERJF(K,J)),RERF)
  CONTINUE
10
C
C          IF STATIC ANALYSIS, RETURN
C
C          IF (DT.EQ.0.E0.OR.NMAS.EQ.0) GO TO 70
C
C          CALCULATE DISPLACEMENTS AT MIDDLE OF TIME INTERVAL.
C
C          DO 30 I=1,NDFJ
C            J=IDFI(I)
C            K=IDFII(I)
C            IF (DAS(K,J).EQ.0.E0) GO TO 20
C            BETX=6.E0*((SOLN(I)-DIS(K,J))/(DT*DT) -VEL(K,J)/DT-0.5E0*ACC(K,J))/
10T
C            DEFOR(I)=BETX*DT*DT/48.E0+ACC(K,J)*DT*DT/8.E0+VEL(K,J)*DT/2.E0+ERRS 540
C            10IS(K,J)
C            GO TO 30
C            DEFOR(I)=(SOLN(I)+DIS(K,J))/2.E0
C            CONTINUE
20
30
ERRS 290
ERRS 300
ERRS 310
ERRS 320
ERRS 330
ERRS 340
ERRS 350
ERRS 360
ERRS 370
ERRS 380
ERRS 390
ERRS 400
ERRS 410
ERRS 420
ERRS 430
ERRS 440
ERRS 450
ERRS 460
ERRS 470
ERRS 480
ERRS 490
ERRS 500
ERRS 510
ERRS 520
ERRS 530
ERRS 540
ERRS 550
ERRS 560
ERRS 570
ERRS 580

```

```

L=NDFJ+1
DO 35 I=L,NDF
M=IOFI(I)
DEFOR(I)=(SOLN(I)+DISM(M))/2.E0
35 C
C
C
C
CALCULATE FORCING FUNCTIONS AT MIDDLE OF TIME INTERVAL.

SAVE1=DT
SAVE2=TIME
DT=DT/2.E0
TIME=TIME-DT
IF (NFF.EQ.0) GO TO 40
CALL FORS (TIME)
C
C
C
C
CALCULATE ERROR AT MIDDLE OF TIME INTERVAL.

RERH=0.E0
DO 50 I=1,NDF J
J=IOFI(I)
K=IOFI(I)
IF (OAS(K,J).EQ.0.E0) GO TO 50
DELTA=STPSIZ(I)
CALL DELT (DEFOR,DELTA,I,DERIV,0)
ERJH(K,J)=DERIV*DEFOR(I)/VALUEM
RERH=AMAX1 (ABS (ERJH(K,J)),RERH)
50 C
C
C
C
CONTINUE
RESET DATA
DT=SAVE1

```

```

ERRS 590
ERRS 600
ERRS 610
ERRS 620
ERRS 630
ERRS 640
ERRS 650
ERRS 660
ERRS 670
ERRS 680
ERRS 690
ERRS 700
ERRS 710
ERRS 720
ERRS 730
ERRS 740
ERRS 750
ERRS 760
ERRS 770
ERRS 780
ERRS 790
ERRS 800
ERRS 810
ERRS 820
ERRS 830
ERRS 840
ERRS 850
ERRS 860
ERRS 870
ERRS 880

```



ERRS 890  
ERRS 900  
ERRS 910  
ERRS 920  
ERRS 930  
ERRS 940  
ERRS 950  
ERRS 960  
ERRS 970  
ERRS 980  
ERRS 990

TIME=SAVE2  
DO 60 I=1,NDF J  
J=IDFI(I)  
K=IDFII(I)  
XDJ(K,J)=SOLN(I)  
L=NDFJ+1  
DO 65 I=L,NDF  
M=IDFI(I)  
XDM(M)=SOLN(I)  
RETURN  
END

60  
65  
70

```

CFAIL 0 10
SUBROUTINE FAIL
C
C THIS SUBROUTINE CHECKS THE MACROSCOPIC FAILURE CRITERIA FOR
C A REINFORCED CONCRETE MEMBER(M).
C
C
COMMON DATA(10000),KDATA(500)
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),
1 SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),JNLK(9),ICODE(9),NAME(9)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1 PI,REF,REH,RERZ,SERR,IBEGIN,THALT,TIME,TINK,TINY,TPROB
INTEGER HEAD,DHEAD
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,
2 NCRO,NDF,NDFD,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,
4 NTIMES,NVEL,IINITD
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BDM(10,45),
1 BWF(45),D(45),DP(45),DPP(45),DWF(45),EFFL(10,45),EFLM(45),
2 HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),
3 TFWF(45),TWWF(45),UDM(45),URM(45),XBEG(10,45),
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),
5 YFIBR(11,45),YLDS(45),XDM(45),PDF(7,45),DISM(45)
COMMON/SAVEBK/SAVACC(3,50),SAVAXL(2,45),SAVCRV(2,45),SAVMOM(2,45)
1 ,SAVSHR(2,45),SAVSRP(3,20),SAVSRQ(3,20),SAVXDJ(3,50),
2 SAVVEL(3,50),SVSTRN(12,45),SVSTRS(12,45)
FAIL 0
FAIL 10
FAIL 20
FAIL 30
FAIL 40
FAIL 50
FAIL 60
FAIL 70
FAIL 80
FAIL 90
FAIL 100
FAIL 110
FAIL 120
FAIL 130
FAIL 140
FAIL 150
FAIL 160
FAIL 170
FAIL 180
FAIL 190
FAIL 200
FAIL 210
FAIL 220
FAIL 230
FAIL 240
FAIL 250
FAIL 260
FAIL 270
FAIL 280

```

```

COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB,
1  LTABI,NMAX,NMAXI
COMMON/STRNBK/SRP(4),SRQ(4),UX,UY,UZ,XLEN,AREA,ZZI,IMAT
LOGICAL PASS(2)
DIMENSION ASUBV(2),F(2),FFOUR(2),FTWO(2)
1 ,TEMP(24),STRESS(24),STRAIN(24),SFIVE(24),SEIGHT(24)

C
LINE = NL
EGSIS = 1.E0
IF (IUNITS.EQ.1.OR.IUNITS.EQ.2) EGSIS = 6894.75789
DO 7000 M=1,NM
DO 3000 L=1,2
SAVAXL(L,M) = 0.E0
SAVGRV(L,M) = 0.E0
SAVMOM(L,M) = 0.E0
SAVSHR(L,M) = 0.E0
CONTINUE
3000
XLEN = XL(M)
CALL DEFO(M)

C
C
VERIFY ELEMENT TYPE
IF(MTYPE(M).EQ.5) GO TO 7000
IF(MTYPE(M).EQ.4) GO TO 3170
CALL MEMB(M,UR,UD,3)
NGRPM = NGRP(M)
NNG = NGRPM + 14
NTIESM = NTIES(M)

C
C
COLLECT ELEMENT DIMENSIONS
TEMP(1) = YFIBR( 1,M)

```

```

FAIL 290
FAIL 300
FAIL 310
FAIL 320
FAIL 330
FAIL 340
FAIL 350
FAIL 360
FAIL 370
FAIL 380
FAIL 390
FAIL 400
FAIL 410
FAIL 420
FAIL 430
FAIL 440
FAIL 450
FAIL 460
FAIL 470
FAIL 480
FAIL 490
FAIL 500
FAIL 510
FAIL 520
FAIL 530
FAIL 540
FAIL 550
FAIL 560
FAIL 570
FAIL 580

```

FAIL 590  
 FAIL 600  
 FAIL 610  
 FAIL 620  
 FAIL 630  
 FAIL 640  
 FAIL 650  
 FAIL 660  
 FAIL 670  
 FAIL 680  
 FAIL 690  
 FAIL 700  
 FAIL 710  
 FAIL 720  
 FAIL 730  
 FAIL 740  
 FAIL 750  
 FAIL 760  
 FAIL 770  
 FAIL 780  
 FAIL 790  
 FAIL 800  
 FAIL 810  
 FAIL 820  
 FAIL 830  
 FAIL 840  
 FAIL 850  
 FAIL 860  
 FAIL 870  
 FAIL 880

```

TEMP(2) = YFIBR( 2,M)
TEMP(3) = YFIBR( 6,M)
TEMP(4) = YFIBR(10,M)
TEMP(5) = YFIBR(11,M)
DO 3010 J=6,14
  TEMP(J) = YFIBR(J-4,M)
3010 CONTINUE
DO 3020 J=15,24
  TEMP(J) = YBAR(J-14,M)
3020 CONTINUE
DO 3150 L=1,2
  ESMAX = -TINY
  ESMIN = TINY
  NESMAX = 1
  NESMIN = 1
  IF(MSTAT(M).EQ.3) GO TO 3040

C
C
STRESS AND STRAIN COMPUTATIONS FOR AN ELASTIC ELEMENT
XLOC = 0.E0
IF(L.EQ.2) XLOC = XLEN
DO 3030 K=1,NNG
  IF(K.GE.1.AND.K.LE.5) J = MCODE(M)
  IF(K.GE.6.AND.K.LE.14) J = MATR(M)
  IF(K.GE.15.AND.K.LE.24) J = MBAR(K-14,M)
  CALL STRN(M,XLOC,TEMP(K),STRAIN(K))
  ELASMD = ET(J)
  IF(STRAIN(K).LE.0.E0) ELASMD = EC(J)
  STRESS(K) = ELASMD*STRAIN(K)
  IF(K.LE.14.AND.STRAIN(K).GT.0.E0) STRESS(K) = 0.E0
  IF(K.LT.15) GO TO 3030

```



```

IF(STRAIN(K).LT.ESMAX) GO TO 3025
ESMAX=STRAIN(K)
NESMAX=K-14
GO TO 3030
3025 IF(STRAIN(K).GT.ESMIN) GO TO 3030
ESMIN=STRAIN(K)
NESMIN=K-14
3030 CONTINUE
GO TO 3100
C
C
C
C
STRESSES AND STRAINS FOR YIELDED R/C ELEMENTS
3040 INDEX = KDATA(LPSI+M)-1+NGRPM*40+168
C
C
UNCONFINED CONCRETE STRESSES
LBGN = INDEX+(L-1)*40+6
LEND = LBGN+35
K = 0
DO 3050 KK=LBGN,LEND,8
K = K+1
STRESS(K) = DATA(KK)
CONTINUE
3050 INDEX = KDATA(LPI+M)+NGRPM*5+(L-1)*5+20
STRAIN(1) = DATA(INDEX+1)
STRAIN(5) = DATA(INDEX+5)
C
C
CONFINED CONCRETE STRESSES
INDEX = KDATA(LPSI+M)+NGRPM*40+(L-1)*72+319
LBGN = INDEX+6
LEND = LBGN+67

```

```

FAIL 890
FAIL 900
FAIL 910
FAIL 920
FAIL 930
FAIL 940
FAIL 950
FAIL 960
FAIL 970
FAIL 980
FAIL 990
FAIL1000
FAIL1010
FAIL1020
FAIL1030
FAIL1040
FAIL1050
FAIL1060
FAIL1070
FAIL1080
FAIL1090
FAIL1100
FAIL1110
FAIL1120
FAIL1130
FAIL1140
FAIL1150
FAIL1160
FAIL1170
FAIL1180

```

```

DO 3060 KK=LBGN,LEND,8
K = K+1
STRESS(K) = DATA(KK)
3060 CONTINUE
C
C REINFORCING STEEL STRAINS.
INDEX = KDATA(LPI+M)-1+NGRPM*3
LBGN = INDEX + L
LEND = INDEX+NGRPM*2
DO 3070 KK=LBGN,LEND,2
K = K+1
STRAIN(K) = DATA(KK)
3070 CONTINUE
INDEX = KDATA(LPSI+M)-1+NGRPM*24+(L-1)*8
LBGN = INDEX+5
LEND = INDEX+NGRPM*16
C
C REINFORCING STEEL STRESSES.
K = 14
DO 3080 KK=LBGN,LEND,16
K = K+1
SFIVE(K) = DATA(KK)
SEIGHT(K) = DATA(KK+3)
3080 CONTINUE
DO 3090 K=15, NNG
STRESS(K) = -SEIGHT(K)
IF (STRAIN(K)-SFIVE(K).GE.0.E0) STRESS(K) = SEIGHT(K)
3090 CONTINUE
3100 SAVCRV(L,M) = (STRAIN(1)-STRAIN(5))/(TEMP(1)-TEMP(5))
C

```

```

FAIL1190
FAIL1200
FAIL1210
FAIL1220
FAIL1230
FAIL1240
FAIL1250
FAIL1260
FAIL1270
FAIL1280
FAIL1290
FAIL1300
FAIL1310
FAIL1320
FAIL1330
FAIL1340
FAIL1350
FAIL1360
FAIL1370
FAIL1380
FAIL1390
FAIL1400
FAIL1410
FAIL1420
FAIL1430
FAIL1440
FAIL1450
FAIL1460
FAIL1470
FAIL1480

```

```

C      STRESS RESULTANTS DUE TO UNCONFINED CONCRETE
DO 3110 K=1,4
  WIDTH = BMEM(M)
  IF(K.EQ.2.OR.K.EQ.3) WIDTH = WIDTH - BPP(M)
  FORCE = (STRESS(K)+STRESS(K+1))/2.E0*WIDTH*(TEMP(K)-TEMP(K+1))
  IF(ABS(FORCE).LE.TINY) GO TO 3110
  IF (L.EQ.2) SAVAXL(2,M) = SAVAXL(2,M) + FORCE
  CENT=(TEMP(K)-TEMP(K+1))*(2.E0*STRESS(K)+STRESS(K+1))/
    1(STRESS(K)+STRESS(K+1))/3.E0
  SAVMOM(L,M) = SAVMOM(L,M)+FORCE*(CENT+TEMP(K+1))
3110 CONTINUE
C
C      STRESS RESULTANTS DUE TO CONFINED CONCRETE
DO 3130 K=6,13
  AREA = BPP(M)*(TEMP(K)-TEMP(K+1))
C
C      REMOVE CONCRETE DISPLACED BY REINFORCING STEEL
DO 3120 N=1,NGRPM
  IF(YBAR(N,M).LT.TEMP(K).AND.YBAR(N,M).GT.TEMP(K+1))
    *   AREA = AREA - AGRP(N,M)
    *   IF(YBAR(N,M).EQ.TEMP(K).OR.YBAR(N,M).EQ.TEMP(K+1))
      *   AREA = AREA - AGRP(N,M)/2.E0
3120 CONTINUE
  FORCE = (STRESS(K)+STRESS(K+1))*AREA/2.E0
  IF(ABS(FORCE).LE.TINY) GO TO 3130
  IF (L.EQ.2) SAVAXL(2,M) = SAVAXL(2,M) + FORCE
  CENT=(TEMP(K)-TEMP(K+1))*(2.E0*STRESS(K)+STRESS(K+1))/
    1(STRESS(K)+STRESS(K+1))/3.E0
  SAVMOM(L,M) = SAVMOM(L,M)+FORCE*(CENT+TEMP(K+1))
3130 CONTINUE

```

```

FAIL1490
FAIL1500
FAIL1510
FAIL1520
FAIL1530
FAIL1540
FAIL1550
FAIL1560
FAIL1570
FAIL1580
FAIL1590
FAIL1600
FAIL1610
FAIL1620
FAIL1630
FAIL1640
FAIL1650
FAIL1660
FAIL1670
FAIL1680
FAIL1690
FAIL1700
FAIL1710
FAIL1720
FAIL1730
FAIL1740
FAIL1750
FAIL1760
FAIL1770
FAIL1780

```

```

C
C
C      STRESS RESULTANTS DUE TO REINFORCING STEEL
DO 3140 K=15,NNG
FORCE = STRESS(K)*AGRP(K-14,M)
IF(L.EQ.2) SAVAXL(2,M) = SAVAXL(2,M) + FORCE
SAVMOM(L,M) = SAVMOM(L,M)+FORCE*TEMP(K)
3140 CONTINUE
IF(L.EQ.2) SAVMOM(2,M)=-SAVMOM(2,M)
IF(L.EQ.1) ETOPA=STRAIN(1)
IF(L.EQ.1) EBOTA=STRAIN(5)
IF(L.EQ.2) ETOPB=STRAIN(1)
IF(L.EQ.2) EBOTB=STRAIN(5)
ECHAX=AMAX1(ETOPA,EBOTA,ETOPB,EBOTB)
ECHIN = AMIN1 (ETOPA,EBOTA,ETOPB,EBOTB)
3150 CONTINUE
SAVAXL(1,M) = -SAVAXL(2,M)
SAVSHR(2,M) = -(SAVMOM(1,M)+SAVMOM(2,M))/XLEN+SAVAXL(2,M)*UY
SAVSHR(1,M) = -SAVSHR(2,M)
GO TO 5000

C      WIDE FLANGE STRESSES AND STRAINS.
C
C
3170 CALL WIDE (M,UR,UD,3)
DO 4080 L=1,2
IF(MSTAT(M).EQ.3) GO TO 4020

C      ELASTIC STRESSES AND STRAINS
C      J = MATH(M)
XLOC = 0.E0
IF(L.EQ.2) XLOC = XLEN

```

```

FAIL1790
FAIL1800
FAIL1810
FAIL1820
FAIL1830
FAIL1840
FAIL1850
FAIL1860
FAIL1870
FAIL1880
FAIL1890
FAIL1900
FAIL1910
FAIL1920
FAIL1930
FAIL1940
FAIL1950
FAIL1960
FAIL1970
FAIL1980
FAIL1990
FAIL2000
FAIL2010
FAIL2020
FAIL2030
FAIL2040
FAIL2050
FAIL2060
FAIL2070
FAIL2080

```



```

DO 4010 K=1,11
CALL STRN(M,XLOC,YFIBR(K,M),STRAIN(K))
IF (STRAIN(K).LE.0.E0) STRESS(K) = STRAIN(K)*EC(J)
IF (STRAIN(K).GT.0.E0) STRESS(K) = STRAIN(K)*ET(J)
4010 CONTINUE
GO TO 4060

C
C INELASTIC STRESSES AND STRAINS
4020 INDEX = KDATA(LPI+M)+21
LBGN = INDEX+(L-1)*11
LEND = LBGN+10
K = 0
DO 4030 KK=LBGN,LEND
K = K+1
STRAIN(K) = DATA(KK)
4030 CONTINUE
INDEX = KDATA(LPSI+M)+167
LBGN = INDEX+(L-1)*88+5
LEND = LBGN + 80
K = 0
DO 4040 KK=LBGN,LEND,8
K = K+1
SFIVE(K) = DATA(KK)
SEIGHT(K) = DATA(KK+3)
4040 CONTINUE
DO 4050 K=1,11
STRESS(K) = -SEIGHT(K)
IF (STRAIN(K)-SFIVE(K).GE.0.E0) STRESS(K) = SEIGHT(K)
4050 CONTINUE
4060 SAVCRV(L,M) = (STRAIN(1)-STRAIN(11))/(YFIBR(1,M)-YFIBR(11,M))

```

```

FAIL2090
FAIL2100
FAIL2110
FAIL2120
FAIL2130
FAIL2140
FAIL2150
FAIL2160
FAIL2170
FAIL2180
FAIL2190
FAIL2200
FAIL2210
FAIL2220
FAIL2230
FAIL2240
FAIL2250
FAIL2260
FAIL2270
FAIL2280
FAIL2290
FAIL2300
FAIL2310
FAIL2320
FAIL2330
FAIL2340
FAIL2350
FAIL2360
FAIL2370
FAIL2380

```

```

DO 4070 K=1,10
  WIDTH = TWLF(M)
  IF(K.EQ.1.OR.K.EQ.10) WIDTH = BWF(M)
  FORCE=(STRESS(K)+STRESS(K+1))*WIDTH*(YFIBR(K,M)-YFIBR(K+1,M))/2.E0
  IF(ABS(FORCE).LE.TINY) GO TO 4070
  IF(L.EQ.2) SAVAXL(2,M) = SAVAXL(2,M) + FORCE
  CENT=(YFIBR(K,M)-YFIBR(K+1,M))*(2.E0*STRESS(K)+STRESS(K+1))/
  1(STRESS(K)+STRESS(K+1))/3.E0
  SAVMOM(L,M) = SAVMOM(L,M)+FORCE*(CENT+YFIBR(K+1,M))
4070 CONTINUE
  IF(L.EQ.2) SAVMOM(2,M)=-SAVMOM(2,M)
  IF(L.EQ.1) ETOPA=STRAIN(1)
  IF(L.EQ.1) EBOTA=STRAIN(11)
  IF(L.EQ.2) ETOPB=STRAIN(1)
  IF(L.EQ.2) EBOTB=STRAIN(11)
  ESMAX=AMAX1(ETOPA,EBOTA,ETOPB,EBOTB)
  ESMIN = AMIN1 (ETOPA,EBOTA,ETOPB,EBOTB)
4080 CONTINUE
  SAVAXL(1,M) = -SAVAXL(2,M)
  SAVSHR(2,M) = -(SAVMOM(1,M)+SAVMOM(2,M))/XLEN+SAVAXL(2,M)*UY
  SAVSHR(1,M) = -SAVSHR(2,M)
C
C DETERMINATION OF CRITERIA TO BE CHECKED.
C
5000 J = MBAR(NESMAX,M)
  IF(MTYPE(M).EQ.4) J = MATW(M)
C
C STEEL FRACTURE CRITERIA REF. B.3.1.2
C
  IF(ABS(ESMAX).LT.STN(7,J)) GO TO 5020
  FAIL2390
  FAIL2400
  FAIL2410
  FAIL2420
  FAIL2430
  FAIL2440
  FAIL2450
  FAIL2460
  FAIL2470
  FAIL2480
  FAIL2490
  FAIL2500
  FAIL2510
  FAIL2520
  FAIL2530
  FAIL2540
  FAIL2550
  FAIL2560
  FAIL2570
  FAIL2580
  FAIL2590
  FAIL2600
  FAIL2610
  FAIL2620
  FAIL2630
  FAIL2640
  FAIL2650
  FAIL2660
  FAIL2670
  FAIL2680

```

```

LINE = LINE + 1
IF (LINE.GT.NL) CALL PAGE
IFAIL = 1
PRINT 610, IP(M), IQ(M)
610 FORMAT( 39H **STEEL FRACTURE DETECTED IN ELEMENT , I3, 1H-, I3,
+ 39H. THE ANALYSIS IS TERMINATED (FAIL).**)
5020 IF (MTYPE(M).EQ.4) GO TO 7000
C
C CONCRETE CRUSHING REF.8.3.1.1
IF (NTIESM.GT.0) GO TO 5313
J = MCODE(M)
TEMPR = (3.E0*EGSIS + .002E0*FCFY(J))/(FCFY(J)-1.E3*EGSIS)
IF (TEMPR.GT.3.5E-3) TEMPR = 3.5E-3
EPSTAR = CA*TEMPR
IF (EPSTAR-ABS(ECMAX).GT.0.E0) GO TO 5313
LINE = LINE + 1
IF (LINE.GT.NL) CALL PAGE
IFAIL = 1
PRINT 630, IP(M), IQ(M)
630 FORMAT( 42H **CONCRETE CRUSHING DETECTED IN ELEMENT , I3, 1H-, I3,
+ 39H. THE ANALYSIS IS TERMINATED (FAIL).**)
C
C SIMULTANEOUS BAR BUCKLING AND CONCRETE CRUSHING REF.8.3.1.3
5313 IF (NTIESM.EQ.0) GO TO 532
J = MBAR(NESMIN,M)
DO 100 K=1,6
IF ((ABS(ESMIN).GT.STN(K,J).AND.ABS(ESMIN).LT.STN(K+1,J)) .OR.
* (ABS(ESMIN).EQ.STN(K,J))) GO TO 5030
100 CONTINUE
5030 ETAN = SLOPE(K,J)

```

```

FAIL2690
FAIL2700
FAIL2710
FAIL2720
FAIL2730
FAIL2740
FAIL2750
FAIL2760
FAIL2770
FAIL2780
FAIL2790
FAIL2800
FAIL2810
FAIL2820
FAIL2830
FAIL2840
FAIL2850
FAIL2860
FAIL2870
FAIL2880
FAIL2890
FAIL2900
FAIL2910
FAIL2920
FAIL2930
FAIL2940
FAIL2950
FAIL2960
FAIL2970
FAIL2980

```

```

FSTRS = STS(K,J)+ETAN*ABS(ESMIN)
CRIT = CB*PI*PI/16.E0*(80M(NESMIN,M)/STIES(7,M))*ETAN
IF (CRIT-FSTRS .GT. 0.E0) GO TO 532
LINE = LINE + 1
IF (LINE.GT.NL) CALL PAGE
IF (ISTOP.EQ.1) GO TO 5031
IFAIL = 1
PRINT 640, IP(M), IQ(M)
FORMAT( 52H **SIMULTANEOUS BAR BUCKLING AND CONCRETE CRUSHING ,
2 20HDETECTED IN ELEMENT ,I3,1H-,I3,
+ 39H. THE ANALYSIS IS TERMINATED (FAIL).***)
GO TO 532
5031 PRINT 650, IP(M), IQ(M)
650 FORMAT( 52H ** SIMULTANEOUS BAR BUCKLING AND CONCRETE CRUSHING ,
2 20HDETECTED IN ELEMENT ,I3,1H-,I3,
+ 39H. THE ANALYSIS IS CONTINUING (FAIL). **)
C
C SHEAR-FLEXURE CHECK CLASSIFICATION SEGMENT
C
532 PASS(1) = .FALSE.
PASS(2) = .FALSE.
C
C SET OPTIONAL AND CONSTANT FUNCTION VALUES
J = NCODE(M)
TEMPO = SAVAXL(2,M)/BMEM(M)/SQRT(FCFY(J))
FFOURA = TEMPO/D(M)
FFOURB = TEMPO/(HMEM(M)-DP(M))
IF(TEMPO.GE.0.E0) ALFA = 0.025E0*(4.E0-CD)
IF(TEMPO.LT.0.E0) ALFA = 0.05E0*(2.E0+CD)
FTWOBR = 1.E3/BMEM(M)/SQRT(FCFY(J))

```

```

FAIL2990
FAIL3000
FAIL3010
FAIL3020
FAIL3030
FAIL3040
FAIL3050
FAIL3060
FAIL3070
FAIL3080
FAIL3090
FAIL3100
FAIL3110
FAIL3120
FAIL3130
FAIL3140
FAIL3150
FAIL3160
FAIL3170
FAIL3180
FAIL3190
FAIL3200
FAIL3210
FAIL3220
FAIL3230
FAIL3240
FAIL3250
FAIL3260
FAIL3270
FAIL3280

```



```

C      TEMPO = ABS(SAVSHR(1,M))/BMEM(M)/SQRT(FCFY(J))
C      FA = TEMPO/D(M)
C      FB = TEMPO/(HMEM(M)-DP(M))
C
C      COMPUTE STEEL AREAS ABOVE AND BELOW CENTROID OF GROSS SECTION.
C
C      ASTOP = 0.E0
C      ASBOT = 0.E0
C      ASTOT = 0.E0
C      DO 200 I=1,NGRPM
C      ASTOT = ASTOT+AGRP(I,M)
C      IF(HTOP(M)-HMEM(M)/2.E0.GT.YBAR(I,M)) ASBOT = ASBOT+AGRP(I,M)
C      IF(HTOP(M)-HMEM(M)/2.E0.EQ.YBAR(I,M)) ASBOT = ASBOT+AGRP(I,M)/2.E0
C      CONTINUE
C      ASTOP = ASTOT-ASBOT
C
C      CLASSIFY BENDING STATE BY END MOMENTS - - SIX POSSIBLE CONFIGS.
C
C      DENOM = (EBOT8-ETOP8)-(EBOT4-ETOP4)
C
C      RETURN IF SHEAR-FLEXURE FAILURE IS SUBORDINATE TO OTHER CRITERIA
C
C      IF (ABS(DENOM).LE.TINY) GO TO 7000
C      XX = (ETOP4-EBOT4)/DENOM*XL(M)
C      KCH = 1
C      IF (XX.GE.0.E0 .AND. XX.LE.XLEN) GO TO 30
C      KCH = 2
C      CHL = XLEN
C      IF(XX.LE.0.E0.AND.EBOT8.GT.ETOP8) GO TO 11
C      IF(XX.LE.0.E0.AND.EBOT8.LT.ETOP8) GO TO 21

```

```

FAIL3290
FAIL3300
FAIL3310
FAIL3320
FAIL3330
FAIL3340
FAIL3350
FAIL3360
FAIL3370
FAIL3380
FAIL3390
FAIL3400
FAIL3410
FAIL3420
FAIL3430
FAIL3440
FAIL3450
FAIL3460
FAIL3470
FAIL3480
FAIL3490
FAIL3500
FAIL3510
FAIL3520
FAIL3530
FAIL3540
FAIL3550
FAIL3560
FAIL3570
FAIL3580

```



```

C      12 DCHK = D(M)
      DFAC = CHL/DCHK/2.E0-0.5E0
      IF(DFAC.LT.0.5E0) DFAC = 0.5E0
      IF(DFAC.GT.1.5E0) DFAC = 1.5E0
      EMHD = OFAC*DCHK

C      RETURN IF POTENTIAL CRACK IS WITHIN JOINT
C
C      IF(EMHD.LE.XBEGM(M)) GO TO 7000
      XCS = XX-EMHD
      FFOUR(2) = FFOUR
      ASUBS = ASBOT
      FTWO(2) = FTWOBR*ASUBS/XCS
      F(2) = FA
      DO 122 N=1,NTIESM
      IF(XBEGS(N,M).LE.EMHD.AND.EMHD.LE.XBEGS(N,M)+NSPAC(N,M))*
      * STIES(N,M) ASUBV(2) = ATIES(N,M)
      122 CONTINUE
      GO TO 5321

C      LARGER NEGATIVE MOMENT AT RIGHT (Q) END OF ELEMENT . . . .
C      . . . . ZERO MOMENT OUTSIDE SPAN LENGTH
C
C      21 DCHK = HMEM(M)-DP(M)
      DFAC = CHL/DCHK/2.E0-0.5E0
      IF(DFAC.LT.0.5E0) DFAC = 0.5E0
      IF(DFAC.GT.1.5E0) DFAC = 1.5E0
      EMHD = OFAC*DCHK
C

```

```

FAIL3890
FAIL3900
FAIL3910
FAIL3920
FAIL3930
FAIL3940
FAIL3950
FAIL3960
FAIL3970
FAIL3980
FAIL3990
FAIL4000
FAIL4010
FAIL4020
FAIL4030
FAIL4040
FAIL4050
FAIL4060
FAIL4070
FAIL4080
FAIL4090
FAIL4100
FAIL4110
FAIL4120
FAIL4130
FAIL4140
FAIL4150
FAIL4160
FAIL4170
FAIL4180

```

```

C
C
      RETURN IF POTENTIAL CRACK IS WITHIN JOINT
      IF (EMHD.LE.(CHL-EFLM(M)-XBEGM(M))) GO TO 7000
      XCS = CHL-XX-EMHD
      FFOUR(2) = FFOURB
      ASUBS = ASTOP
      FTWO(2) = FTWOBR*ASUBS/XCS
      F(2) = FB
      DO 211 N=1,NTIESM
      IF (XBEGS(N,M).LE.XL(M)-EMHD.AND.XL(M)-EMHD.LE.XBEGS(N,M)+
      * NSPAC(N,M)*STIES(N,M)) ASUBV(2) = ATIES(N,M)
      211 CONTINUE
      GO TO 5321
C
C
      LARGER NEGATIVE MOMENT AT LEFT(P) END OF ELEMENT . . . .
      . . . ZERO MOMENT OUTSIDE SPAN LENGTH
      22 DCHK = HMEM(M)-OP(M)
      DFAC = CHL/DCHK/2.E0-0.5E0
      IF (DFAC.LT.0.5E0) DFAC = 0.5E0
      IF (DFAC.GT.1.5E0) DFAC = 1.5E0
      EMHD = DFAC*DCHK
      RETURN IF POTENTIAL CRACK IS WITHIN JOINT
      IF (EMHD.LE.XBEGM(M)) GO TO 7000
      XCS = XX-EMHD
      FFOUR(2) = FFOURB
      ASUBS = ASTOP
      FTWO(2) = FTWOBR*ASUBS/XCS
      FAIL4190
      FAIL4200
      FAIL4210
      FAIL4220
      FAIL4230
      FAIL4240
      FAIL4250
      FAIL4260
      FAIL4270
      FAIL4280
      FAIL4290
      FAIL4300
      FAIL4310
      FAIL4320
      FAIL4330
      FAIL4340
      FAIL4350
      FAIL4360
      FAIL4370
      FAIL4380
      FAIL4390
      FAIL4400
      FAIL4410
      FAIL4420
      FAIL4430
      FAIL4440
      FAIL4450
      FAIL4460
      FAIL4470
      FAIL4480

```





```

311 CONTINUE
C
C SET FUNCTION VALUES FOR RIGHT PORTION (POSITIVE MOMENT)
C
DCHK = D(M)
CHL = XL(M)-XX
DFAC = CHL/DCHK/2.E0-0.5E0
IF(DFAC.LT.0.5E0) DFAC = 0.5E0
IF(DFAC.GT.1.5E0) DFAC = 1.5E0
EMHD = DFAC*DCHK
C
C SET BYPASS FLAG FOR THIS PORTION IF POTENTIAL CRACK IS WITHIN JOIN
C
C IF(EMHD.LE.XL(M)-EFLM(M)-XBEGM(M)) PASS(2) = .TRUE.
C
C RETURN IF BOTH BYPASS FLAGS HAVE BEEN SET
C
C IF(PASS(1).AND.PASS(2)) GO TO 7000
C
C XCS = CHL-EMHD
C FFOUR(2) = FFOUR
C ASUBS = ASBOT
C FTWO(2) = FTWOBR*ASUBS/XCS
C F(2) = FA
C DO 312 N=1,NTIESM
C IF(XBEGS(N,M).LE.XL(M)-EMHD.AND.XL(M)-EMHD.LE.XBEGS(N,M)+
* NSPAC(N,M)*STIES(N,M)) ASUBV(2) = ATIES(N,M)
312 CONTINUE
GO TO 5321
C
C POSITIVE MOMENT AT LEFT (P) END OF ELEMENT . . . .

```

```

FAIL4790
FAIL4800
FAIL4810
FAIL4820
FAIL4830
FAIL4840
FAIL4850
FAIL4860
FAIL4870
FAIL4880
FAIL4890
JOINFAIL4900
FAIL4910
FAIL4920
FAIL4930
FAIL4940
FAIL4950
FAIL4960
FAIL4970
FAIL4980
FAIL4990
FAIL5000
FAIL5010
FAIL5020
FAIL5030
FAIL5040
FAIL5050
FAIL5060
FAIL5070
FAIL5080

```

```

C      . . . ZERO MOMENT WITHIN SPAN LENGTH
C
C      SET FUNCTION VALUES FOR LEFT PORTION (POSITIVE MOMENT)
C
32  DCHK = D(M)
    CHL = XX
    DFAC = CHL/DCHK/2.E0-0.5E0
    IF(DFAC.LT.0.5E0) DFAC = 0.5E0
    IF(DFAC.GT.1.5E0) DFAC = 1.5E0
    EMHD = DFAC*DCHK

C      SET BYPASS FLAG FOR THIS PORTION IF POTENTIAL CRACK IS WITHIN JOINT
C
C      IF(EMHD.LE.XBEGM(M)) PASS(1) = .TRUE.
C      XCS = CHL-EMHD
C      FFOUR(1) = FFOUR
C      ASUBS = ASBOT
C      FTWO(1) = FTWOBR*ASUBS/XCS
C      F(1) = FA
C      DO 321 N=1,NTIESM
C      IF(XBEGS(N,M).LE.EMHD.AND.EMHD.LE.XBEGS(N,M)+NSPAC(N,M))*
C      * STIES(N,M)) ASUBV(1) = ATIES(N,M)
C      321 CONTINUE
C
C      SET FUNCTION VALUES FOR RIGHT PORTION (NEGATIVE MOMENT)
C
C      DCHK = HMEM(M)-DP(M)
C      CHL = XL(M)-XX
C      DFAC = CHL/DCHK/2.E0-0.5E0
C      IF(DFAC.LT.0.5E0) DFAC = 0.5E0

```

```

FAIL5090
FAIL5100
FAIL5110
FAIL5120
FAIL5130
FAIL5140
FAIL5150
FAIL5160
FAIL5170
FAIL5180
FAIL5190
FAIL5200
FAIL5210
FAIL5220
FAIL5230
FAIL5240
FAIL5250
FAIL5260
FAIL5270
FAIL5280
FAIL5290
FAIL5300
FAIL5310
FAIL5320
FAIL5330
FAIL5340
FAIL5350
FAIL5360
FAIL5370
FAIL5380

```

```

C      IF(DFAC.GT.1.5E0) DFAC = 1.5E0
C      EMHD = DFAC*DCHK
C      SET BYPASS FLAG FOR THIS PORTION IF POTENTIAL CRACK IS WITHIN JOIN
C      IF(EMHD.LE.XL(M)-EFLM(M)-XBEGM(M)) PASS(2) = .TRUE.
C      RETURN IF BOTH BYPASS FLAGS HAVE BEEN SET
C      IF(PASS(1).AND.PASS(2)) GO TO 7000
C      XCS = CHL-EMHD
C      FFOUR(2) = FFOUR3
C      ASUBS = ASTOP
C      FTWO(2) = FTWOBR*ASUBS/XCS
C      F(2) = F8
C      DO 322 N=1,NTIESM
C      IF(XBEGS(N,M).LE.XL(M)-EMHD.AND.XL(M)-EMHD.LE.XBEGS(N,M)+
C      * NSPAC(N,M)*STIES(N,M)) ASUBV(2) = ATIES(N,M)
C      322 CONTINUE
C      SHEAR-FLEXURE CRITERIA
C      5321 IF(ECMIN*ECMAX.GE.0.E0) GO TO 7000
C      DO 400 N=KCH,2
C      IF(PASS(N)) GO TO 400
C      TEMPO = 1.5E0+CC*FTWO(N)
C      TCHK = 3.E0*(7.E0+2.E0*CC)/14.E0
C      IF(TEMPO.GT.TCHK) TEMPO = TCHK
C      FSTAR = TEMPO-ALFA*FFFOUR(N)
C
FAIL5390
FAIL5400
FAIL5410
FAIL5420
FAIL5430
FAIL5440
FAIL5450
FAIL5460
FAIL5470
FAIL5480
FAIL5490
FAIL5500
FAIL5510
FAIL5520
FAIL5530
FAIL5540
FAIL5550
FAIL5560
FAIL5570
FAIL5580
FAIL5590
FAIL5600
FAIL5610
FAIL5620
FAIL5630
FAIL5640
FAIL5650
FAIL5660
FAIL5670
FAIL5680

```



```

C
C      DETECTION OF THE PRINCIPAL DIAGONAL CRACK LEADING TO FAILURE(3.2.1)FAIL5690
      FAIL5700
      IF(NTIESM.GT.0) GO TO 5050
      IF(FSTAR-F(N).GT.0.E0) GO TO 400
      IF(ISTOP.EQ.1) GO TO 5040
      LINE = LINE + 1
      IF (LINE.GT.NL) CALL PAGE
      IFAIL = 1
      PRINT 660, IP(M),IQ(M)
      660 FORMAT( 49H ***PRINCIPAL DIAGONAL CRACK DETECTED IN ELEMENT ,I3,
2      1H-,I3,39H. THE ANALYSIS IS TERMINATED (FAIL).***)
      GO TO 400
      5040 PRINT 670, IP(M),IQ(M)
      670 FORMAT( 49H ** PRINCIPAL DIAGONAL CRACK DETECTED IN ELEMENT ,I3,
2      1H-,I3,39H. THE ANALYSIS IS CONTINUING (FAIL). **)
      GO TO 400
C
C      PRINCIPAL DIAGONAL CRACK PLUS YIELDING OF WEB REINFORCEMENT(3.2.2)FAIL5860
      FAIL5870
      FAIL5880
      FAIL5890
      FAIL5900
      FAIL5910
      FAIL5920
      FAIL5930
      FAIL5940
      FAIL5950
      FAIL5960
      FAIL5970
      2      20HDETECTED IN ELEMENT ,I3,1H-,I3,
      FAIL5980

```

```

CFORK      0 10
SUBROUTINE FORK (J1,I)
C
C SUBROUTINE TO INTERPRET TYPE OF DATA CARD IN BEAM.
C
C THE VALUE OF I IS SET TO INDICATE THE TYPE OF CARD.
C I = 1, ELEMENT PARAMETER CARD.
C I = 2, CONCRETE DATA CARD.
C I = 3, LONGITUDINAL REINFORCEMENT DATA CARD.
C I = 4, STIRRUP DATA CARD.
C I = 5, TIE DATA CARD.
C I = 6, WIDE FLANGE DATA CARD.
C I = 7, LEAF SPRING DATA CARD.
C I = 8, DATA CARD CANNOT BE INTERPRETED.
C I = 9, END CARD OF ELEMENT DATA BLOCK.
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),FORK 140
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)FORK 150
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,FORK 160
1 IREG,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,FORK 170
2 NCRO,NDF,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,FORK 180
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB3,NTAPE,FORK 190
4 NTIMES,NVEL,IINITD,FORK 200
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BDM(10,45),FORK 210
1 BWF(45),D(45),OP(45),OPP(45),DWF(45),EFFL(10,45),EFLM(45),FORK 220
2 HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),FORK 230
3 TFWF(45),TWWF(45),UDM(45),URM(45),X3EG(10,45),FORK 240
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),FORK 250
5 YFIBR(11,45),YLOS(45),XDM(45),PDF(7,45),DISM(45)FORK 260
DATA IA,IB,IC,ID,IE,IF/4H ,4HBARS,4HSTIR,4HTIES,4HWFST,4HLEAF/ FORK 270
FORK 280

```

```

CFITS 0 10
SUBROUTINE FITS (STEP, FVAL, DSTEP, AVAL, I)
C
C THIS SUBROUTINE FITS A PARABOLIC CURVE TO OBTAIN A BETTER ESTIMATE
C OF THE LOCATION OF THE MINIMUM.
C
C DIMENSION STEP(4), FVAL(4), DSTEP(4)
C
C STEP(1)= STEP(I+1) - STEP(I+2)
C STEP(3)=STEP(I+3)-STEP(I+2)
C DF1=DSTEP(1)*(FVAL(I+3)-FVAL(I+2))
C DF3=DSTEP(3)*(FVAL(I+1)-FVAL(I+2))
C DF=DF1-DF3
C IF (DF.EQ.0.E0) GO TO 20
C DSTEP(2)=.5E0*(DSTEP(1)*DF1-DSTEP(3)*DF3)/(DF1-DF3)
C AVAL=(DF3-DF1)*SIGN(1.E0,DSTEP(1))*SIGN(1.E0,DSTEP(3))*SIGN(1.E0,
1 DSTEP(1)-DSTEP(3))
C GO TO 30
C DSTEP(2)=.5E0*(DSTEP(1)+DSTEP(3))
C AVAL=0.E0
C RETURN
C END
FITS 0
FITS 10
FITS 20
FITS 30
FITS 40
FITS 50
FITS 60
FITS 70
FITS 80
FITS 90
FITS 100
FITS 110
FITS 120
FITS 130
FITS 140
FITS 150
FITS 160
FITS 170
FITS 180
FITS 190
FITS 200

```

```

+ 39H. THE ANALYSIS IS TERMINATED (FAIL).***)
  GO TO 400
5060 PRINT 690, IP(M), IQ(M)
690 FORMAT( 53H ** PRINCIPAL DIAGONAL CRACK PLUS WEB STEEL YIELDING ,
2      20HDETECTED IN ELEMENT ,I3,1H-,I3,
+ 39H. THE ANALYSIS IS CONTINUING (FAIL). **)
400 CONTINUE
7000 CONTINUE
      RETURN
      END

FAIL5990
FAIL6000
FAIL6010
FAIL6020
FAIL6030
FAIL6040
FAIL6050
FAIL6060
FAIL6070
FAIL6080

```



```

10      DATA IG/4H0000/
      I=8
      IF (J1.EQ.IA) I=1
      IF (J1.EQ.IB) I=3
      IF (J1.EQ.IC) I=4
      IF (J1.EQ.ID) I=5
      IF (J1.EQ.IE) I=6
      IF (J1.EQ.IF) I=7
      IF (J1.EQ.IG) I=9
      IF (I.NE.8) GO TO 30
      CALL MATY (J1,MATN)
      IF (MATN.NE.0) GO TO 20
      IF (LINE.GT.NL) CALL PAGE
      IERR=IERR+1
      LINE=LINE+1
      FORMAT (1H,30H**FIRST WORD OF ELEMENT CARD ,I3,1H,,A4,60H IS NEIFORK 440
      1  EITHER A COMPONENT TYPE NOR A MATERIAL NAME (FORK)*** )
      PRINT 10, ICARD,J1
      GO TO 30
      I=2
      RETURN
      END
20
30

```

```

FORK 290
FORK 300
FORK 310
FORK 320
FORK 330
FORK 340
FORK 350
FORK 360
FORK 370
FORK 380
FORK 390
FORK 400
FORK 410
FORK 420
FORK 430
FORK 440
FORK 450
FORK 460
FORK 470
FORK 480
FORK 490
FORK 500

```

```

CFORS      0 10
C          SUBROUTINE FORS (T)
C          THIS SUBROUTINE EVALUATES THE JOINT FORCING FUNCTIONS AT A SPECIFIC
C          COMMON DATA(10000),KDATA(500)
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),DIS(3,50),ERJF(3,50),
1  ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
2  XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CE,DHEAD(20),DT,EPS,HEAD(20),
1  PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,
1  IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,
2  NCRD,NDF,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,
3  NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRI,NSAVE,NTAB,NTAPE,
4  NTIMES,NVEL
COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB,
1  LTABI,NMAX,NMAXI
C          INTEGER HEAD,DHEAD
C          INITIALIZE STORAGE LOCATIONS
DO 20 K=1,3
DO 20 J=1,NJD
F(K,J)=0.0E0
DO 90 I=1,NFF
C          DETERMINE DATA STORAGE LOCATIONS
LLL=LFF+4*(I-1)
FORS      0
FORS     10
FORS     20
FORS     30
FORS     40
FORS     50
FORS     60
FORS     70
FORS     80
FORS     90
FORS    100
FORS    110
FORS    120
FORS    130
FORS    140
FORS    150
FORS    160
FORS    170
FORS    180
FORS    190
FORS    200
FORS    210
FORS    220
FORS    230
FORS    240
FORS    250
FORS    260
FORS    270
FORS    280

```







FORS 890  
 FORS 900  
 FORS 910  
 FORS 920  
 FORS 930  
 FORS 940  
 FORS 950  
 FORS 960  
 FORS 970  
 FORS 980  
 FORS 990  
 FORS1000  
 FORS1010

F(2,JL)=F(2,JL)+FJL\*DX/XLM  
 F(3,JL)=F(3,JL)+W\*XLM/10.E0  
 F(1,JR)=F(1,JR)-FJR\*DY/XLM  
 F(2,JR)=F(2,JR)+FJR\*DX/XLM  
 F(3,JR)=F(3,JR)-W\*XLM/15.E0  
 GO TO 90

STORE VALUE OF JOINT FORCING FUNCTION

F(KK,JL)=F(KK,JL)+VALUE\*A+B  
 CONTINUE  
 RETURN  
 END

C  
 C  
 C  
 80  
 90

```

CFTAB 0 10
      SUBROUTINE FTAB
C
C      THIS SUBROUTINE READS FROM CARDS AND ERROR CHECKS DATA INPUT TO THFTAB
C      FUNCTION TABLES DATA BLOCK
C
      COMMON DATA(10000),KDATA(500)
      COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1      PI,REF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
      INTEGER HEAD,DHEAD
      COMMON/MAINBK/IBODY,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,FTAB 0
1      IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,FTAB 10
2      NCRO,NDF,NDFD,NDFJ,NDIS,NDL,NFF,NJOR,NJ,NJD,NJER,NL,NLD,FTAB 20
3      NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,FTAB 30
4      NTIMES,NVEL,IINITD
      COMMON/SCALE/EGSIF,EGSIL
      COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB,FTAB 40
1      LTABI,NMAX,NMAXI
C
      DIMENSION ADATA(6),BDATA(6),DP(6)
C
      INITIALIZE VARIABLES USED IN THIS SUBROUTINE
C
      I=0
      J=0
      JERR=0
      KERR=0
      IUNIT=IUNITS
      IERR=IERR
      NTAB=0
      FTAB 50
      FTAB 60
      FTAB 70
      FTAB 80
      FTAB 90
      FTAB 100
      FTAB 110
      FTAB 120
      FTAB 130
      FTAB 140
      FTAB 150
      FTAB 160
      FTAB 170
      FTAB 180
      FTAB 190
      FTAB 200
      FTAB 210
      FTAB 220
      FTAB 230
      FTAB 240
      FTAB 250
      FTAB 260
      FTAB 270
      FTAB 280

```

	LTAB=LCURV+NDF*(NDF+1)/2	FTAB 290
	LFF=LTAB	FTAB 300
	LMAXI=LFFI+2	FTAB 310
	XEGSIF = 1.E0/EGSIF	FTAB 320
		FTAB 330
	CHECK FOR AVAILABILITY OF STORAGE TO STORE FIRST SET OF DATA	FTAB 340
	IF (LMAXI.GT.NMAXI) GO TO 170	FTAB 350
		FTAB 360
	READ BLOCK 7 TITLE CARD.	FTAB 370
	READ (NCRD,10) DHEAD	FTAB 380
	FORMAT (20A4)	FTAB 390
10		FTAB 400
C		FTAB 410
C		FTAB 420
C	READ BLOCK 7, CARD 2 (NONE REQUIRED).	FTAB 430
C		FTAB 440
20	FORMAT (I4,6X,6E10.0)	FTAB 450
C	READ (NCRD,20) IA,(ADATA(M),M=1,6)	FTAB 460
C	CHECK FOR NO INPUT DATA TO DATA BLOCK	FTAB 470
C	IF (IA.EQ.0) GO TO 610	FTAB 480
30	II=I+1	FTAB 490
C		FTAB 500
C	CHECK SEQUENCE OF DATA TABLE NUMBERS	FTAB 510
	IF (IA.EQ.II) GO TO 40	FTAB 520
	IERR=IERR+1	FTAB 530
	JERR=1	FTAB 540
	GO TO 200	FTAB 550
		FTAB 560
C	READ BLOCK 7, CARD 3 TYPE	FTAB 570
C	READ (NCRD,20) IB,(BDATA(M),M=1,6)	FTAB 580
40		

C	K=0	FTAB 590
C	CHECK TO SEE IF LAST DATA CARD READ IS A CONTINUATION OF SAME FUNC	FTAB 600
	IF (IA.EQ.IB) GO TO 60	FTAB 610
	K=1	FTAB 620
C	COUNT DATA POINTS ON CARD	FTAB 630
C	00 50 M=3,5,2	FTAB 640
	IF (ADATA(M).EQ.0.E0.AND.ADATA(M+1).EQ.0.E0) GO TO 70	FTAB 650
50	K=K+1	FTAB 660
	GO TO 70	FTAB 670
60	K=3	FTAB 680
70	KK=2*K	FTAB 690
	LMAX=LFF+KK	FTAB 700
C	CHECK FOR AVAILABLE STORAGE	FTAB 710
C	IF (LMAX.LE.NMAX) GO TO 110	FTAB 720
	IERR=IERR+1	FTAB 730
	KERR=1	FTAB 740
	IF (IB.EQ.0) GO TO 100	FTAB 750
C	IF STORAGE NOT AVAILABLE, READ REMAINING CARDS IN DATA BLOCK	FTAB 760
C	FORMAT (I5)	FTAB 770
80	READ (NCRD,80) IB	FTAB 780
90	IF (IB.NE.0) GO TO 90	FTAB 790
100	IF (J.GT.0) GO TO 150	FTAB 800
	GO TO 200	FTAB 810
110	J=J+K	FTAB 820
C	MAKE SI,ENGLISH CONVERSIONS.	FTAB 830
C		FTAB 840
		FTAB 850
		FTAB 860
		FTAB 870
		FTAB 880



	00 120 M=2,6,2		FTAB 890
120	ADATA(M) = ADATA(M)*EGSIF		FTAB 900
C			FTAB 910
C	STORE DATA		FTAB 920
	00 620 M=1, KK		FTAB 930
620	DATA(LFF+M)=ADATA(M)		FTAB 940
	LFF=LFF+KK		FTAB 950
C			FTAB 960
C	CHECK FOR NEW FUNCTION TABLE		FTAB 970
	IF (IA.NE.IB) GO TO 150		FTAB 980
C			FTAB 990
C	TRANSFER DATA FROM LAST DATA CARD READ		FTAB1000
	00 140 M=1,6		FTAB1010
140	ADATA(M)=8DATA(M)		FTAB1020
C			FTAB1030
C	RETURN TO READ NEXT DATA CARD		FTAB1040
	GO TO 30		FTAB1050
C			FTAB1060
C	INCREMENT FUNCTION TABLE COUNTER		FTAB1070
150	I=I+1		FTAB1080
	KDATA(LFFI+1)=LFF-2*J+1		FTAB1090
	KDATA(LFFI+2)=J		FTAB1100
	LFFI=LFFI+2		FTAB1110
	IF (IB.EQ.0) GO TO 200		FTAB1120
	J=0		FTAB1130
C			FTAB1140
C	TRANSFER DATA FROM LAST DATA CARD READ		FTAB1150
	IA=IB		FTAB1160
	00 160 M=1,6		FTAB1170
160	ADATA(M)=8DATA(M)		FTAB1180

C	LMAXI=LFFI+2	FTAB1190
C	CHECK FOR AVAILABILITY OF STORAGE	FTAB1200
	IF (LMAXI.LE.NMAXI) GO TO 30	FTAB1210
170	IERR=IERR+1	FTAB1220
	LERR=1	FTAB1230
	IF (IB.EQ.0) GO TO 200	FTAB1240
C		FTAB1250
C	IF STORAGE NOT AVAILABLE, READ REMAINING CARDS IN DATA BLOCK	FTAB1260
180	READ (NCRO,190) IB	FTAB1270
190	FORMAT (I5)	FTAB1280
	IF (IB.NE.0) GO TO 180	FTAB1290
C		FTAB1300
C	SET NUMBER OF FUNCTION TABLES INPUT	FTAB1310
200	NTAB=I	FTAB1320
C		FTAB1330
C	INITIALIZE OUTPUT COUNTER	FTAB1340
210	I=0	FTAB1350
C		FTAB1360
C	IF NO OUTPUT REQUIRED, SKIP DATA OUTPUT SECTION	FTAB1370
	IF (IPRINT.EQ.0) GO TO 240	FTAB1380
C		FTAB1390
	PRINT PROBLEM DESCRIPTION AND PAGE NUMBER	FTAB1400
C	PRINT TABLE HEADING	FTAB1410
C	CALL PAGE	FTAB1420
220	FORMAT (1H,20A4)	FTAB1430
	WRITE (NPRT,220) DHEAD	FTAB1440
230	FORMAT (1H0,50X,15HFUNCTION TABLES/)	FTAB1450
	WRITE (NPRT,230)	FTAB1460
	LINE=LINE+2	FTAB1470
		FTAB1480

C				FTA31490
C		CHECK FOR NO DATA STORED		FTAB1500
240		IF (NTAB.EQ.0) GO TO 550		FTAB1510
C				FTAB1520
C		INCREMENT OUTPUT COUNTER		FTAB1530
250		I=I+1		FTAB1540
		K=KDATA(LTAB1+2*I-1)		FTAB1550
		J=KDATA(LTAB1+2*I)		FTAB1560
C				FTAB1570
C		IF NO OUTPUT REQUIRED, SKIP DATA OUTPUT SECTION		FTAB1580
		IF (IPRINT.EQ.0) GO TO 310		FTAB1590
		LINE = LINE + 5		FTAB1600
		IF (LINE.LT.NL) GO TO 270		FTAB1610
		CALL PAGE		FTAB1620
		WRITE (NPRT,230)		FTAB1630
		LINE=LINE+2		FTAB1640
C				FTAB1650
C		OUTPUT HEADINGS		FTA31660
260		FORMAT (1H0,9X,18HFUNCTION TABLE NO.,15,10X,16HNUMBER OF POINTS,15)		FTAB1670
270		WRITE (NPRT,260) I, J		FTA31680
C				FTA31690
C		OUTPUT METRIC UNITS		FTAB1700
280		FORMAT (/ ,1H ,3(7X,8HTIME (S),8X,11HFORCE (N) ),/)		FTAB1710
		IF (IIUNIT.GE.2) WRITE (NPRT,280)		FTA31720
C				FTAB1730
C		OUTPUT ENGLISH UNITS		FTAB1740
290		FORMAT (/ ,1H ,3(7X,8HTIME (S),8X,11HFORCE (LB) ),/)		FTAB1750
		IF (IIUNIT.LE.1) WRITE (NPRT,290)		FTAB1760
C				FTA31770
C		PREPARE DATA FOR OUTPUT		FTAB1780

FTAB1790  
FTAB1800  
FTAB1810  
FTAB1820  
FTAB1830  
FTAB1840  
FTAB1850  
FTAB1860  
FTAB1870  
FTAB1880  
FTAB1890  
FTAB1900  
FTAB1910  
FTAB1920  
FTAB1930  
FTAB1940  
FTAB1950  
FTAB1960  
FTAB1970  
FTAB1980  
FTAB1990  
FTAB2000  
FTAB2010  
FTAB2020  
FTAB2030  
FTAB2040  
FTAB2050  
FTAB2060  
FTAB2070  
FTAB2080

```

310 JJ=J*2
    KK=K-1
320 N=6
    IF (JJ.LT.6) N=JJ
    DO 330 M=1,N
330 DP(M)=DATA(KK+M)
    C
    C CONVERT OUTPUT DATA UNITS IF NECESSARY.
    DO 340 M=2,N,2
340 DP(M) = DP(M)*XEGSIF
    C IF NO OUTPUT UNITS REQUIRED, SKIP DATA OUTPUT SECTION
    IF (IPRINT.EQ.0) GO TO 370
    C
    C OUTPUT DATA
    C
360 FORMAT (6(5X,1PE12.5))
    WRITE (NPRT,360) (DP(M),M=1,N)
    LINE=LINE+1
370 IF (JJ.LE.6) GO TO 410
    IF (IPRINT.EQ.0) GO TO 400
    IF (LINE.LT.NL) GO TO 400
    CALL PAGE
    WRITE (NPRT,230)
    WRITE (NPRT,260) I,J
    IF (IIUNIT.LE.1) WRITE (NPRT,290)
    IF (IIUNIT.GE.2) WRITE (NPRT,280)
    LINE = LINE + 5
400 KK=KK+6
    JJ=JJ-6
    GO TO 320

```



```

C
C
410
C
C
420
430
440
C
450
C
460
470
480
490
C
C

      CHECK FOR ERRORS AND OUTPUT ERROR MESSAGES
      L=KDATA(LTABI+2*I-1)
      LL=L+2*KDATA(LTABI+2*I)-2
      DO 420 M=L,LL,2

      CHECK FOR NEGATIVE TIME INPUT
      IF (DATA(M).LT.0.E0) GO TO 430
      CONTINUE
      GO TO 490
      IERR=IERR+1
      FORMAT (1H,42H*** VALUE OF TIME INPUT FOR FUNCTION TABLE,15,26H
1 IS NEGATIVE (FTAB). ***)
      PRINT 440, I
      ITAG=1
      LINE=LINE+1
      IF (LINE.LT.NL) GO TO 480
      CALL PAGE
      IF (IPRINT.EQ.0) GO TO 490
      WRITE (NPRT,230)
      WRITE (NPRT,260) I,J
      IF (IIUNIT.EQ.0.OR.IIUNIT.EQ.1) GO TO 460
      WRITE (NPRT,280)
      GO TO 470
      WRITE (NPRT,290)
      LINE=LINE+5
      GO TO (490,530,570,590,610), ITAG
      L=KDATA(LTABI+2*I-1)+2

      CHECK FOR NEGATIVE TIME STEP IN TABLE

```

```

FTAB2090
FTAB2100
FTAB2110
FTAB2120
FTAB2130
FTAB2140
FTAB2150
FTAB2160
FTAB2170
FTAB2180
FTAB2190
FTAB2200
FTAB2210
FTAB2220
FTAB2230
FTAB2240
FTAB2250
FTAB2260
FTAB2270
FTAB2280
FTAB2290
FTAB2300
FTAB2310
FTAB2320
FTAB2330
FTAB2340
FTAB2350
FTAB2360
FTAB2370
FTAB2380

```



AD-A038 317

VIRGINIA POLYTECHNIC INST AND STATE UNIV BLACKSBURG --ETC F/6 13/13  
RELIABILITY STUDY OF SINGER. VOLUME II. USER'S MANUAL.(U)

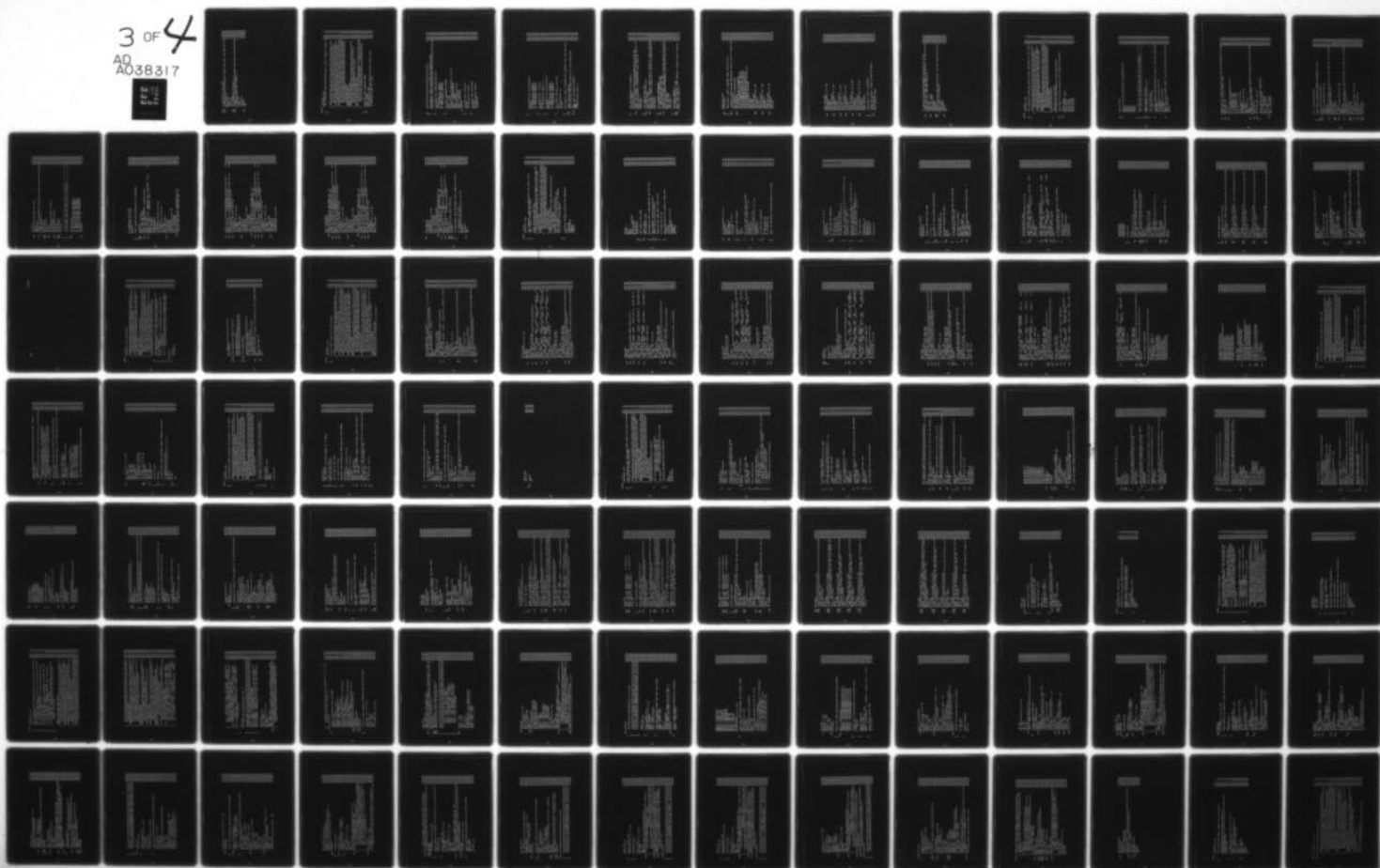
JAN 77 A E SOMERS, S M HOLZER, J C BRADSHAW F29601-75-C-0050

AFWL-TR-76-192-VOL-2

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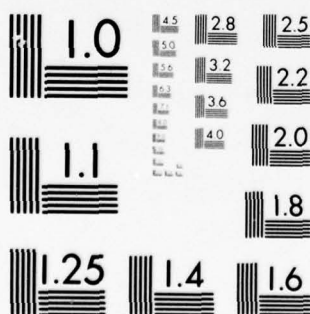
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570 IF (KERR.EQ.0) GO TO 590
580 FORMAT (1H ,68H***INSUFFICIENT STORAGE AVAILABLE FOR FUNCTION TABL
      1ES (FTAB).**
      PRINT 580
      ITAG=4
      GO TO 450
590 IF (LERR.EQ.0) GO TO 610
600 FORMAT (1H ,84H***INSUFFICIENT STORAGE AVAILABLE FOR FUNCTION TABL
      1E IDENTIFICATION DATA (FTAB).**
      PRINT 600
      ITAG=5
      GO TO 450
      RETURN
      END
      FTAB2690
      FTAB2700
      FTAB2710
      FTAB2720
      FTAB2730
      FTAB2740
      FTAB2750
      FTAB2760
      FTAB2770
      FTAB2780
      FTAB2790
      FTAB2800
      FTAB2810
      FTAB2820

```



20	FORMAT(I5,2(A2,3X),A1,4X,2A1,3X,A1,4X,I5,A1)	GIDE 290
C		GIDE 300
C	READ BLOCK 1, CARD 2 OF CONTROL DATA (REQUIRED CARD).	GIDE 310
C	READ(NCRD,20) ISTART,UNITS,SLIN,ISTOP,PRINT,PAGEN,STRES,ITAPE,PLOT	GIDE 320
C		GIDE 330
C	SET IUNITS FLAG. 0=EE,1=ES,2=SS,3=SE	GIDE 340
	IUNITS = 0	GIDE 350
	IF (UNITS.EQ.ES) IUNITS=1	GIDE 360
	IF (UNITS.EQ.SS) IUNITS=2	GIDE 370
	IF (UNITS.EQ.SE) IUNITS=3	GIDE 380
C		GIDE 390
C	SET UNITS CONVERSION FACTORS.	GIDE 400
	EGSIF = 1.E0	GIDE 410
	EGSIL = 1.E0	GIDE 420
	IF(IUNITS.EQ.0.OR.IUNITS.EQ.2) GO TO 40	GIDE 430
	EGSIF = 4.4482216152605E0	GIDE 440
	EGSIL = .0254E0	GIDE 450
	IF(IUNITS.EQ.1) GO TO 40	GIDE 460
	EGSIF = 1.E0/EGSIF	GIDE 470
	EGSIL = 1.E0/EGSIL	GIDE 480
	40 CONTINUE	GIDE 490
C		GIDE 500
C	SET ILIN FLAG. 0=II,1=FI.	GIDE 510
	ILIN=0	GIDE 520
	IF (SLIN.EQ.FI) ILIN=1	GIDE 530
C		GIDE 540
C	SET ISTOP FLAG. 0=C,1=STOP	GIDE 550
	IFLAG=1	GIDE 560
	IF (ISTOP.EQ.CF) IFLAG=0	GIDE 570
	ISTOP=IFLAG	GIDE 580

C	SET IPRINT FLAG. 0=M,1=S,2=0,3=E	GIDE 590
C	IPRINT=1	GIDE 600
	IF (PRINT.EQ.SM) IPRINT=0	GIDE 610
	IF (PRINT.EQ.DM) IPRINT=2	GIDE 620
	IF (PRINT.EQ.EM) IPRINT=3	GIDE 630
C		GIDE 640
C	SET MPRINT FLAG. 0=M,1=S.	GIDE 650
	MPRINT = 1	GIDE 660
	IF (PAGEM.EQ.SM) MPRINT = 0	GIDE 670
C		GIDE 680
C	SET ISTRES FLAG. 0=N,1=S,2=R,3=B	GIDE 690
	ISTRES=0	GIDE 700
	IF (ISTRES.EQ.TS) ISTRES=1	GIDE 710
	IF (ISTRES.EQ.SR) ISTRES=2	GIDE 720
	IF (ISTRES.EQ.BB) ISTRES=3	GIDE 730
C		GIDE 740
C	SET IPLOT=0, NO PLOT,, =1, PLOT.	GIDE 750
	N=0	GIDE 760
	IF (PLOT.EQ.SR) N=1	GIDE 770
	IPLOT=N	GIDE 780
C		GIDE 790
C	READ BLOCK 1, CARD 3 SOLUTION DATA (REQUIRED CARD) AND TEST DATA.	GIDE 800
C		GIDE 810
C	FORMAT (A1,7X,I2,5E10.0)	GIDE 820
220	READ (NCRD,220) ANAL,IINITD,TBEGIN,THALT,TINK,SERR,TPROB	GIDE 830
C		GIDE 840
C	SET IANAL FLAG. (0=STATIC,1=DYNAMIC)	GIDE 850
	IANAL = 0	GIDE 860
	IF (ANAL.EQ.DM) IANAL = 1	GIDE 870
		GIDE 880





```

300 PRINT 290, TINK
C DISACC=SERR
C READ BLOCK 1, CARD 4 (REQUIRED CARD) AND TEST DATA.
C
320 FORMAT(1H, 23H** FAILURE COEFFICIENT ,A2,25H IS OUT OF RANGE, SET
1 TO ,E9.2,3H**)
READ (NCRD,221) CA,CB,CC,CD,CE
221 FORMAT(5E10.0)
C SET DEFAULT VALUES IF NECESSARY
IF(CA.EQ.8888.OR.CA.EQ.0.E0) CA=1.E0
IF(CB.EQ.8888.OR.CB.EQ.0.E0) CB=2.E0
IF(CC.EQ.8888.OR.CC.EQ.0.E0) CC=3.5E0
IF(CD.EQ.8888.OR.CD.EQ.0.E0) CD=0.E0
IF(CE.EQ.8888.OR.CE.EQ.0.E0) CE=4.E0/3.E0
IF(CA.LE.1.23E0) GO TO 322
IREC=IREC+1
CA=1.23E0
322 PRINT 320,AC,CA
IF(CA.GE.1.E0) GO TO 324
IREC=IREC+1
CA=1.E0
324 PRINT 320,AC,CA
IF(CB.LE.4.E0) GO TO 326
IREC=IREC+1
CB=4.E0
326 PRINT 320,BC,CB
IF(CB.GE.1.E0) GO TO 328
IREC=IREC+1
CB=1.E0

```

GIDE1190  
GIDE1200  
GIDE1210  
GIDE1220  
GIDE1230  
GIDE1240  
GIDE1250  
GIDE1260  
GIDE1270  
GIDE1280  
GIDE1290  
GIDE1300  
GIDE1310  
GIDE1320  
GIDE1330  
GIDE1340  
GIDE1350  
GIDE1360  
GIDE1370  
GIDE1380  
GIDE1390  
GIDE1400  
GIDE1410  
GIDE1420  
GIDE1430  
GIDE1440  
GIDE1450  
GIDE1460  
GIDE1470  
GIDE1480

328	PRINT 320,8C,CB	GIDE1490
	IF(CC.LE.5.83E0) GO TO 330	GIDE1500
	IREC=IREC+1	GIDE1510
	CC=5.83E0	GIDE1520
330	PRINT 320,CCC,CC	GIDE1530
	IF(CC.GE.3.5E0) GO TO 332	GIDE1540
	IREC=IREC+1	GIDE1550
	CC=3.5E0	GIDE1560
332	PRINT 320,CCC,CC	GIDE1570
	IF(CD.LE.1.E0) GO TO 334	GIDE1580
	CD=1.E0	GIDE1590
334	PRINT 320,DC,CD	GIDE1600
	IF(CD.GE.0.E0) GO TO 336	GIDE1610
	IREC=IREC+1	GIDE1620
	CD=0.E0	GIDE1630
336	PRINT 320,DC,CD	GIDE1640
	IF(CE.LE.4.E0/3.E0) GO TO 338	GIDE1650
	IREC=IREC+1	GIDE1660
	CE=4.E0/3.E0	GIDE1670
338	PRINT 320,EC,CE	GIDE1680
	IF(CE.GE.4.E0/7.E0) GO TO 340	GIDE1690
	IREC=IREC+1	GIDE1700
	CE=4.E0/7.E0	GIDE1710
	PRINT 320,EC,CE	GIDE1720
C	READ BLOCK 1, CARD 5 (REQUIRED).	GIDE1730
C		GIDE1740
C		GIDE1750
C	SEARCH FOR A BLANK ^ ASSUME IT ENDS THE BLOCK.	GIDE1760
340	DO 380 I=1,100	GIDE1770
	READ (NCRD,10) OHEAD	GIDE1780

350	IF ((DHEAD(1).EQ.8888).OR.(DHEAD(1).EQ.ZZZZ)) GO TO 400	GIDE1790
	FORMAT (95H **AT LEAST ONE CARD IS OUT-OF-SORT. THE NEXT CARD WAS	GIDE1800
	1 EXPECTED TO BE A ZERO CARD (GIDE).*** )	GIDE1810
	PRINT 350	GIDE1820
370	FORMAT (1H ,20A4)	GIDE1830
	PRINT 370, DHEAD	GIDE1840
	IERR=IERR+1	GIDE1850
380	CONTINUE	GIDE1860
390	FORMAT (84H ***A ZEROS CARD FOR BLOCK 1 WAS NOT FOUND AFTER 100 CAGIDE1870	GIDE1880
	1RDS HAD BEEN READ (GIDE)*** )	GIDE1890
	PRINT 390	GIDE1900
	IERR=IERR+1	GIDE1910
400	RETURN	GIDE1920
	END	





```

20      BET(K,J)=TINY
C
C      FOR(K,J) AND IFOR INITIALIZED IN SUBROUTINE BODY.
C      NINC=0
C      JERR=0
C      NDIS=0
C      NVEL=0
C      NACC=0
C      NJER=0
C      NJOR=0
C
C      * * * * *
C      READ JOINT NO. AND INITIAL CONDITION TYPE AND COMPONENT.
C      * * * * *
C      FORMAT (I5,A1,4X,3E10.0)
C      READ (NCRD,30) J,L,(A(I),I=1,3)
C
C      TEST FOR LAST CARD.
C      IF (J.EQ.0) GO TO 340
C
C      INCREMENT COUNTER AND CHECK RANGE OF JOINT NO. AND TYPE INDICATOR.
C      NINC=NINC+1
C      IF (J.GE.1.AND..J.LE.NJ) GO TO 80
C      IERR=IERR+1
C      IF (JERR.EQ.1) GO TO 70
C      CALL PAGE
C      FORMAT (1H,10X,44HINPUT ERRORS IN INITIAL CONDITION DATA BLOCK//)
C      WRITE (NPRT,50)
C      JERR=1
C
50      INIT 290
C      INIT 300
C      INIT 310
C      INIT 320
C      INIT 330
C      INIT 340
C      INIT 350
C      INIT 360
C      INIT 370
C      INIT 380
C      INIT 390
C      INIT 400
C      INIT 410
C      INIT 420
C      INIT 430
C      INIT 440
C      INIT 450
C      INIT 460
C      INIT 470
C      INIT 480
C      INIT 490
C      INIT 500
C      INIT 510
C      INIT 520
C      INIT 530
C      INIT 540
C      INIT 550
C      INIT 560
C      INIT 570
C      INIT 580

```

```

60  FORMAT (14H *** JOINT NO.,15,50H LESS THAN ONE OR GREATER THAN LARINIT 590
70  1GEST JOINT NO. =,14,12H (INIT). ***/)
80  PRINT 60, J,NJ
    GO TO 40
    LA = 0
    IF (L.EQ.ND(5).OR.L.EQ.ND(6)) LA=1
    IF (L.EQ.ND(1)) LA=2
    IF (L.EQ.ND(2)) LA=3
    IF (L.EQ.ND(3)) LA=4
    IF (L.EQ.ND(4)) LA=5
    L=LA
    IF (L.NE.0) GO TO 110
    IERR=IERR+1
    IF (JERR.EQ.1) GO TO 100
    CALL PAGE
    WRITE (NPRT,50)
    JERR=1
90  FORMAT (1H ,26H*** INITIAL CONDITION TYPE,15,9H AT JOINT,15,27H NOINIT 760
100  1T ACCEPTABLE (INIT). ***)
110  PRINT 90, L,J
    GO TO 40
    IF (NJ.GT.NJD) GO TO 40
C
C  CHANGE UNITS OF INITIAL CONDITIONS.
    IF (L.EQ.5) GO TO 120
    A(1) = A(1)*EGSIL
    A(2) = A(2)*EGSIL
    GO TO 130
120  A(1) = A(1)*EGSIF
    A(2) = A(2)*EGSIF
    INIT 600
    INIT 610
    INIT 620
    INIT 630
    INIT 640
    INIT 650
    INIT 660
    INIT 670
    INIT 680
    INIT 690
    INIT 700
    INIT 710
    INIT 720
    INIT 730
    INIT 740
    INIT 750
    INIT 760
    INIT 770
    INIT 780
    INIT 790
    INIT 800
    INIT 810
    INIT 820
    INIT 830
    INIT 840
    INIT 850
    INIT 860
    INIT 870
    INIT 880

```

C	A(3) = A(3)*(EGSIF*EGSIL)	INIT 890
C	STORE INITIAL CONDITION COMPONENT ACCORDING TO TYPE.	INIT 900
C		INIT 910
130	GO TO (140,180,220,260,300), L	INIT 920
140	IFOR=1	INIT 930
	IF (DIS(1,J).EQ.TINY) GO TO 160	INIT 940
	JERR=1	INIT 950
	IERR=IERR+1	INIT 960
150	FORMAT (1H,12H***JOINT NO.,I5,60H HAS MORE THAN ONE SET OF INITIAL	INIT 970
	1L DISPLACEMENTS (INIT).*** )	INIT 980
	PRINT 150, J	INIT 990
160	DO 170 I=1,3	INIT 1000
170	DIS(I,J)=A(I)	INIT 1010
	GO TO 40	INIT 1020
180	IF (VEL(1,J).EQ.TINY) GO TO 200	INIT 1030
	JERR=1	INIT 1040
	IERR=IERR+1	INIT 1050
190	FORMAT (1H,12H***JOINT NO.,I5,60H HAS MORE THAN ONE SET OF INITIAL	INIT 1060
	1L VELOCITIES (INIT).*** )	INIT 1070
200	PRINT 190, J	INIT 1080
210	DO 210 I=1,3	INIT 1090
	VEL(I,J)=A(I)	INIT 1100
	GO TO 40	INIT 1110
220	IF (ACC(1,J).EQ.TINY) GO TO 240	INIT 1120
	DO 230 I=1,3	INIT 1130
230	ACC(I,J)=A(I)+ACC(I,J)	INIT 1140
	GO TO 40	INIT 1150
240	DO 250 I=1,3	INIT 1160
250	ACC(I,J)=A(I)	INIT 1170
		INIT 1180





```

C
C
C
360 IF (JERR.NE.0) GO TO 670
370 IF (NINC.EQ.0) GO TO 670
    NPAGE=1
    PRINT HEADING WITH EITHER EQ OR SI DIMENSIONS
    CALL PAGE
    FORMAT (1H,20A4,/)
    WRITE (NPRT,370) OHEAD
    FORMAT (1H,33X,24HINITIAL CONDITION DATA /)
    WRITE (NPRT,380)
380
390 FORMAT (1H,92H JOINT CONDITION TYPE X COMPONENT UNITS
10COMPONENT UNITS Z COMPONENT UNITS /)
    WRITE (NPRT,390)
    DO 660 J=1,NJ
    IN=NPAGE*IUNITS
    ILINE=LINE
    IF (DIS(1,J).EQ.TINY) GO TO 440
    LINE=LINE+1
    IF (LINE.LT.NL) GO TO 400
    CALL PAGE
    WRITE (NPRT,390)
    A(1)=DIS(1,J)
    A(2)=DIS(2,J)
    A(3)=DIS(3,J)
    IF(NPAGE.EQ.2) GO TO 430
    A(1) = A(1)/EGSIL
    A(2) = A(2)/EGSIL
    430 IF(IN.GE.2.AND.IN.LE.4) WRITE(NPRT,410) J,A
    IF(IN.LT.2.OR.IN.GT.4) WRITE(NPRT,420) J, /
INIT1490
INIT1500
INIT1510
INIT1520
INIT1530
INIT1540
INIT1550
INIT1560
INIT1570
INIT1580
INIT1590
Y CINIT1600
INIT1610
INIT1620
INIT1630
INIT1640
INIT1650
INIT1660
INIT1670
INIT1680
INIT1690
INIT1700
INIT1710
INIT1720
INIT1730
INIT1740
INIT1750
INIT1760
INIT1770
INIT1780

```

```

410      FORMAT (1H ,I5,2X,14H DISPLACEMENT ,2X,0PE12.5,2X,10H M
1E12.5,1X,9H M      ,2X,0PE12.5,2X,9H RAD )
420      FORMAT (1H ,I5,2X,14H DISPLACEMENT ,2X,0PE12.5,2X,10H IN.
1E12.5,1X,9H IN.      ,2X,0PE12.5,2X,9H RAD )
440      IF (VEL(1,J).EQ.TINY) GO TO 490
        LINE=LINE+1
        IF (LINE.LT.NL) GO TO 450
        CALL PAGE
        WRITE (NPRT,390)
450      A(1)=VEL(1,J)
        A(2)=VEL(2,J)
        A(3)=VEL(3,J)
        IF(NPAGE.EQ.2) GO TO 480
        A(1) = A(1)/EGSIL
        A(2) = A(2)/EGSIL
480      IF(IN.GE.2.AND.IN.LE.4) WRITE(NPRT,460) J,A
        IF(IN.LT.2.OR.IN.GT.4) WRITE(NPRT,470) J,A
460      FORMAT (1H ,I5,2X,14H VELOCITY ,2X,0PE12.5,2X,10H M/S
1E12.5,1X,9H M      ,2X,0PE12.5,2X,9H RAD/S )
470      FORMAT (1H ,I5,2X,14H VELOCITY ,2X,0PE12.5,2X,10H IN./S
1E12.5,1X,9H IN./S      ,2X,0PE12.5,2X,9H RAD/S )
490      IF (ACC(1,J).EQ.TINY) GO TO 540
        LINE=LINE+1
        IF (LINE.LT.NL) GO TO 500
        CALL PAGE
        WRITE (NPRT,390)
500      A(1)=ACC(1,J)
        A(2)=ACC(2,J)
        A(3)=ACC(3,J)
        IF(NPAGE.EQ.2) GO TO 530

```

```

,1PINIT1790
INIT1800
,1PINIT1810
INIT1820
INIT1830
INIT1840
INIT1850
INIT1860
INIT1870
INIT1880
INIT1890
INIT1900
INIT1910
INIT1920
INIT1930
INIT1940
INIT1950
,1PINIT1960
INIT1970
,1PINIT1980
INIT1990
INIT2000
INIT2010
INIT2020
INIT2030
INIT2040
INIT2050
INIT2060
INIT2070
INIT2080

```

```

530 A(1) = A(1)/EGSIL
    A(2) = A(2)/EGSIL
    IF(IN.GE.2.AND.IN.LE.4) WRITE(NPRT,510) J,A
    IF(IN.LT.2.OR.IN.GT.4) WRITE(NPRT,520) J,A
510   FORMAT (1H ,I5,2X,14H ACCELERATION ,2X,0PE12.5,2X,10H M/S**2
    1E12.5,1X,9H M/S**2 ,2X,0PE12.5,2X,9H RAD/S**2)
520   FORMAT (1H ,I5,2X,14H ACCELERATION ,2X,0PE12.5,2X,10H IN./S**2 ,1PE12.5,2X,9H RAD/S**2)
540   IF (8ET(1,J).EQ.TINY) GO TO 590
    LINE=LINE+1
    IF (LINE.LT.NL) GO TO 550
    CALL PAGE
    WRITE (NPRT,390)
550   A(1)=8ET(1,J)
    A(2)=8ET(2,J)
    A(3)=8ET(3,J)
    IF(NPAGE.EQ.2) GO TO 580
    A(1) = A(1)/EGSIL
    A(2) = A(2)/EGSIL
580   IF(IN.GE.2.AND.IN.LE.4) WRITE(NPRT,560) J,A
    IF(IN.LT.2.OR.IN.GT.4) WRITE(NPRT,570) J,A
560   FORMAT (1H ,I5,2X,14H JERK
    1E12.5,1X,9H M/S**3 ,0PE12.5,2X,9H RAD/S**3)
570   FORMAT (1H ,I5,2X,14H JERK
    1E12.5,1X,9H IN./S**3,0PE12.5,2X,9H RAD/S**3)
590   IF (FOR(1,J).EQ.TINY) GO TO 650
    LINE=LINE+1
    IF (LINE.LT.NL) GO TO 600
    CALL PAGE
    WRITE (NPRT,390)

```

```

INIT2090
INIT2100
INIT2110
INIT2120
INIT2130 ,1PINIT2130
INIT2140
INIT2150 ,1PINIT2150
INIT2160
INIT2170
INIT2180
INIT2190
INIT2200
INIT2210
INIT2220
INIT2230
INIT2240
INIT2250
INIT2260
INIT2270
INIT2280
INIT2290
INIT2300 ,1PINIT2300
INIT2310
INIT2320 ,1PINIT2320
INIT2330
INIT2340
INIT2350
INIT2360
INIT2370
INIT2380

```



```

600 A(1)=FOR(1,J)
    A(2)=FOR(2,J)
    A(3)=FOR(3,J)
    IF(NPAGE.EQ.2) GO TO 630
    A(1) = A(1)/EGSIF
    A(2) = A(2)/EGSIF
    A(3) = A(3)/(EGSIF*EGSIL)
630 IF(IN.GE.2.AND.IN.LE.4) WRITE(NPRT,610) J,A
    IF(IN.LT.2.OR.IN.GT.4) WRITE(NPRT,620) J,A
610 FORMAT (1H,15,2X,14H LOAD,2X,0PE12.5,2X,10H N
    1E12.5,1X,9H N,2X,0PE12.5,2X,9H N*M)
620 FORMAT (1H,15,2X,14H LOAD,2X,0PE12.5,2X,10H LB
    1E12.5,1X,9H LB,2X,0PE12.5,2X,9H LB*IN.)
640 FORMAT (1H)
650 IF (LINE.GT.ILINE) WRITE (NPRT,640)
660 CONTINUE
C
C IF INPUT-OUTPUT UNITS ARE MIXED, PRINT SECOND SET OF DATA.
C
    IF (NPAGE.EQ.2) GO TO 670
    IF (IUNITS.EQ.0.OR.IUNITS.EQ.2) GO TO 670
    NPAGE=2
    GO TO 360
    RETURN
    END
670

```

```

INIT2390
INIT2400
INIT2410
INIT2420
INIT2430
INIT2440
INIT2450
INIT2460
INIT2470
    ,1PINIT2480
INIT2490
    ,1PINIT2500
INIT2510
INIT2520
INIT2530
INIT2540
INIT2550
INIT2560
INIT2570
INIT2580
INIT2590
INIT2600
INIT2610
INIT2620
INIT2630

```

```

CJFCR 0 10
SUBROUTINE JFOR
C
C THIS SUBROUTINE READS AND ERROR CHECKS DATA INPUT TO THE
C JOINT FORCING FUNCTION DATA BLOCK.
C
COMMON DATA(10000),KDATA(500)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1 PI,REF,REH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
INTEGER HEAD,DHEAD
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,
1 IREG,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLO,LERR,LINE,NACC,NCM,
2 NCRD,NDF,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,
4 NTIMES,NVEL,IINITO
COMMON/SCALE/EGSIF,EGSIL
COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB,
1 LTABI,NMAX,NMAXI
DIMENSION IERR(50,5),AD(4),AK(3)
DATA EX,WY,ZZ,SI,CS/1HX,1HY,1HZ,1HS,1HC/
DATA AD/4H NORM,4H X,4H Y,4H Z/,888/4H /
DATA AK/4H COS,4H SINE,4H CNST/

C
C INITIALIZE VARIABLES USED BY THIS SUBROUTINE
C I=0
C IERR=IERR
C IUNIT=IUNITS
C JERROR=0
C KERROR=0
JFOR 0
JFOR 10
JFOR 20
JFOR 30
JFOR 40
JFOR 50
JFOR 60
JFOR 70
JFOR 80
JFOR 90
JFOR 100
JFOR 110
JFOR 120
JFOR 130
JFOR 140
JFOR 150
JFOR 160
JFOR 170
JFOR 180
JFOR 190
JFOR 200
JFOR 210
JFOR 220
JFOR 230
JFOR 240
JFOR 250
JFOR 260
JFOR 270
JFOR 280

```

```

10 LP=LFF
C LPI=LFFI
C NDL=0
C NFF=0
C XEGSIF = 1.E0/EGSIF
30 DO 10 M=1,NJD
C DO 10 N=1,5
C IERROR(M,N)=0
C READ BLOCK 8 TITLE CARD.
C
C FORMAT (20A4)
30 READ (NCRD,30) DHEAD
C
C READ BLOCK 8, CARD 2 (NCNE REQUIRED) AND TEST DATA.
C
C READ (NCRD,50) J,JA,AY,LA,AL,A,B,C,D
50 FORMAT (2I5,A1,4X,I4,A1,4E10.0)
C
C CHECK FOR LAST CARD INPUT TO DATA BLOCK
C
C IF (J.EQ.0) GO TO 180
C
C CHECK AVAILABILITY OF STORAGE TO STORE DATA
C LL=LP+4
C LLI=LPI+5
C IF (LL.LE.NMAX) GO TO 60
C IERR=IERR+1
C JERROR=1
C GO TO 70
JFOR 290
JFOR 300
JFOR 310
JFOR 320
JFOR 330
JFOR 340
JFOR 350
JFOR 360
JFOR 370
JFOR 380
JFOR 390
JFOR 400
JFOR 410
JFOR 420
JFOR 430
JFOR 440
JFOR 450
JFOR 460
JFOR 470
JFOR 480
JFOR 490
JFOR 500
JFOR 510
JFOR 520
JFOR 530
JFOR 540
JFOR 550
JFOR 560
JFOR 570
JFOR 580

```

60	IF (LLI.LE.NMAXI) GO TO 90	JFOR 590
	IERR=IERR+1	JFOR 600
	KERROR=1	JFOR 610
70	READ (NCRQ,80) J	JFOR 620
80	FORMAT (I5)	JFOR 630
	IF (J.NE.0) GO TO 70	JFOR 640
	GO TO 180	JFOR 650
C		JFOR 660
C	INCREMENT JOINT COUNTER	JFOR 670
90	I=I+1	JFOR 680
	LP=LL	JFOR 690
	LPI=LLI	JFOR 700
C		JFOR 710
C	CHECK THAT JOINT NUMBER INPUT IS DEFINED	JFOR 720
	IF (J.GT.0.AND.J.LE.NJ) GO TO 100	JFOR 730
	IERR=IERR+1	JFOR 740
	IERROR(I,1)=1	JFOR 750
100	IF (JA.EQ.0) GO TO 110	JFOR 760
	IF (JA.GT.0.AND.JA.LE.NJ) GO TO 110	JFOR 770
	IERR=IERR+1	JFOR 780
	IERROR(I,1)=1	JFOR 790
C		JFOR 800
C	SET DIRECTION PARAMETERS.	JFOR 810
110	K = 1	JFOR 820
	IF (AY.EQ.EX) K=2	JFOR 830
	IF (AY.EQ.WY) K=3	JFOR 840
	IF (AY.EQ.ZZ) K=4	JFOR 850
C		JFOR 860
C	CHECK THAT REFERENCE FUNCTION SPECIFIED IS DEFINED	JFOR 870
C		JFOR 880



```

C
C
C 120
IF (LA.LE.NTAB) GO TO 120
IERR=IERR+1
IERROR(I,3)=1

C
C
C SET FUNCTION TYPE PARAMETER.
L = -1
IF (LA.GT.0) L=LA
IF (AL.EQ.SI) L=-2
IF (AL.EQ.CS) L=-3
SET SCALE FACTOR DEFAULT
IF(A.EQ.888.OR.A.EQ.0.E0)A=1.E0

C
C
C CHECK THAT A LOADED JOINT IS GIVEN FOR A DISTRIBUTED LOAD.
IF(JA.EQ.0) NJOR = NJOR + 1
IF(JA.NE.0) NDL = NDL + 1

C
C
C CHECK THAT TIME PERIOD INPUT IS COMPATIBLE WITH THE
REFERENCE FUNCTION SPECIFIED.
IF(L.GE.-1.AND.0.NE.0.E0) IERROR(I,4) = 1
IF(L.LT.-1.AND.0.LE.0.E0) IERROR(I,5) = 1

C
C
C STORE INPUT DATA
KDATA(LPI-4) = J
KDATA(LPI-3)=JA
KDATA(LPI-2)=K
KDATA(LPI-1)=L
KDATA(LPI)=2

C
C
C DATA(LP-3)=A

```

```

JFOR 890
JFOR 900
JFOR 910
JFOR 920
JFOR 930
JFOR 940
JFOR 950
JFOR 960
JFOR 970
JFOR 980
JFOR 990
JFOR1000
JFOR1010
JFOR1020
JFOR1030
JFOR1040
JFOR1050
JFOR1060
JFOR1070
JFOR1080
JFOR1090
JFOR1100
JFOR1110
JFOR1120
JFOR1130
JFOR1140
JFOR1150
JFOR1160
JFOR1170
JFOR1180

```

JFOR1190  
JFOR1200  
JFOR1210  
JFOR1220  
JFOR1230  
JFOR1240  
JFOR1250  
JFOR1260  
JFOR1270  
JFOR1280  
JFOR1290  
JFOR1300  
JFOR1310  
JFOR1320  
JFOR1330  
JFOR1340  
JFOR1350  
JFOR1360  
JFOR1370  
JFOR1380  
JFOR1390  
JFOR1400  
JFOR1410  
JFOR1420  
JFOR1430  
JFOR1440  
JFOR1450  
JFOR1460  
JFOR1470  
JFOR1480

```

DATA(LP-2) = 8*EGSIF
DATA(LP-1)=C
DATA(LP)=0
RETURN TO READ NEXT INPUT CARD
GO TO 40
SET NUMBER OF JOINT FORCING FUNCTIONS INPUT
NFF=I
CHECK FOR NO INPUT
IF (NFF.EQ.0) GO TO 500
INITIALIZE COUNTERS FOR OUTPUT
LL=LFF
MM=LFFI
I=0
IF NO OUTPUT REQUIRED, SKIP DATA OUTPUT SECTION
IF (IPRINT.EQ.0) GO TO 280
PRINT DATA BLOCK HEADING
CALL PAGE
FORMAT (1H,20A4)
WRITE (NPRT,200) DHEAD
LINE=LINE+1
FORMAT (1H0,25X,30HJOINT FORCING FUNCTION DATA /)
WRITE (NPRT,220)
LINE=LINE+2

```



C	J=KDATA(MM+1)	JFOR1790
C	JA=KDATA(MM+2)	JFOR1800
C	K=KDATA(MM+3)	JFOR1810
	L=KDATA(MM+4)	JFOR1820
	OUTPUT DATA	JFOR1830
	L1=L+4	JFOR1840
	IF (L1.LE.3) GO TO 310	JFOR1850
290	FORMAT (1H, I5, 3X, I5, 6X, A4, 4X, I4, 5X, 4(0PE14.5))	JFOR1860
	WRITE (NPRT, 290) J, JA, AD(K), L, A, B, C, D	JFOR1870
	GO TO 320	JFOR1880
300	FORMAT (1H, I5, 3X, I5, 6X, A4, 4X, A4, 5X, 4(0PE14.5))	JFOR1890
310	WRITE (NPRT, 300) J, JA, AD(K), AK(L1), A, B, C, D	JFOR1900
320	CONTINUE	JFOR1910
	ITAG=1	JFOR1920
330	LINE=LINE+1	JFOR1930
	IF (LINE.LE.NL) GO TO 360	JFOR1940
	IF (IPRINT.EQ.0) GO TO 360	JFOR1950
	CALL PAGE	JFOR1960
	WRITE (NPRT, 220)	JFOR1970
	IF (IIUNIT.EQ.0.OR.IIUNIT.EQ.1) GO TO 340	JFOR1980
	WRITE (NPRT, 230)	JFOR1990
	GO TO 350	JFOR2000
340	WRITE (NPRT, 240)	JFOR2010
350	WRITE (NPRT, 260)	JFOR2020
	LINE=LINE+5	JFOR2030
360	GO TO (370, 400, 420, 440, 460, 480), ITAG	JFOR2040
370	LL=LL+4	JFOR2050
	MM=MM+5	JFOR2060
		JFOR2070
		JFOR2080



C					JFOR2090
C					JFOR2100
C					JFOR2110
380		IF (IERROR(I,1).EQ.0) GO TO 400			JFOR2120
		PRINT 390, J			JFOR2130
390		FORMAT (1H,23H*** JOINT NUMBER INPUT,I3,34H, HAS NOT BEEN DEFINE			JFOR2140
		10 (JFOR). ***)			JFOR2150
		ITAG=2			JFOR2160
		GO TO 330			JFOR2170
400		IF (IERROR(I,2).EQ.0) GO TO 420			JFOR2180
410		FORMAT (1H,33H*** THE DISTRIBUTED LOAD OF JOINT,I4,39H HAS NO LOA			JFOR2190
		10ED JOINT GIVEN (JFOR). ***)			JFOR2200
		PRINT 410, J			JFOR2210
		ITAG=3			JFOR2220
		GO TO 330			JFOR2230
420		IF (IERROR(I,3).EQ.0) GO TO 440			JFOR2240
430		FORMAT (1H,43H*** REFERENCE FUNCTION CODE INPUT FOR JOINT,I3,27H			JFOR2250
		11S NOT DEFINED (JFOR). ***)			JFOR2260
		PRINT 430, J			JFOR2270
		ITAG=4			JFOR2280
		GO TO 330			JFOR2290
440		IF (IERROR(I,4).EQ.0) GO TO 460			JFOR2300
450		FORMAT (1H,23H* TIME PERIOD FOR JOINT,I4,49H IS IRRELEVANT AND HA			JFOR2310
		1S BEEN IGNORED (JFOR).*)			JFOR2320
		IREC=IREC+1			JFOR2330
		PRINT 450, J			JFOR2340
		ITAG=5			JFOR2350
		GO TO 330			JFOR2360
460		IF (IERROR(I,5).EQ.0) GO TO 480			JFOR2370
470		FORMAT (1H,78H*** POSITIVE TIME PERIOD MUST BE INPUT FOR REFERENC			JFOR2380

```

1E FUNCTION INPUT FOR JOINT ,I3,12H (JFOR). ***)
IERR = IERR + 1
PRINT 470, J
ITAG=6
GO TO 330
IF (I.LT.NFF) GO TO 280

CHECK FOR MULTIPLE OUTPUT

IF (IIUNIT.EQ.0.OR.IIUNIT.EQ.2) GO TO 500
IF (IERR.GT.IIERR) GO TO 500
IF (IPRINT.EQ.0) GO TO 500
XEGSIF = 1.E0
IF(IIUNIT.EQ.1) IIUNIT = 2
IF(IIUNIT.EQ.3) IIUNIT = 0
LINE=NL+1
GO TO 190

CHECK FOR TERMINATION DUE TO LACK OF STORAGE

IF (JERROR.EQ.0) GO TO 520
FORMAT (1H,71H**INSUFFICIENT STORAGE AVAILABLE FOR JOINT FORCING
1 DATA. (JFOR).*** )
PRINT 510
GO TO 540
IF (KERROR.EQ.0) GO TO 540
FORMAT (1H,81H**INSUFFICIENT STORAGE AVAILABLE FOR JOINT FORCE
1 IDENTIFICATION DATA (JFCR).*** )
PRINT 530
RETURN

480
C
C
C
500
510
C
520
530
540
JFOR2390
JFOR2400
JFOR2410
JFOR2420
JFOR2430
JFOR2440
JFOR2450
JFOR2460
JFOR2470
JFOR2480
JFOR2490
JFOR2500
JFOR2510
JFOR2520
JFOR2530
JFOR2540
JFOR2550
JFOR2560
JFOR2570
JFOR2580
JFOR2590
JFOR2600
JFOR2610
JFOR2620
JFOR2630
JFOR2640
JFOR2650
JFOR2660
JFOR2670
JFOR2680

```

JFOR2690

END





```

IF (SPRING(5,ILS).LE.0.E0) GO TO 999
CALL DEFO(M)
C C FIND LEAF GENERALIZED FORCES AT END *S*.
C
SRQ(1)=SPRING(4,ILS)*UX
SRQ(2)=SPRING(2,ILS)*UY+SPRING(3,ILS)*UZ
SRQ(3)=SPRING(1,ILS)*UY+SPRING(2,ILS)*UZ
C
C FIND LEAF STRAIN ENERGY.
C
UR=.5E0*(SRQ(1)*UX+SRQ(2)*UZ+SRQ(3)*UY)
IF(UR.LT.TINY) UR=0.E0
IF (IFLAG.NE.3) GO TO 999
IF (UR.LE.SPRING(5,ILS)) GO TO 999
SPRING(5,ILS)=0.E0
101 FORMAT(1H,15H **LEAF SPRING ,I3,32H FAILED AT THIS LOADING.(LEAF)
1**)
WRITE (NPRT,101) ILS
999 RETURN
END
LEAF 290
LEAF 300
LEAF 310
LEAF 320
LEAF 330
LEAF 340
LEAF 350
LEAF 360
LEAF 370
LEAF 380
LEAF 390
LEAF 400
LEAF 410
LEAF 420
LEAF 430
LEAF 440
LEAF 450
LEAF 460
LEAF 470
LEAF 480
LEAF 490

```



```

DATA DS/4HIGN0,4HRE ,4+STOP,4H /
DATA DR/4HR/C-,4HSTIR,4HRUPS,4H R/,4HC-TI,4HED ,4H WF ,4HIN R,
14M/C ,4H WF,4H BEA,4HM ,4HLEAF,4H SPR,4HING /
DATA DQ/4HSTIR,4HRUPS ,4H TI,4HES /
NPAS=1
ICURR=1
IF (IUNITS.GT.1) ICURR=2
IF (IERR.NE.0) CALL PAGE
FORMAT (1H0,20X,25HELEMENT CONTROL VARIABLES/)
WRITE (NPRT,20)
FORMAT (1H ,60H ELEMENT JOINTS ELEMENT TYPE CONCRETES BEHAVIOLINK 390
1R SHEAR /)
WRITE (NPRT,30)
LINE=LINE+6
DO 60 I=1,NM
IF (LINE.LT.NL) GO TO 50
CALL PAGE
WRITE (NPRT,30)
FORMAT (1H ,2X,I3,4X,I3,1H-,I3,3X,3A4,2X,A4,1X,A4,2X,2A4,2X,2A4)
IR=3*(MTYPE(I)-1)+1
IS=2*(MSHEAR(I))+1
IA=MCODE(I)
IF (MTYPE(I).EQ.4) IA=9
IB=MATR(I)
IF (MTYPE(I).EQ.4) IB=MATW(I)
IT=2*(MSTAT(I)-1)+1
WRITE (NPRT,40) I,IP(I),IQ(I),OR(IR),OR(IR+1),OR(IR+2),NAME(IA),NALINK 550
1ME(IB),DU(IT),DU(IT+1),DS(IS),DS(IS+1)
LINE=LINE+1
NWF = 0

```





130	LINE=LINE+1	LINK 890
	CONTINUE	LINK 900
140	CALL PAGE	LINK 910
	FORMAT (20X,28H ELEMENT CROSS SECTION DATA /)	LINK 920
	WRITE (NPRT,140)	LINK 930
150	FORMAT (1H,69H ELEMENT JOINT DEPTH- TOP TO	LINK 940
	1 DEPTH- TOP TO ,	LINK 950
	WRITE (NPRT,150)	LINK 960
160	FORMAT (1H,69H NUMBER NUMBERS LOWER REBAR,IN. UPPER REBAR,IN.	LINK 970
	1 REF. AXIS, IN. /)	LINK 980
	IF (ICURR.EQ.1) WRITE (NPRT,160)	LINK 990
170	FORMAT (1H,69H NUMBER NUMBERS LOWER REBAR, M UPPER REBAR, M	LINK1000
	1 REF. AXIS, M /)	LINK1010
	IF (ICURR.EQ.2) WRITE (NPRT,170)	LINK1020
	LINE=LINE+6	LINK1030
	DO 200 I=1,NM	LINK1040
	IF (LINE.LT.NL) GO TO 190	LINK1050
	CALL PAGE	LINK1060
	WRITE (NPRT,150)	LINK1070
	IF (ICURR.EQ.1) WRITE (NPRT,160)	LINK1080
	IF (ICURR.EQ.2) WRITE (NPRT,170)	LINK1090
180	FORMAT (1H,2X,I3,4X,I3,1H-,I3,3X,0PE12.5,5X,0PE12.5,5X,	LINK1100
	10PE12.5,4X,0PE12.5)	LINK1110
190	IF (MTYPE(I).EQ.4) GO TO 200	LINK1120
	WRITE (NPRT,180) I,IP(I),IQ(I),D(I),CP(I),MTOP(I)	LINK1130
	LINE=LINE+1	LINK1140
200	CONTINUE	LINK1150
C		LINK1160
C	OUTPUT REINFORCEMENT DATA, FIRST, LONGITUDINAL,	LINK1170
	IPST=0	LINK1190



```

270 CONTINUE
280 LINE=LINE+1
C
C
    THEN LATERAL.
    IPST=0
    DO 390 J=1,NH
    IB=MTIES(J)
    NLAT=NTIES(J)
    IF (NPAS.EQ.1) YLDS(J) = YLDS(J)/(EGSIF/EGSIL**2)
    IF (NLAT.EQ.0) GO TO 390
    IF (IPST.NE.0) GO TO 336
    IPST=1
    CALL PAGE
    FORMAT (1H,43X,32H LATERAL REINFORCEMENT GROUPS /)
    WRITE (NPRT,290)
    300 FORMAT (118H BASE      JOINT  GROUP  REBAR  MAT+L  REBAR
1      SPACING OF  NO. OF START OF  YIELD STRESS  CONFINEMENT)
    WRITE (NPRT,300)
    310 FORMAT (119H ELEMENT  NUMBERS  NUMBER  TYPE  NAME  AREA,IN.**2
12  REBARS, IN. SPACES GROUP, IN. LB/IN.**2  FACTOR *PDP*/LINK1680
2)
    IF (ICURR.EQ.1) WRITE (NPRT,310)
    320 FORMAT (119H ELEMENT  NUMBER  NUMBER  TYPE  NAME  AREA, M**2LINK1710
1  REBARS, M. SPACES GROUP, M. N/M**2  FACTOR *PDP*/LINK1720
2)
    IF (ICURR.EQ.2) WRITE (NPRT,320)
    LINE=LINE+6
    336 IF (NSPAC(6,J).EQ.-1) GO TO 360
    DO 350 I=1,NLAT
    IF (LINE.LE.NL) GO TO 340

```

```

LINK1490
LINK1500
LINK1510
LINK1520
LINK1530
LINK1540
LINK1550
LINK1560
LINK1570
LINK1580
LINK1590
LINK1600
LINK1610
LINK1620
LINK1630
LINK1640
LINK1650
LINK1660
LINK1670
LINK1680
LINK1690
LINK1700
LINK1710
LINK1720
LINK1730
LINK1740
LINK1750
LINK1760
LINK1770
LINK1780

```

```

330 CALL PAGE
      WRITE (NPRT,300)
      IF (ICURR.EQ.1) WRITE (NPRT,310)
      IF (ICURR.EQ.2) WRITE (NPRT,320)
      FORMAT (1H,2X,I3,4X,I3,4X,I3,3X,I3,5X,A4,2X,A4,1X,0PE12.5,2X,
340 10PE12.5,3X,I3,4X,0PE11.4,2X,0PE12.5,2X,0PE12.5)
      WRITE (NPRT,330) J,IP(J),IQ(J),I,DQ(1),DQ(2),NAME(IB),ATIES(I,J),SLINK1850
      1TIES(I,J),NSPAC(I,J),XBEGS(I,J),YLDOS(J),PDP(I,J)
350 LINE=LINE+1
      GO TO 390
360 DO 380 I=1,NLAT
      IF (LINE.LE.NL) GO TO 370
      CALL PAGE
      WRITE (NPRT,300)
      IF (ICURR.EQ.1) WRITE (NPRT,310)
      IF (ICURR.EQ.2) WRITE (NPRT,320)
370 WRITE (NPRT,330) J,IP(I),IQ(I),I,DQ(3),DQ(4),NAME(IB),ATIES(I,J),SLINK1950
      1TIES(I,J),NSPAC(I,J),XBEGS(I,J),YLDOS(J),PDP(I,J)
380 LINE=LINE+1
390 CONTINUE
      C
      C
      OUTPUT MEMBER DATA ON STEEL FOR COMPOSITE SECTIONS
      IF (NCM.EQ.0.AND.NWF.EQ.0) GO TO 470
      CALL PAGE
      IF(NWF.NE.0) GO TO 403
400 FORMAT (1H,21X,46H WIDE FLANGE DIMENSIONS FOR COMPOSITE ELEMENTS/
      1)
      WRITE (NPRT,400)
      GO TO 413
403 WRITE (NPRT,405)

```

```

LINK1790
LINK1800
LINK1810
LINK1820
LINK1830
LINK1840
LINK1850
LINK1860
LINK1870
LINK1880
LINK1890
LINK1900
LINK1910
LINK1920
LINK1930
LINK1940
LINK1950
LINK1960
LINK1970
LINK1980
LINK1990
LINK2000
LINK2010
LINK2020
LINK2030
LINK2040
LINK2050
LINK2060
LINK2070
LINK2080

```



```

405 FORMAT (1H ,21X,23H WIDE FLANGE DIMENSIONS/)
410 FORMAT (1H ,75H BASE JOINT THICKNESS,
1KNES DEPTH OF )
413 WRITE (NPRT,410)
420 FORMAT (1H ,79H ELEMENT NUMBERS FLANGE,IN.
1EB, IN. BEAM, IN. /)
IF (ICURR.EQ.1) WRITE (NPRT,420)
430 FORMAT (1H ,68H ELEMENT NUMBERS FLANGE, M
1EB, M BEAM, M/)
IF (ICURR.EQ.2) WRITE (NPRT,430)
DO 460 I=1,NM
IF (LINE.LE.NL) GO TO 450
CALL PAGE
WRITE (NPRT,410)
IF (ICURR.EQ.2) WRITE (NPRT,430)
IF (ICURR.EQ.1) WRITE (NPRT,420)
440 FORMAT (1H ,2X,I3,4X,I3,1H-,I3,2X,4(0PE12.5,2X))
450 IF(MTYPE(I).LT.3) GO TO 460
WRITE (NPRT,440) I,IP(I),IQ(I),IFWF(I),BMF(I),TMMF(I),DMF(I)
460 CONTINUE
C
C OUTPUT LEAF SPRING DATA.
470 IF (NLS.EQ.0) GO TO 550
CALL PAGE
480 FORMAT (1H ,26X,31H LEAF SPRING ELEMENT PARAMETERS/)
WRITE (NPRT,480)
490 FORMAT (1H ,101H LEAF JOINT DISPL. OF TIP ROTATION OF
1TATION OF TIP ELONGATION OF STORABLE ENERGY)
WRITE (NPRT,490)
500 FORMAT (1H ,101H SPRING NUMBERS FORCE, LB/IN. FORCE, LB/RAD
MOLINK2090 THICKNESS
LINK2100 WIDTH OF
LINK2110 FLANGE,IN.
LINK2120 OF
LINK2130 FLANGE,IN.
LINK2140 OF
LINK2150 FLANGE, M
LINK2160 FLANGE, M
LINK2170
LINK2180
LINK2190
LINK2200
LINK2210
LINK2220
LINK2230
LINK2240
LINK2250
LINK2260
LINK2270
LINK2280
LINK2290
LINK2300
LINK2310
LINK2320
LINK2330
LINK2340
ROLINK2350
LINK2360
LINK2370
MOLINK2380

```

```

1MENT,IN,*L8/RAD  AXIS FORCE,L8/IN.  LIMIT,IN.-L8  /)
IF (ICURR.EQ.1) WRITE (NPRT,500)
FORMAT (1H ,101H SPRING  NUMBERS  FORCE, N/M  FORCE,N/RAD
1MENT, M*N/RAD  AXIS FORCE, N/M  LIMIT,M-N  /)
IF (ICURR.EQ.2) WRITE (NPRT,510)
DO 540 I=1,NLS
IF (LINE.LE.NL) GO TO 530
CALL PAGE
WRITE (NPRT,490)
IF (ICURR.EQ.2) WRITE (NPRT,510)
IF (ICURR.EQ.1) WRITE (NPRT,500)
520  FORMAT (1H ,3X,I3,4X,I3,2X,0PE12.5,3X,0PE12.5,2X,0PE12.5,7X,
1,0PE12.5,8X,0PE12.5)
530  WRITE (NPRT,520) I,IPL(I),IQL(I),(SPRING(J,I),J=1,5)
540  CONTINUE
C
C
C  MAKE SI,ENGLISH CONVERSIONS.
550  IF(IUNITS.EQ.0.OR.IUNITS.EQ.2.OR.NPAS.GT.1) RETURN
NPAS = NPAS + 1
IF(IUNITS.EQ.1) ICURR = 2
IF(IUNITS.EQ.3) ICURR = 1
DO 580 MEM=1,NM
XL(MEM) = XL(MEM)*EGSIL
8MEM(MEM)=8MEM(MEM)*EGSIL
8PP(MEM)=8PP(MEM)*EGSIL
D(MEM)=D(MEM)*EGSIL
DP(MEM)=DP(MEM)*EGSIL
DPP(MEM)=DPP(MEM)*EGSIL
EFLM(MEM)=EFLM(MEM)*EGSIL
LINK2390
LINK2400
MOLINK2410
LINK2420
LINK2430
LINK2440
LINK2450
LINK2460
LINK2470
LINK2480
LINK2490
LINK2500
LINK2510
LINK2520
LINK2530
LINK2540
LINK2550
LINK2560
LINK2570
LINK2580
LINK2590
LINK2600
LINK2610
LINK2620
LINK2630
LINK2640
LINK2650
LINK2660
LINK2670
LINK2680

```

LINK2690  
LINK2700  
LINK2710  
LINK2720  
LINK2730  
LINK2740  
LINK2750  
LINK2760  
LINK2770  
LINK2780  
LINK2790  
LINK2800  
LINK2810  
LINK2820  
LINK2830  
LINK2840  
LINK2850  
LINK2860  
LINK2870  
LINK2880  
LINK2890  
LINK2900  
LINK2910  
LINK2920  
LINK2930  
LINK2940  
LINK2950  
LINK2960

```

HMEM(MEM)=HMEM(MEM)*EGSIL
XBEGM(MEM)=XBEGM(MEM)*EGSIL
YLOS(MEM) = YLOS(MEM)*EGSIF/EGSIL**2
DWF(MEM)=DWF(MEM)*EGSIL
TFWF(MEM)=TFWF(MEM)*EGSIL
TWWF(MEM)=TWWF(MEM)*EGSIL
BWF(MEM)=BWF(MEM)*EGSIL
HTOP(MEM)=HTOP(MEM)*EGSIL
HTWF(MEM)=HTWF(MEM)*EGSIL

C
DO 570 I=1,6
  ATIES(I, MEM) = ATIES(I, MEM)*EGSIL**2
  STIES(I, MEM)=STIES(I, MEM)*EGSIL
  XBEGS(I, MEM)=XBEGS(I, MEM)*EGSIL
570 DO 580 IGRP=1,10
  AGRP(IGRP, MEM) = AGRP(IGRP, MEM)*EGSIL**2
  EFFL(IGRP, MEM)=EFFL(IGRP, MEM)*EGSIL
  XBEG(IGRP, MEM)=XBEG(IGRP, MEM)*EGSIL
  YBAR(IGRP, MEM)=YBAR(IGRP, MEM)*EGSIL
580 DO 590 I=1, NLS
  DO 585 J=1,4
  SPRING(J, I)=SPRING(J, I)*EGSIL/EGSIF
  SPRING(5, I)=SPRING(5, I)*EGSIL*EGSIF
585 DO 595 J=1, NJ
  X(J) = X(J)*EGSIL
  Y(J) = Y(J)*EGSIL
595 GO TO 10
END

```





```

1HJOINT,7X,11HX-DIRECTION,7X,11HY-DIRECTION,7X,11HOF INERTIA) LUMP 290
WRITE (NPRT,70) LUMP 300
LINE=LINE+9 LUMP 310
90 FORMAT (1H ,12X,11HLB*S**2/IN.,7X,11HLB*S**2/IN.,7X,11HLB*S**2*IN. LUMP 320
1/) LUMP 330
IF ((NPAGE.EQ.1.AND.IUNITS.LE.1).OR. (NPAGE.EQ.2.AND.
1 (IUNITS.EQ.0.OR.IUNITS.EQ.3))) WRITE (NPRT,90) LUMP 340
110 FORMAT (1H ,17X,2HKG,16X,2HKG,13X,7HKG*M**2/) LUMP 350
IF ((NPAGE.EQ.1.AND.IUNITS.GT.1).OR. (NPAGE.EQ.2.AND. LUMP 360
1 (IUNITS.EQ.1.OR.IUNITS.EQ.2))) WRITE (NPRT,110) LUMP 370
LINE=LINE+2 LUMP 380
C LUMP 390
C LUMP 400
C LUMP 410
C LUMP 420
C LUMP 430
C LUMP 440
C LUMP 450
C LUMP 460
C LUMP 470
C LUMP 480
C LUMP 490
C LUMP 500
C LUMP 510
C LUMP 520
C LUMP 530
C LUMP 540
C LUMP 550
C LUMP 560
C LUMP 570
C LUMP 580

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200	IF (LINE.LE.NL) GO TO 240	LUMP 590
	CALL PAGE	LUMP 600
	WRITE (NPRT,40)	LUMP 610
	WRITE (NPRT,50)	LUMP 620
	WRITE (NPRT,60)	LUMP 630
	WRITE (NPRT,70)	LUMP 640
	LINE=LINE+6	LUMP 650
	IF (NPAGE.EQ.1) GO TO 210	LUMP 660
	IF (IUNITS.EQ.1) GO TO 230	LUMP 670
	GO TO 220	LUMP 680
210	IF (IUNITS.GT.1) GO TO 230	LUMP 690
220	WRITE (NPRT,90)	LUMP 700
	LINE=LINE+2	LUMP 710
	GO TO 240	LUMP 720
230	WRITE (NPRT,110)	LUMP 730
	LINE=LINE+2	LUMP 740
C	END OF DO LOOP.	LUMP 750
C		LUMP 760
C		LUMP 770
240	CONTINUE	LUMP 780
C		LUMP 790
C	IF INPUT-OUTPUT UNITS ARE MIXED, PRINT SECOND SET OF DATA.	LUMP 800
C		LUMP 810
	IF (NPAGE.EQ.2) GO TO 250	LUMP 820
	IF (IUNITS.EQ.0.OR.IUNITS.EQ.2) GO TO 250	LUMP 830
	NPAGE=2	LUMP 840
	GO TO 20	LUMP 850
250	RETURN	LUMP 860
C		LUMP 870
	END	LUMP 880

```

CMASS      0 10
C          SUBROUTINE MASS
C
C          THIS SUBROUTINE READS FROM CARDS LUMPED MASSES AT THE JOINTS.
C
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1  MATH(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2  MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),DIS(3,50),ERJF(3,50),
1  ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
1  XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)
COMMON/LEAD8K/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1  PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
INTEGER HEAD,DHEAD
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,MASS
1  IREG,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,MASS
2  NCRO,NDF,NDFD,NDFJ,NDIS,NOL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,MASS
3  NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,MASS
4  NTIMES,NVEL,IINITD
C          * * * * *
C          READ USER'S TITLE AND INITIALIZE JOINT AND ERROR COUNTER.
C          * * * * *
C          FORMAT (20A4)
C          READ (NCRO,10) DHEAD
C          NMAS=0
C          JERR=0
C          DO 20 J=1,NJ
C
MASS      0
MASS     10
MASS     20
MASS     30
MASS     40
MASS     50
MASS     60
MASS     70
MASS     80
MASS     90
MASS    100
MASS    110
MASS    120
MASS    130
MASS    140
MASS    150
MASS    160
MASS    170
MASS    180
MASS    190
MASS    200
MASS    210
MASS    220
MASS    230
MASS    240
MASS    250
MASS    260
MASS    270
MASS    280

```

20	DO 20 I=1,3	MASS 290
C	DAS(I,J)=0.E0	MASS 300
C	READ JOINT NO. AND LUMPED MASSES AT THE JOINT.	MASS 310
30	FORMAT (I5,X,3E10.0)	MASS 320
40	READ (NCRD,30) J,B,C,D	MASS 330
C		MASS 340
C	TEST TO SEE IF LAST CARD.	MASS 350
C		MASS 360
C	IF (J.EQ.0) GO TO 170	MASS 370
C		MASS 380
C	INCREMENT JOINT COUNTER AND CHECK RANGE OF JOINT NUMBER.	MASS 390
C		MASS 400
C		MASS 410
	NMAS=NMAS+1	MASS 420
	IF (J.GE.1.AND. J.LE.NJ) GO TO 90	MASS 430
	IERR=IERR+1	MASS 440
	IF (JERR.EQ.1) GO TO 80	MASS 450
	CALL PAGE	MASS 460
50	FORMAT (1H,20A4,//)	MASS 470
	WRITE (NPRT,50) OHEAD	MASS 480
60	FORMAT (1H,10X,41HINPUT ERRORS IN EXTERNAL LUMPED MASS DATA//)	MASS 490
	WRITE (NPRT,60)	MASS 500
	JERR=1	MASS 510
70	FORMAT (14H *** JOINT NO.,I5,50H LESS THAN ONE OR GREATER THAN LARMAS	MASS 520
	1GEST JOINT NO. =,I4,12H (MASS). ***)	MASS 530
80	PRINT 70, J,NJ	MASS 540
	GO TO 40	MASS 550
90	IF (NJ.GT.NJD) GO TO 40	MASS 560
C		MASS 570
C		MASS 580



C	IF UNEQUAL MASSES DETECTED, PRINT WARNING AND CONTINUE.	MASS 590
C		MASS 600
	IF (ABS(B-C).LT.EPS) GO TO 130	MASS 610
	IF (JERR.EQ.1) GO TO 120	MASS 620
	CALL PAGE	MASS 630
	WRITE (NPRT,60)	MASS 640
	JERR=1	MASS 650
110	FORMAT (1H,66H** WARNING. INPUT VALUES OF TRANSLATIONAL MASS PARAMETERS AT JOINT,I5,43H NOT EQUAL IN X AND Y DIRECTIONS (MASS). **)	MASS 660
120	PRINT 110, J	MASS 670
	IREC=IREC+1	MASS 680
C		MASS 690
C	IF MASS IS NEGATIVE, STORE POSITIVE VALUE AND CONTINUE.	MASS 700
C		MASS 710
		MASS 720
130	IF (B.GT.-EPS.OR.C.GT.-EPS) GO TO 160	MASS 730
	IREC=IREC+1	MASS 740
	IF (JERR.EQ.1) GO TO 150	MASS 750
	CALL PAGE	MASS 760
	WRITE (NPRT,60)	MASS 770
	JERR=1	MASS 780
140	FORMAT (34H * NEGATIVE MASS DETECTED AT JOINT,I5,41H IGNORED, POSITIVE VALUE STORED (MASS). *)	MASS 790
150	PRINT 140, J	MASS 800
	IREC=IREC+1	MASS 810
	DAS(1, J)=ABS(B)	MASS 820
	DAS(2, J)=ABS(C)	MASS 830
	DAS(3, J)=D	MASS 840
	GO TO 40	MASS 850
	DAS(1, J)=B	MASS 860
160	DAS(2, J)=C	MASS 870
		MASS 880

DAS(3,J)=0  
GO TO 40  
  
C  
170 RETURN  
END

MASS 890  
MASS 900  
MASS 910  
MASS 920  
MASS 930

```

CMATP 0 10
SUBROUTINE MATP
C
C THIS SUBROUTINE READS FROM CARDS, ERROR CHECKS, AND STORES INFORMATION
C DEFINING THE MATERIAL PROPERTIES
C
COMMON/FIBER/DENS(9), EC(9), EPSU(9), ET(9), FCFY(9), G(9), PR(9), S(9),
1 SLOPE(8,9), ST(17,6), STN(8,9), STS(8,9), UNLK(9), ICODE(9), NAME(9)
COMMON/LEADBK/AVDM, AVGL, CA, CB, CC, CD, CE, OHEAD(20), DT, EPS, HEAD(20),
1 PI, RERF, RERH, RERZ, SERR, TBEGIN, THALT, TIME, TINK, TINY, TPROB
INTEGER HEAD, OHEAD, 8888, ZZZZ, PAME
COMMON/MAINBK/IANAL, ICURV, IERR, IFAIL, IFOR, ILIN, IPAGE, IPLOT, IPRINT, MATP
1 IREC, ISTART, ISTOP, ISTRES, ITAPE, IUNITS, IYLD, LERR, LINE, NACC, NCM, MATP
2 NCRD, NDF, NDFD, NDFJ, NDIS, NDL, NFF, NJOR, NING, NJ, NJD, NJER, NL, NLD,
3 NLS, NLSR, NM, NMAS, NMAT, NMATD, NMD, NPLOT, NPRI, NSAVE, NTAB, NTAPE,
4 NTIMES, NVEL, IINITD
COMMON/SCALE/EGSIF, EGSIL
DIMENSION IERROR(9,16), STSK(8), TYPA(5,3)
C
DATA TYPA/4HUNCO,4HNFIN,4HED C,4HONCR,4HETE ,
1 4HCONF,4HINED,4H CON,4HCRET,4HE ,
2 4HREIN,4HFORC,4HING ,4HSTEE,4HL /
DATA 8888/4H /, ZZZZ/4H0000/, UA/1HU/, CS/1HC/, FT/2H$$/
C
C INITIALIZE PARAMETERS USED BY SUBROUTINE
C
J=0
NMAT=0
IERR=IERR
DO 10 K=1,16

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10      DO 10 M=1,9
          IERROR(M,K)=0
          EGSIS = EGSIF/EGSIL**2
          EGSID = 1.E0
          EGSISS = 1.E0

C      C
C      CHANGE UNITS OF STORED STRESS-STRAIN CURVES.
C      IF(IUNITS.EQ.0.OR.IUNITS.EQ.3) GO TO 21
          EGSISS = 6894.7572E0
          EGSID = 271447.1375E0
          DO 20 I=1,6
              DO 20 K=1,9
                  20 ST(K,I) = ST(K,I)*EGSISS
                  21 CONTINUE

C      C
C      READ DATA BLOCK TITLE CARD
          READ (NCRD,30) DHEAD
          FORMAT (20A4)

30      C
C      READ FIRST DATA CARD

C      C
          FORMAT (A4,1X,A1,4X,7E10.0)
          READ (NCRD,40) PAME,TC,A,B,C,D,E,F
          PAME = MATERIAL NAME
          TC = TYPE OF MATERIAL-U=0=UNCONF. CONC., C=1=CONFINED CONC.,2=STEEL
          A = CRUSHING (CONCRETE) OR YIELD (STEEL) STRENGTH
          B = POISSON'S RATIO, LINEAR ELASTIC
          C = SHEAR MODULUS, LINEAR ELASTIC
          D = DENSITY
          E = UNLOADING CURVE DATA (K FOR CONCRETE)

C      C
          MATP 290
          MATP 300
          MATP 310
          MATP 320
          MATP 330
          MATP 340
          MATP 350
          MATP 360
          MATP 370
          MATP 380
          MATP 390
          MATP 400
          MATP 410
          MATP 420
          MATP 430
          MATP 440
          MATP 450
          MATP 460
          MATP 470
          MATP 480
          MATP 490
          MATP 500
          MATP 510
          MATP 520
          MATP 530
          MATP 540
          MATP 550
          MATP 560
          MATP 570
          MATP 580

```



C	F = UNLOADING CURVE DATA	MATP 590
C	QAME = MATERIAL IDENTIFICATION DATA (NAME)	MATP 600
C		MATP 610
C	CHECK FOR LAST CARD INPUT TO DATA BLOCK	MATP 620
	IF ((PAME.EQ.9888).OR.(PAME.EQ.ZZZZ)) GO TO 570	MATP 630
C		MATP 640
C	INCREMENT MATERIAL COUNTER	MATP 650
	J=J+1	MATP 660
	ICODE(J)=2	MATP 670
	IF (TC.EQ.UA) ICODE(J)=0	MATP 680
	IF (TC.EQ.CS) ICODE(J)=1	MATP 690
	IC=ICODE(J)+1	MATP 700
C		MATP 710
C	CHECK FOR AVAILABILITY OF STORAGE	MATP 720
	IF (J.LE.NMATD) GO TO 70	MATP 730
	J=NMATD	MATP 740
	IERROR(J,1)=1	MATP 750
	IERR=IERR+1	MATP 760
C		MATP 770
C	IF STORAGE NOT AVAILABLE, READ REMAINING DATA CARDS FOR MATERIAL	MATP 780
	READ (NCRD,60) AZ,AZ	MATP 790
60	FORMAT (A4/A4)	MATP 800
	GO TO 560	MATP 810
C		MATP 820
C	STORE DATA FROM FIRST CARD	MATP 830
70	NAME(J)=PAME	MATP 840
	PR(J)=B	MATP 850
C		MATP 860
C	READ REMAINING DATA CARDS FOR MATERIAL	MATP 870
C		MATP 890

```

      READ (NCRD,40) PAME,TC,(STS(I,J),STN(I,J),I=1,3),STS(4,J)      MATP 890
      IF ((PAME.NE.NAME(J)).AND.(PAME.NE.388B).AND.(PAME.NE.ZZZZ)) GO TOMATP 900
1 90      MATP 910
      GO TO 100      MATP 920
      FORMAT (53H ***MATERIAL DATA CARDS ARE OUT-OF-SORT FOR MATERIAL ,AMATP 930
14,12H (MATP).*** )
      PRINT 80, NAME(J)      MATP 940
      IERR=IERR+1      MATP 950
      READ (NCRD,40) PAME,TC,STN(4,J),(STS(I,J),STN(I,J),I=5,7)      MATP 960
      GO TO 50      MATP 970
100      READ (NCRD,40) PAME,TC,STN(4,J),(STS(I,J),STN(I,J),I=5,7)      MATP 980
      IF ((PAME.NE.NAME(J)).AND.(PAME.NE.888B).AND.(PAME.NE.ZZZZ)) GO TOMATP1000
1 110      MATP1010
      GO TO 120      MATP1020
      PRINT 80, NAME(J)      MATP1030
      IERR=IERR+1      MATP1040
      GO TO 50      MATP1050
C      MATP1060
C      CHECK FOR MONOTONICITY OF STRAINS AND INTERCHANGE CARD DATA IF
C      NECESSARY      MATP1070
C      ITIME=0      MATP1080
      DO 170 I=2,7      MATP1090
      IF (ABS(STN(I-1,J)).GT.ABS(STN(I,J))) GO TO 140      MATP1100
      GO TO 170      MATP1110
140      IF (ITIME.GT.0) GO TO 160      MATP1120
      ITIME=1      MATP1130
      DO 150 I1=1,7      MATP1140
      STSK(I1)=STS(I1,J)      MATP1150
      STS(1,J)=STN(4,J)      MATP1160
      STS(2,J)=STN(5,J)      MATP1170
      MATP1180

```

```

160 STS(3,J)=STN(6,J)
    STS(4,J)=STN(7,J)
    STS(5,J)=STN(1,J)
    STS(6,J)=STN(2,J)
    STS(7,J)=STN(3,J)
    STN(1,J)=STSK(5)
    STN(2,J)=STSK(6)
    STN(3,J)=STSK(7)
    STN(4,J)=STSK(1)
    STN(5,J)=STSK(2)
    STN(6,J)=STSK(3)
    STN(7,J)=STSK(4)
    GO TO 170
    IERROR(J,15)=1
    IERR=IERR+1
    GO TO 180
    CONTINUE
170
C
180 IF (A.EQ.0.E0) A = STS(2,J)
    STORE INPUT DATA AND CONVERT UNITS.
    FCFY(J) = A*EGSIS
    DENS(J) = D*(EGSIS/EGSIL)
    G(J) = C*EGSIS
    E = E*EGSIS
    DO 200 I=1,8
200 STS(I,J) = STS(I,J)* EGSIS
    IF (IERROR(J,3).NE.0.OR.IERROR(J,4).NE.0) GO TO 560
    IF (ICODE(J).EQ.2) GO TO 225
C
C CHECK FOR REVERSE LOADING STRESS-STRAIN POINT SPECIFIED FOR CONCRETE
    MATP1190
    MATP1200
    MATP1210
    MATP1220
    MATP1230
    MATP1240
    MATP1250
    MATP1260
    MATP1270
    MATP1280
    MATP1290
    MATP1300
    MATP1310
    MATP1320
    MATP1330
    MATP1340
    MATP1350
    MATP1360
    MATP1370
    MATP1380
    MATP1390
    MATP1400
    MATP1410
    MATP1420
    MATP1430
    MATP1440
    MATP1450
    MATP1460
    MATP1470
    MATP1480

```

```

220      IF (E.NE.0.E0.OR.F.NE.0.E0) GO TO 220
          E=.25E0
          F=0.E0
          UNLK(J)=E
          GO TO 227
225      UNLK(J)=1.E0
227      STN(8,J)=F
          STS(8,J)=E
          C
          C      CHECK THAT INPUT VALUE OF POISSON'S RATIO IS WITHIN LIMITS
          IF (PR(J).GE.0.E0.AND.PR(J).LT.0.5E0) GO TO 230
          IERROR(J,7)=1
          IREC = IREC + 1
          C
          C      CHECK THAT INPUT VALUE OF SHEAR MODULUS IS WITHIN LIMITS.
          IF(G(J).GE.0.AND.G(J).LT.1.5E7*EGSISS) GO TO 240
          IERROR(J,8)=1
          IERR=IERR+1
          C
          C      CHECK THAT INPUT VALUE OF MATERIAL DENSITY IS WITHIN LIMITS
          IF(DENS(J).GE.0.E0.AND.DENS(J).LE.0.5E0*EGSID) GO TO 250
          IERROR(J,9)=1
          IREC = IREC + 1
          C
          C      CHECK THAT INPUT VALUE OF UNLOADING CURVE CONSTANT IS WITHIN LIMIT
          IF(ICODE(J).EQ.2)GO TO 256
250      IF (STS(8,J).GT.0.E0.AND.STS(8,J).LE.1.E0) GO TO 260
254      IERROR(J,10)=1
          IERR=IERR+1
          MATP1490
          MATP1500
          MATP1510
          MATP1520
          MATP1530
          MATP1540
          MATP1550
          MATP1560
          MATP1570
          MATP1580
          MATP1590
          MATP1600
          MATP1610
          MATP1620
          MATP1630
          MATP1640
          MATP1650
          MATP1660
          MATP1670
          MATP1680
          MATP1690
          MATP1700
          MATP1710
          MATP1720
          MATP1730
          MATP1740
          MATP1750
          MATP1760
          MATP1770
          MATP1780

```



```

256      GO TO 260
260      IF (STS(8,J).LT.0.E0.OR.STN(8,J).LT.0.E0)GO TO 254
270      DO 270 I=1,7
          IF (STS(I,J).NE.0.E0.OR.STN(I,J).NE.0.E0) GO TO 440
          CONTINUE
          IF (IC.EQ.3) GO TO 340
          *****
          C      GENERATE STRESS-STRAIN CURVE FOR CONCRETE (CONFINED,UNCONFINED).
          C      *****
          C      *****
          C      *****
          C      *****
          C      CHECK THAT INPUT VALUE OF CRUSHING STRENGTH IS WITHIN LIMITS
          IF (FCFY(J).GE.2.5E3*EGSISS.AND.FCFY(J).LE.8.E3*EGSISS) GO TO 300
          IERROR(J,11)=1
          IERR=IERR+1
          DO 290 I=1,7
              SLOPE(I,J)=99999.E0
              EPSU(J)=99999.E0
              SLOPE(8,J)=99999.E0
              ET(J)=99999.E0
              EC(J)=99999.E0
          GO TO 560
          STS(1,J)=0.E0
          STS(2,J) = -.5E0*FCFY(J)
          STS(3,J)=-.85E0*FCFY(J)
          STS(4,J)=-1.0E0*FCFY(J)
          STS(7,J)=-2.E-1*FCFY(J)
          STN(1,J)=0.0E0
          STN(2,J)=-.586E-3
          STN(3,J)=-1.225E-3
          STN(4,J)=-2.0E-3
          MATP1790
          MATP1800
          MATP1810
          MATP1820
          MATP1830
          MATP1840
          MATP1850
          MATP1860
          MATP1870
          MATP1880
          MATP1890
          MATP1900
          MATP1910
          MATP1920
          MATP1930
          MATP1940
          MATP1950
          MATP1960
          MATP1970
          MATP1980
          MATP1990
          MATP2000
          MATP2010
          MATP2020
          MATP2030
          MATP2040
          MATP2050
          MATP2060
          MATP2070
          MATP2080

```



```

C
360      FA=ABS(FCFY(J))
      DO 380 I=1,7
      STN(I,J)=99999.E0
      STS(I,J)=99999.E0
380      SLOPE(I,J)=99999.E0
      SLOPE(8,J)=99999.E0
      EPSU(J)=99999.E0
      ET(J)=99999.E0
      EC(J)=99999.E0

C
C      GENERATE STRESS-STRAIN CURVE
C
C      FIND INTERPOLATION RANGE.
      DO 390 I=1,6
      IF (FCFY(J).GE.ST(1,I)) GO TO 390
      I1=I-1
      GO TO 400
390      CONTINUE
      I1 = I - 1
      IF (FCFY(J).GT.ST(1,I)) I1 = I
      IF ((I1.GT.0).AND.(I1.LT.6)) GO TO 410
      IERROR(J,13)=1
      IERR=IERR+1
      GO TO 430

C
C      PERFORM INTERPOLATION
410      ALP=(ST(1,I1+1)-FA)/(ST(1,I1+1)-ST(1,I1))
      BET=1.E0-ALP
      DO 420 I=2,NST

```

```

MATP2390
MATP2400
MATP2410
MATP2420
MATP2430
MATP2440
MATP2450
MATP2460
MATP2470
MATP2480
MATP2490
MATP2500
MATP2510
MATP2520
MATP2530
MATP2540
MATP2550
MATP2560
MATP2570
MATP2580
MATP2590
MATP2600
MATP2610
MATP2620
MATP2630
MATP2640
MATP2650
MATP2660
MATP2670
MATP2680

```





```

      STSMAX=ABS(STS(K,J))
      NSTN=K
465  CONTINUE
      EPSU(J)=STN(NSTN,J)
C
C
C
      DETERMINE THE SLOPES OF THE SEGMENTS OF THE STRESS-STRAIN CURVES
470  DO 490 L=2,7
      TNUM=STS(L,J)-STS(L-1,J)
      TDEN=STN(L,J)-STN(L-1,J)
      IF (TDEN.NE.0.0) GO TO 480
      SLOPE(L-1,J)=1.0E0
      GO TO 490
480  SLOPE(L-1,J)=TNUM/TDEN
      CONTINUE
      IF (ICODE(J).EQ.2) GO TO 510
      ET(J)=0.0E0
      EC(J)=SLOPE(1,J)
      GO TO 560
510  TNUM=STS(8,J)-STS(1,J)
      TDEN=STN(8,J)-STN(1,J)
      IF (TDEN.NE.0.0E0) GO TO 520
      SLOPE(7,J)=1.0E0
      GO TO 530
520  SLOPE(7,J)=TNUM/TDEN
530  TNUM=STS(3,J)-STS(8,J)
      TDEN=STN(3,J)-STN(8,J)
      IF (TDEN.NE.0.0E0) GO TO 540
      SLOPE(8,J)=1.0E0
      GO TO 550

```

```

MATP2990
MATP3000
MATP3010
MATP3020
MATP3030
MATP3040
MATP3050
MATP3060
MATP3070
MATP3080
MATP3090
MATP3100
MATP3110
MATP3120
MATP3130
MATP3140
MATP3150
MATP3160
MATP3170
MATP3180
MATP3190
MATP3200
MATP3210
MATP3220
MATP3230
MATP3240
MATP3250
MATP3260
MATP3270
MATP3280

```

540	SLOPE(8,J)=TNUM/TDEN	MATP3290
550	ET(J)=SLOPE(1,J)	MATP3300
560	EC(J)=SLOPE(1,J)	MATP3310
	CONTINUE	MATP3320
	IF (G(J).NE.0.E0) GO TO 50	MATP3330
	IF (EC(J).NE.0.E0) G(J)=EC(J)/(2.E0*(1.E0+PR(J)))	MATP3340
	IF (ET(J).NE.0.E0) G(J)=ET(J)/(2.E0*(1.E0+PR(J)))	MATP3350
	GO TO 50	MATP3360
570	NMAT=J	MATP3370
	IIUNIT=IUNITS	MATP3380
	NPAGE = 1	MATP3390
580	CONTINUE	MATP3400
C		MATP3410
C	IF NO DATA OUTPUT REQUIRED, SKIP DATA OUTPUT	MATP3420
C		MATP3430
	IF (IPRINT.EQ.0) GO TO 610	MATP3440
C		MATP3450
C	WRITE GENERAL PROBLEM DESCRIPTION AND PAGE NUMBER	MATP3460
	CALL PAGE	MATP3470
C		MATP3480
C	WRITE DATA BLOCK HEADING	MATP3490
590	FORMAT (1H,20A4,//)	MATP3500
	WRITE (NPRT,590) DHEAD	MATP3510
600	FORMAT (1H,19X,19HMATERIAL CONSTANTS )	MATP3520
	WRITE (NPRT,600)	MATP3530
	LINE=LINE+2	MATP3540
C		MATP3550
C	CHECK FOR NO INPUT TO DATA BLOCK	MATP3560
610	IF (NMAT.NE.0) GO TO 630	MATP3570
620	FORMAT (1H,44H*** NO MATERIAL PROPERTIES INPUT (MATP). ***)	MATP3580



```

C
C
C
660
670
680
690
700
710
720
730
740

ETI = ET(I)*XEGSIS
IF (IPRINT.EQ.0) GO TO 890
IF (IIUNIT.EQ.0.OR.IIUNIT.EQ.1) GO TO 780

PRINT SI UNIT OUTPUT.

FORMAT (/ ,1H ,8HMATERIAL,3X,A4,17X,5A4)
WRITE (NPRT,660) NAME(I), (TYPA(J,IC), J=1,5)
IF (ICODE(I).EQ.2) GO TO 690
FORMAT (1H ,17HCRUSHING STRENGTH,13X,0PE15.7,2X,6HN/M**2,/,1H ,15H
1YOUNG+S MODULUS,15X,0PE15.7,2X,9HN/M.**2 )
WRITE(NPRT,670) FCFYI,ECI
GO TO 710

FORMAT (1H ,14HYIELD STRENGTH,16X,0PE15.7,2X,6HN/M**2,/,1H ,15HYOUMATP4020
1NGS MODULUS ,15X,0PE15.7,2X,9HN/M.**2 )
WRITE(NPRT,680) FCFYI,ETI
FORMAT (1H ,15HPOISSON+S RATIO,15X,0PE15.7,/,1H ,21HELASTIC SHEAR
1MODULUS,9X,0PE15.7,2X,6HN/M**2,/,1H ,16HMATERIAL DENSITY,14X,0PE15
2.7,2X,6HN/M**3,/,1H ,25HUNLOADING CURVE CONSTANTS,5X,0PE15.7,E15.7
3)
WRITE(NPRT,700) PR(I),GI,DENSI,STSK(8),STN(8,I)
FORMAT (1H ,28HSTRESS-STRAIN CURVE POINTS- )
WRITE (NPRT,720)
IF (IC.NE.2) GO TO 760
FORMAT (1H ,20H STRESS (N/M**2) ,1X,4(0PE14.5),6X,A2,6X,2(0PE14
1.5))
WRITE (NPRT,730) (STSK(K),K=1,4),FT,STSK(6),STSK(7)
FORMAT (1H ,20H STRAIN (M/M) ,1X,4(0PE14.5),6X,A2,12X,A2,6X,
1(0PE14.5),/,76X,44H $$THESE VALUES DEPEND ON STIRRUP SPACING. )
WRITE (NPRT,740) (STN(K,I),K=1,4),FT,STN(7,I)
MATP3390
MATP3900
MATP3910
MATP3920
MATP3930
MATP3940
MATP3950
MATP3960
MATP3970
MATP3980
MATP3990
MATP4000
MATP4010
MATP4020
MATP4030
MATP4040
MATP4050
MATP4060
MATP4070
MATP4080
MATP4090
MATP4100
MATP4110
MATP4120
MATP4130
MATP4140
MATP4150
MATP4160
MATP4170
MATP4180

```



```

750      GO TO 890
760      FORMAT (1H, 20H STRESS (N/M**2) , 1X, 7(0PE14.5))
770      WRITE (NPRT, 750) (STSK(K), K=1, 7)
770      FORMAT (1H, 20H STRAIN (M/M) , 1X, 7(0PE14.5))
770      WRITE (NPRT, 770) (STN(K, I), K=1, 7)
770      GO TO 890
770      PRINT ENGLISH UNIT OUTPUT
770      C
770      C
770      C
770      WRITE (NPRT, 660) NAME(I), (TYPA(J, IC), J=1, 5)
770      IF (ICODE(I).EQ.2) GO TO 810
770      FORMAT (1H, 17HCRUSHING STRENGTH, 13X, 0PE15.7, 2X, 9HLB/IN.**2, /, 1H ,
770      115HYOUNG+S MODULUS, 15X, 0PE15.7, 2X, 9HLB/IN.**2)
770      WRITE (NPRT, 790) FCFYI, ECI
770      GO TO 830
770      FORMAT (1H, 14HYIELD STRENGTH, 16X, 0PE15.7, 2X, 9HLB/IN.**2, /, 1H , 15H
770      1YOUNGS MODULUS , 15X, 0PE15.7, 2X, 9HLB/IN.**2)
770      WRITE (NPRT, 800) FCFYI, ETI
770      FORMAT (1H, 15HPOISSON+S RATIO, 15X, 0PE15.7, /, 1H , 21HELASTIC SHEAR
770      1MODULUS, 9X, 0PE15.7, 2X, 9HLB/IN.**2, /, 1H , 16HMATERIAL DENSITY, 14X, 1PM
770      2E15.7, 2X, 9HLB/IN.**3, /, 1H , 25HUNLOADING CURVE CONSTANTS, 5X, 0PE15.7
770      3, 2X, 0PE15.7)
770      WRITE (NPRT, 820) PR(I), GI, DENSI, STSK(8), STN(8, I)
770      WRITE (NPRT, 720)
770      IF (IC.NE.2) GO TO 870
770      FORMAT (1H, 20H STRESS (LB/IN.**2), 1X, 4(0PE14.5), 6X, A2, 6X, 2(0PE14
770      1.5))
770      WRITE (NPRT, 840) (STSK(K), K=1, 4), FT, STSK(6), STSK(7)
770      FORMAT (1H, 20H STRAIN (IN./IN.) , 1X, 4(0PE14.5), 6X, A2, 12X, A2, 6X,
770      1(0PE14.5), /, 76X, 44H $THESE VALUES DEPEND ON STIRRUP SPACING. )
770      MATP4190
770      MATP4200
770      MATP4210
770      MATP4220
770      MATP4230
770      MATP4240
770      MATP4250
770      MATP4260
770      MATP4270
770      MATP4280
770      MATP4290
770      MATP4300
770      MATP4310
770      MATP4320
770      MATP4330
770      MATP4340
770      MATP4350
770      MATP4360
770      MATP4370
770      MATP4380
770      MATP4390
770      MATP4400
770      MATP4410
770      MATP4420
770      MATP4430
770      MATP4440
770      MATP4450
770      MATP4460
770      MATP4470
770      MATP4480

```



```

980      CONTINUE
990      IF (IERROR(I,6).EQ.0) GO TO 1010
1000     FORMAT (1H,52H*** NEGATIVE CONCRETE OFFSET SPECIFIED FOR MATERIAL
1      ,A4,12H (MATP). ***)
      PRINT 1000, NAME(I)
      ITAG=5
      GO TO 920
1010     IF (IERROR(I,7).EQ.0) GO TO 1030
1020     FORMAT (1H0,47H** VALUE OF POISSON'S RATIO INPUT FOR MATERIAL ,A4,
1      53H IS OUTSIDE ALLOWABLE LIMITS OF 0.0 TO 0.5 (MATP). **)
      PRINT 1020, NAME(I)
      ITAG=6
      GO TO 920
1030     IF (IERROR(I,8).EQ.0) GO TO 1050
1040     FORMAT (1H,52H*** VALUE OF THE ELASTIC SHEAR MODULUS FOR MATERIAL
1      ,A4,40H IS OUTSIDE ALLOWABLE LIMITS (MATP). ***)
      PRINT 1040, NAME(I)
      ITAG=7
      GO TO 920
1050     IF (IERROR(I,9).EQ.0) GO TO 1070
1060     FORMAT (1H0,30H** DENSITY INPUT FOR MATERIAL ,A4,64H LIES OUTSIDE
1      ALLOWABLE LIMITS OF 0.0 TO 0.5 LB/IN**3 (MATP). **)
      PRINT 1060, NAME(I)
      ITAG=8
      GO TO 920
1070     IF (IERROR(I,10).EQ.0) GO TO 1090
1080     FORMAT (1H,48H*** UNLOADING CURVE CONSTANT INPUT FOR MATERIAL ,A4,
1      46H DOES NOT LIE BETWEEN 0.0 AND 1.0 (MATP).***
      PRINT 1080, NAME(I)
      ITAG=9

```

```

MATP4790
MATP4800
MATP4810
MATP4820
MATP4830
MATP4840
MATP4850
MATP4860
MATP4870
MATP4880
MATP4890
MATP4900
MATP4910
MATP4920
MATP4930
MATP4940
MATP4950
MATP4960
MATP4970
MATP4980
MATP4990
MATP5000
MATP5010
MATP5020
MATP5030
MATP5040
MATP5050
MATP5060
MATP5070
MATP5080

```

```

1090 GO TO 920
1100 IF (IERROR(I,11).EQ.0) GO TO 1130
      FORMAT (1H ,59H** VALUE OF CONCRETE CRUSHING STRENGTH INPUT FOR MATERIAL ,A4,53H IS OUTSIDE ALLOWABLE LIMITS FOR INTERNALLY GENERATED,1X,32HSTRESS-STRAIN CURVES (MATP). ***)
      PRINT 1100, NAME(I)
      ITAG=10
      GO TO 910
1130 IF (IERROR(I,13).EQ.0) GO TO 1150
1140 FORMAT (1H ,37H**YIELD STRENGTH INPUT FOR MATERIAL ,A4,64H IS NOT
      1 IN THE ACCEPTABLE RANGE OF 33000 TO 75000 PSI.(MATP)*** )
      PRINT 1140, NAME(I)
      ITAG = 11
      GO TO 910
1150 IF (IERROR(I,14).EQ.0) GO TO 1180
1160 FORMAT (1H ,46H** NO STRESS-STRAIN CURVE INPUT FOR MATERIAL ,A4,12H (MATP). ***)
      PRINT 1160, NAME(I)
      ITAG = 12
      GO TO 920
1180 IF (IERROR(I,15).EQ.0) GO TO 1200
1190 FORMAT (1H ,58H** THE ABSOLUTE VALUES OF THE STRAINS INPUT FOR MATERIAL ,A4,39H ARE NOT IN ASCENDING ORDER (MATP). ***)
      PRINT 1190, NAME(I)
      ITAG = 13
      GO TO 920
1200 IF (IERROR(I,1).EQ.0) GO TO 1220
1210 FORMAT (1H ,56H** MORE MATERIALS INPUT THAN PROGRAM IS CODED TO HANDLE,13,12H (MATP). ***)
      PRINT 1210

```

MATP5090  
MATP5100  
MATP5110  
MATP5120  
MATP5130  
MATP5140  
MATP5150  
MATP5160  
MATP5170  
MATP5180  
MATP5190  
MATP5200  
MATP5210  
MATP5220  
MATP5230  
MATP5240  
MATP5250  
MATP5260  
MATP5270  
MATP5280  
MATP5290  
MATP5300  
MATP5310  
MATP5320  
MATP5330  
MATP5340  
MATP5350  
MATP5360  
MATP5370  
MATP5380



MATP5390  
 MATP5400  
 MATP5410  
 MATP5420  
 MATP5430  
 MATP5440  
 MATP5450  
 MATP5460  
 MATP5470  
 MATP5480  
 MATP5490  
 MATP5500  
 MATP5510  
 MATP5520  
 MATP5530  
 MATP5540  
 MATP5550  
 MATP5560  
 MATP5570  
 MATP5580  
 MATP5590  
 MATP5600  
 MATP5610  
 MATP5620

```

      ITAG = 14
      GO TO 920
1220  CONTINUE
      C
      C CHECK FOR END OF OUTPUT
      C
      IF (IIUNIT.EQ.0.OR.IIUNIT.EQ.2) GO TO 1240
      IF (IERR.GT.IIERR) GO TO 1240
      IF (IPRINT.EQ.0) GO TO 1240
      C
      C CHECK FOR MULTIPLE OUTPUT
      C
      C
      NPAGE = 2
      IF (IIUNIT.EQ.1) IIUNIT = 2
      IF (IIUNIT.EQ.3) IIUNIT = 0
      GO TO 580
      C
      C CHANGE STORED STRESS-STRAIN CURVES TO ORIGINAL UNITS.
      C 1240 IF(IUNITS.EQ.0.OR.IUNITS.EQ.3) GO TO 2021
            DO 2020 I=1,6
            DO 2020 K=1,9
            2020 ST(K,I) = ST(K,I)/EGSISS
            2021 RETURN
            END

```

```

CHATY  0 10
SUBROUTINE MATY (INAME,MATN)
C
C SUBROUTINE TO CALCULATE ELEMENT MATERIAL NUMBERS.
C
COMMON /FIBER/ FDUM(399),ICODE(9),NAME(9)
COMMON /MAINBK/ IDUM1(38),NMAT,IDUM2(10)
MATN = 0
DO 10 J=1,NMAT
IF (INAME.EC.NAME(J)) MATN = J
CONTINUE
RETURN
END
10

```

```

MATY  0
MATY 10
MATY 20
MATY 30
MATY 40
MATY 50
MATY 60
MATY 70
MATY 80
MATY 90
MATY 100
MATY 110

```

```

C      0 10
C      SUBROUTINE MEMB (M,UR,UD,IFLAG)
C
C      THIS SUBROUTINE GENERATES STRESS AND ENERGY CALCULATIONS FOR A
C      GENERAL REINFORCED CONCRETE MEMBER(M). THE CALCULATIONS ARE
C      CONTROLLED BY (IFLAG), WHERE
C      IFLAG=1, INDICATES THAT THE RECOVERABLE STRAIN ENERGY(UR)
C      AND THE DISSIPATIVE STRAIN ENERGY (UD) ARE REQUIRED.
C      IFLAG=3, INDICATES THAT STRESS RESULTS ARE REQUIRED FOR PRINT-
C      OUT AND FOR UPDATING THE STRESS HISTORY DATA BANK.
C      THE ELASTIC-PLASTIC STATUS OF THE MEMBER IS INDICATED BY
C      MSTAT(M), WHERE
C
C      MSTAT=1, INDICATES A MEMBER THAT IS RESTRICTED TO LINEAR
C      ELASTIC RESPONSE.
C      MSTAT=2, INDICATES A MEMBER THAT IS CURRENTLY LINEAR ELASTIC
C      BUT MAY GO INELASTIC.
C      MSTAT=3, INDICATES A MEMBER THAT IS INELASTIC.
C
COMMON/ELEMENT/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BDM(10,45),
1 BWF(45),D(45),DP(45),OPP(45),DWF(45),EFFL(10,45),EFLM(45),
2 HMEM(45),HTOP(45),HTWF(45),POP(7,45),SPRING(5,20),STIES(7,45),
3 TFWF(45),TWF(45),UDM(45),URM(45),XBEG(10,45),
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),
5 YFIBR(11,45),YLOS(45),XDM(45),POF(7,45),DISM(45)
COMMON/STRNBK/SRP(4),SRQ(4),UX,UY,UZ,XLEN,AREA,ZZI,IMAT
C
MEMB 0
MEMB 10
MEMB 20
MEMB 30
MEMB 40
MEMB 50
MEMB 60
MEMB 70
MEMB 80
MEMB 90
MEMB 100
MEMB 110
MEMB 120
MEMB 130
MEMB 140
MEMB 150
MEMB 160
MEMB 170
MEMB 180
MEMB 190
MEMB 200
MEMB 210
MEMB 220
MEMB 230
MEMB 240
MEMB 250
MEMB 260
MEMB 270
MEMB 280

```

C	XLEN=XL(M)	MEMB 290
C	IMAT=MATR(M)	MEMB 300
	UR = 0.E0	MEMB 310
	UD = 0.E0	MEMB 320
		MEMB 330
	CHECK FOR INELASTIC ELEMENT.	MEMB 340
	IF (MSTAT(M).EQ.3) UD = UDM(M)	MEMB 350
		MEMB 360
	DETERMINE LOCAL DEFORMATIONS.	MEMB 370
	CALL DEFO (M)	MEMB 380
		MEMB 390
	DETERMINE CONCRETE ENERGY CONTRIBUTION.	MEMB 400
		MEMB 410
	CALL COEN (M,UR,UD,IFLAG)	MEMB 420
		MEMB 430
	DETERMINE LONGITUDINAL STEEL ENERGY CONTRIBUTION.	MEMB 440
		MEMB 450
	CALL STEN (M,UR,UD,IFLAG)	MEMB 460
		MEMB 470
	STORE TOTAL MEMBER ENERGY.	MEMB 480
		MEMB 490
	IF (IFLAG.NE.3) GO TO 30	MEMB 500
	URM(M)=UR	MEMB 510
	UDM(M)=UD	MEMB 520
	RETURN	MEMB 530
	END	MEMB 540

30



```

COUTS      0 10
C          SUBROUTINE OUTS
C          THIS SUBROUTINE REPORTS ANALYSIS RESULTS AT THE END OF EACH TIME
C          STEP AS FOLLOWS:
C          JOINT STATUS: DISPLACEMENT, VELOCITY AND ACCELERATION; REPORTED
C          . FOR ALL OUTPUT OPTIONS.
C          INTERNAL ENERGY DISTRIBUTION, BY ELEMENTS; REPORTED FOR ALL
C          . OUTPUT OPTIONS.
C          AVERAGE STRESSES AND STRAINS, BY ELEMENTS; REPORTED ONLY FOR
C          . OUTPUT OPTIONS ISTRES = *S* OR *B*.
C          ELEMENT END FORCES, BY ELEMENTS; REPORTED ONLY FOR OUTPUT
C          . OPTIONS ISTRES = *R* OR *B*.
C          SOLUTION ACCURACY - OVERALL ENERGY DISTRIBUTION FOR ALL OUTPUT
C          . OPTIONS; ALSO REPORTED BY JOINTS FOR OUTPUT OPTIONS
C          . IPRINT = *D* OR *E*.
C
COMMON DATA(10000),KDATA(500)
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),JIS(3,50),ERJF(3,50),
1  ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
2  XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1  PI,REFR,RRH,RRZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1  MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2  MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),
1  SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLT,IPRINT,OUTS
1  IREG,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,OUTS
OUTS      0
OUTS     10
OUTS     20
OUTS     30
OUTS     40
OUTS     50
OUTS     60
OUTS     70
OUTS     80
OUTS     90
OUTS    100
OUTS    110
OUTS    120
OUTS    130
OUTS    140
OUTS    150
OUTS    160
OUTS    170
OUTS    180
OUTS    190
OUTS    200
OUTS    210
OUTS    220
OUTS    230
OUTS    240
OUTS    250
OUTS    260
OUTS    270
OUTS    280

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2 NCRD,NDF,NDFD,NDFJ,NDIS,NOL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD, OUTS 290
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE, OUTS 300
4 NTIMES,NVEL,IINITD OUTS 310
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),8MEM(45),8PP(45),8DM(10,45), OUTS 320
1 8WF(45),D(45),DP(45),DPP(45),DMF(45),EFFL(10,45),EFLM(45), OUTS 330
2 HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45), OUTS 340
3 TFWF(45),TWWF(45),UDM(45),URM(45),XBEG(10,45), OUTS 350
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45), OUTS 360
5 YFIBR(11,45),YLOS(45),XOM(45),PDF(7,45),DISM(45) OUTS 370
COMMON/PRNTBK/MPRINT OUTS 380
COMMON/SAVEBK/SAVACC(3,50),SAVAXL(2,45),SAVCRV(2,45),SAVMOM(2,45) OUTS 390
1 ,SAVSHR(2,45),SAVSRP(3,20),SAVSRQ(3,20),SAVXDJ(3,50), OUTS 400
2 SAVVEL(3,50),SVSTRN(12,45),SVSTRS(12,45) OUTS 410
COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB, OUTS 420
1 LTABI,NMAX,NMAXI OUTS 430
COMMON/SEEK8K/DEFOR(90),STPSIZ(90),GRAD(90),GRADI(90),DELTAG(90), OUTS 440
1 DIRECT(90),DIAG(90),STEP(4),DSTEP(4),FVAL(4),VALUES(7), OUTS 450
2 DISACC,SSIZE,FUNACC,FUNMIN,CRITL,CRITU,NLIN OUTS 460
COMMON/STRNBK/SRP(4),SRQ(4),UX,UY,UZ,XLEN,AREA,ZZI,IMAT OUTS 470
DIMENSION TEMP(24),STRESS(30),STRAIN(30),PCTYLD(24),PCTFX(6) OUTS 480
1 ,ENERGY(5,4),ETYPE(3,5),LOCA(3,3) OUTS 490
INTEGER EUNIT(2,2),FUNIT(4,2),SUNIT(3,2),AD(3),LENGTH(2), OUTS 500
2 LABELS(6),KOUT(6),LSA(6),LSB(6),LABEL(5,6),ELA,PLA,TIC,CRA, OUTS 510
3 KED,RUP,URD,CRU,HED,HEAD,DHEAD OUTS 520
DATA LENGTH/3H M.,3HIN./,LABELS/4HUPPE,4HR FL,4HANGE,4HLOWE, OUTS 530
2 4HR FL,4HANGE/,FUNIT/4HNEWT,4HONS,4H MET,4HERS,4HPOUN, OUTS 540
3 4HDS,4HINCH,4HES /,EUNIT/4HNT.-,4H M.,4HIN.-,4H LB./, OUTS 550
4 SUNIT/4H NT.,4H/M.*,4H*2,4H LB.,4H/IN.,4H*2 /,AD/2HDX, OUTS 560
5 2HDX,2HRZ/,LABEL/4HSTEE,4HL,U,4HPPER,4H ,4H ,4HSTEE, OUTS 570
6 4HL,L,4HOWER,4H ,4H ,4HEDGE,4H CON,4HC.,4HUPPE, OUTS 580

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7 4HR ,4HCONF,4H. CO,4HNC.,,4H UPP,4HER ,4HCONF,4H. CO, OUTS 590
8 4HNC.,,4H LOW,4HER ,4HEDGE,4H CON,4HC., ,4HLOWE,4HR /, OUTS 600
9 ELA,PLA,TIC,CRA,KED,RUP,URD,CRU,HED/4HELAS,4HPLAS,4HTIC , OUTS 610
* 4HCRAC,4HKED ,4HRUPT,4MURED,4HCRUS,4HHED / OUTS 620
DATA ETYPE/4HRECO,4HVERA,4HBLE ,4HDISS,4HIPAT,4HIVE ,4HKINE, OUTS 630
1 4HTIC ,4H ,4HTOTA,4HL ,4H ,4HEXTE,4HRNAL,4H / OUTS 640
DATA LOCA/4HUNCO,4HNF. ,4HCONC,4HCONF,4H. CO,4HNC. ,4HREIN, OUTS 650
1 4HF. S,4HTEEL/ OUTS 660
OUTS 670
OUTS 680
OUTS 690
OUTS 700
***** OUTS 710
***** THIS SEGMENT REPORTS THE JOINT STATUS ***** OUTS 720
***** OUTS 730
AD(3) = LABELS FOR DIRECTION COMPONENTS OUTS 740
XDJ(I,J)*DMNSLZ = DISPLACEMENT AT JOINT J IN THE I-DIRECTION OUTS 750
VEL(I,J)*DMNSLZ = VELOCITY AT JOINT J IN THE I-DIRECTION OUTS 760
ACC(I,J)*DMNSLZ = ACCELERATION AT JOINT J IN THE I-DIRECTION OUTS 770
OUTS 780
OUTS 790
OUTS 800
OUTS 810
OUTS 820
OUTS 830
OUTS 840
OUTS 850
6000 WRITE (NPRT,6000) TIME,LENGTH (NDIM),LENGTH(NDIM),LENGTH (NDIM) OUTS 860
2 10X,12HDISPLACEMENT,12X,8HVELOCITY,11X,12HACCELERATION/7X, OUTS 870
3 9HDIIRECTION,11X,A3,6H(RAD.),11X,A3,11H(RAD.)/SEC.,5X,A3, OUTS 880

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4      16H(RAD.)/SEC./SEC./7X,9H-----,10X,12H-----,4X,
5      2(5X,14H-----),5H-----/)
90 DO 100 I=1,3
C
C      CONVERT TO STRUCTURE SCALE FOR OUTPUT
      DMNSLZ = AVGL
      IF(I.EQ.3) DMNSLZ = 1.E0
      TEMP(1) = XDJ(I,JTNUM)*DMNSLZ
      SAVXDJ(I,JTNUM)=TEMP(1)
      TEMP(2) = VEL(I,JTNUM)*DMNSLZ
      IF(ABS(VEL(I,JTNUM)-TINY).LE.EPS) TEMP(2)=0.E0
      SAVVEL(I,JTNUM)=TEMP(2)
      TEMP(3) = ACC(I,JTNUM)*DMNSLZ
      IF(ABS(ACC(I,JTNUM)-TINY).LE.EPS) TEMP(3)=0.E0
      SAVACC(I,JTNUM)=TEMP(3)
      WRITE(NPRT,6010) JTNUM,AD(I),(TEMP(K),K=1,3)
      FORMAT(8X,I2,3X,A2,3(11X,1PE11.4))
6010 100 CONTINUE
      WRITE(NPRT,6020)
6020 FORMAT(1H )
      200 CONTINUE
C
C      PRINT OUT LOCAL ELEMENT DISTORTIONS FOR EXTENSIVE OUTPUT.
      IF(IPRINT.LT.3) GO TO 399
      LINE = NL
      DO 300 M=1,NM
      XLEN = XL(M)
      LINE = LINE + 1
      IF (LINE.LT.NL) GO TO 210
      OUTS 890
      OUTS 900
      OUTS 910
      OUTS 920
      OUTS 930
      OUTS 940
      OUTS 950
      OUTS 960
      OUTS 970
      OUTS 980
      OUTS 990
      OUTS1000
      OUTS1010
      OUTS1020
      OUTS1030
      OUTS1040
      OUTS1050
      OUTS1060
      OUTS1070
      OUTS1080
      OUTS1090
      OUTS1100
      OUTS1110
      OUTS1120
      OUTS1130
      OUTS1140
      OUTS1150
      OUTS1160
      OUTS1170
      OUTS1180

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CALL PAGE
LINE = LINE + 4
WRITE(NPRT,6025) LENGTH(NDIM),TIME
FORMAT(15X,27HLOCAL ELEMENT DISTORTIONS (,A3,10H,RAD.) AT ,1PE14.7OUTS1220
1,8H SECONDS//5X,7HELEMENT,6X,5HNODES,6X,9HXDM OR U4,9X,8HUX OR U1,OUTS1230
29X,8HUY OR U2,9X,8HUZ OR U3//)
CALL DEFO(M)
WRITE(NPRT,6026) M,IP(M),IQ(M),XDM(M),UX,UY,UZ
FORMAT(8X,I2,6X,I2,4H TO ,I2,4(3X,1PE14.7))
***** THIS SEGMENT REPORTS THE INTERNAL ENERGY DISTRIBUTION *****
***** THIS SEGMENT REPORTS THE INTERNAL ENERGY DISTRIBUTION *****
***** THIS SEGMENT REPORTS THE INTERNAL ENERGY DISTRIBUTION *****
***** THIS SEGMENT REPORTS THE INTERNAL ENERGY DISTRIBUTION *****
IP(M) = JOINT AT P-END OF MEMBER M
IQ(M) = JOINT AT Q-END OF MEMBER M
URM(M) = RECOVERABLE ENERGY OF MEMBER M
UDM(M) = DISSIPATED ENERGY OF MEMBER M
SYSUR = TOTAL RECOVERABLE SYSTEM ENERGY
SYSUD = TOTAL DISSIPATED SYSTEM ENERGY
SYSU = TOTAL SYSTEM ENERGY

SYSUR = 0.E0
SYSUD = 0.E0
SYSU = 0.E0
LINE = NL
DO 400 M=1,NM
IF(MTYPE(M).NE.4) CALL MEMB(M,UR,UD,1)
IF(MTYPE(M).EQ.4) CALL WIDE(M,UR,UD,1)
SYSUR = SYSUR + URM(M)
SYSUD = SYSUD + UDM(M)

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OUTS1190
OUTS1200
OUTS1210
OUTS1220
OUTS1230
OUTS1240
OUTS1250
OUTS1260
OUTS1270
OUTS1280
OUTS1290
OUTS1300
OUTS1310
OUTS1320
OUTS1330
OUTS1340
OUTS1350
OUTS1360
OUTS1370
OUTS1380
OUTS1390
OUTS1400
OUTS1410
OUTS1420
OUTS1430
OUTS1440
OUTS1450
OUTS1460
OUTS1470
OUTS1480

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400 CONTINUE
  IF(NLS.EQ.0) GO TO 420
  DO 410 L=1,NLS
    CALL LEAF(-L,UR,1)
    SYSUR = SYSUR + UR
  410 CONTINUE
  420 SYSU = SYSUR+SYSUD
    IF(SYSUR.EQ.0.E0) SYSUR=TINY
    IF(SYSUD.EQ.0.E0) SYSUD=TINY
    IF(SYSU.EQ.0.E0) SYSU=TINY
    DO 500 M=1,NM
      TEMP(1) = URM(M)
      TEMP(2) = UDM(M)
      TEMP(3) = TEMP(1)+TEMP(2)
      TEMP(4) = TEMP(1)/SYSUR
      TEMP(5) = TEMP(2)/SYSUD
      TEMP(6) = TEMP(3)/SYSU
      LINE = LINE + 2
    IF(LINE.LT.NL) GO TO 490
    CALL PAGE
    LINE = LINE + 6
    WRITE(NPRT,6030) (EUNIT(J,NDIM),J=1,2),TIME
6030 FORMAT(18X,17HINTERNAL ENERGY (,2A4,21H) - - DISTRIBUTION AT,
  * 1PE11.4,8H SECONDS//
  2 1X,7HELEMENT,4X,11HRECOVERABLE,5X,10HDISSIPATED,7X,7HELEMENT,OUTS1730
  3 6X,3(10HPERCENT OF,5X)/1X,8HIDENTITY,6X,2(6HENERGY,9X),OUTS1740
  4 6HENERGY,7X,11HRECOVERABLE,4X,10HDISSIPATED,4X,10HPARTICIPAT,OUTS1750
  5 3HION/1X,8H-----,6(3X,12H-----),1H-/OUTS1760
490 WRITE(NPRT,6040) IP(M),IQ(M),(TEMP(N),N=1,6)
6040 FORMAT(2X,12,1H-,12,1X,3(4X,0PE11.4),6X,3(2PF8.3,7X)/)
OUTS1490
OUTS1500
OUTS1510
OUTS1520
OUTS1530
OUTS1540
OUTS1550
OUTS1560
OUTS1570
OUTS1580
OUTS1590
OUTS1600
OUTS1610
OUTS1620
OUTS1630
OUTS1640
OUTS1650
OUTS1660
OUTS1670
OUTS1680
OUTS1690
OUTS1700
OUTS1710
OUTS1720
OUTS1730
OUTS1740
OUTS1750
OUTS1760
OUTS1770
OUTS1780

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C      500 CONTINUE
C      IF(ISTRES.NE.1.AND.ISTRES.NE.3 ) GO TO 2999
C      ***** THIS SEGMENT REPORTS AVERAGE STRESSES AND *****
C      ***** STRAINS FOR A REINFORCED CONCRETE ELEMENT *****
C      *****
C      LINE = NL
C      DO 1110 M=1,NM
C      C      VERIFY ELEMENT TYPE
C      C      IF(MTYPE(M).GE.4) GO TO 1110
C      C      NGRPM = NGRP(M)
C      C      XLEN = XL(M)
C      C      AREA = HMEN(M)*BMEM(M)
C      C      FIND GROUP NUMBERS OF UPPER AND LOWER STEEL GROUPS
C      C      TEMPA = HTOP(M)-D(M)
C      C      TEMPB = HTOP(M)-DP(M)
C      C      ITOP = 1
C      C      IBOT = 1
C      C      DO 600 I=1,NGRPM
C      C      IF(ABS((YBAR(I,M))-TEMPA).LE.1.E-2) IBOT = I
C      C      IF(ABS((YBAR(I,M))-TEMPB).LE.1.E-2) ITOP = I
C      C      600 CONTINUE
C      C      COLLECT MEMBER DIMENSIONS AND MATERIAL PROPERTIES
C      C      TEMP(1) = YBAR(ITOP,M)

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OUTS1790  
 OUTS1800  
 OUTS1810  
 OUTS1820  
 OUTS1830  
 OUTS1840  
 OUTS1850  
 OUTS1860  
 OUTS1870  
 OUTS1880  
 OUTS1890  
 OUTS1900  
 OUTS1910  
 OUTS1920  
 OUTS1930  
 OUTS1940  
 OUTS1950  
 OUTS1960  
 OUTS1970  
 OUTS1980  
 OUTS1990  
 OUTS2000  
 OUTS2010  
 OUTS2020  
 OUTS2030  
 OUTS2040  
 OUTS2050  
 OUTS2060  
 OUTS2070  
 OUTS2080

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TEMP(2) = YBAR(IBOT,M)
TEMP(3) = YFIBR( 1,M)
TEMP(4) = YFIBR( 2,M)
TEMP(5) = YFIBR(10,M)
TEMP(6) = YFIBR(11,M)
KOUT(1) = MBAR(ITOP,M)
KOUT(2) = MBAR(IBOT,M)
KOUT(3) = MCODE(M)
KOUT(4) = MATR (M)
KOUT(5) = MATR (M)
KOUT(6) = MCODE(M)
DO 1100 L=1,2
IF(MSTAT(M).EQ.3) GO TO 900

C
C STRESS AND STRAIN COMPUTATIONS FOR AN ELASTIC MEMBER
XLOC = 0.E0
IF(L.EQ.2) XLOC = XLEN
CALL DEFO(M)
DO 800 K=1,6
CALL STRN(M,XLOC,TEMP(K),STRAIN(K))
LSA(K) = ELA
LSB(K) = TIC
IF(K.GE.3.AND.STRAIN(K).GT.0.E0) GO TO 720
J = KOUT(K)
STRESS(K) = EC(J)*STRAIN(K)
IF (STRAIN(K).GT.0.E0) STRESS(K) = ET(J)*STRAIN(K)
PCTYLD(K) = ABS(STRESS(K)/FCFY(J))
IF(PCTYLD(K).GE.1.E0) PCTYLD(K) = 1.E0
PCTFX(K) = ABS(STRAIN(K)/STN(7,J))
IF(PCTFX(K).GE.1.E0) PCTFX(K) = 1.E0
OUTS2090
OUTS2100
OUTS2110
OUTS2120
OUTS2130
OUTS2140
OUTS2150
OUTS2160
OUTS2170
OUTS2180
OUTS2190
OUTS2200
OUTS2210
OUTS2220
OUTS2230
OUTS2240
OUTS2250
OUTS2260
OUTS2270
OUTS2280
OUTS2290
OUTS2300
OUTS2310
OUTS2320
OUTS2330
OUTS2340
OUTS2350
OUTS2360
OUTS2370
OUTS2380

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          KC = 32
          IF(K.EQ.3.OR.K.EQ.6) GO TO 990
          KA = 152
          KB = 72
          KC = 64
          990 IF(K.EQ.3.OR.K.EQ.4) KC = 0
              INDEX = KDATA(LPSI+M)-1+NGRP(M)*40+KA+KC+(L-1)*KB+168
          C
          C      COLLECT STRESS HISTORY DATA
          DO 1000 KK=1,8
              S(KK) = DATA(INDEX+KK)
          1000 CONTINUE
              STRESS(K) = S(6)
              IF(STRAIN(K).GT.(S(8)+STN(1,J))) GO TO 1040
              IF(STRAIN(K).LT.STN(7,J)) GO TO 1030
              L8(K) = TIC
              IF(S(8).GT.0.E0) GO TO 1010
              LSA(K) = ELA
              PCTYLD(K) = STRESS(K)/STS(2,J)
              IF(PCTYLD(K).GE.1.E0) PCTYLD(K) = 1.E0
              GO TO 1020
          1010 LSA(K) = PLA
              PCTYLD(K) = 1.E0
          1020 PCTFX(K) = STRAIN(K)/STN(7,J)
              IF(PCTFX(K).GE.1.E0) PCTFX(K) = 1.E0
              GO TO 1060
          1030 LSA(K) = CRU
              L8(K) = HED
              GO TO 1050
          1040 LSA(K) = CRA

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OUTS2990
OUTS3000
OUTS3010
OUTS3020
OUTS3030
OUTS3040
OUTS3050
OUTS3060
OUTS3070
OUTS3080
OUTS3090
OUTS3100
OUTS3110
OUTS3120
OUTS3130
OUTS3140
OUTS3150
OUTS3160
OUTS3170
OUTS3180
OUTS3190
OUTS3200
OUTS3210
OUTS3220
OUTS3230
OUTS3240
OUTS3250
OUTS3260
OUTS3270
OUTS3280

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      LSB(K) = KED
1050 PCTYLD(K) = 1.E0
      PCTFX(K) = 1.E0
1060 CONTINUE
C
C      PRINTING SECTION
C
1070 DO 1075 K=1,6
      SVSTRS((L-1)*6+K,M) = STRESS(K)
      SVSTRN((L-1)*6+K,M) = STRAIN(K)
1075 CONTINUE
      LINE = LINE + 7
      IF(LINE.LT.NL) GO TO 1080
      CALL PAGE
      LINE = LINE + 16
      WRITE(NPRT,6050) (SUNIT(J,NDIM), J=1,3), TIME
6050 FORMAT(14X,18H AVERAGE STRESSES (,3A4,
      * 33H) IN REINFORCED CONCRETE ELEMENTS,
      2 3H AT,1PE11.4,8H SECONDS//21X,11HSIT f IN THE,2X,2(9X,6HNORMAL OUTS3470
      3 ),6X,7HLOADING,2(4X,7HPERCENT),3H OF/1X,3HEND,3X,7HELEMENT,6XOUTS3480
      4 ,13HCROSS SECTION,10X,6HSTRESS,9X,6HSTRAIN,7X,5HSTATE,4X, OUTS3490
      5 9HOF YIELD,4X,8HFRACTURE/1X,3H-----,3X,7H-----,3X,7H-----, OUTS3500
      6 13H-----,2(3X,12H-----),3X,7H-----,3X, OUTS3510
      7 9H-----,3X,10H-----//)
1080 IPQ = IP(M)
      IF(L.EQ.2) IPQ = IQ(M)
      WRITE(NPRT,6060) IPQ,IP(M),IQ(M), ((LABEL(J,K), J=1,5),STRESS(K),
      2 STRAIN(K),LSA(K),LSB(K),PCTYLD(K),PCTFX(K),K=1,6)
6060 FORMAT(1X,I2,5X,I2,1H-,I2,6(T18,5A4,2X,2(1PE11.4,4X),2A4,2X,
      2 2 (2PF8.3,5X))// )
OUTS3290
OUTS3300
OUTS3310
OUTS3320
OUTS3330
OUTS3340
OUTS3350
OUTS3360
OUTS3370
OUTS3380
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OUTS3490
OUTS3500
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OUTS3560
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1100 CONTINUE
1110 CONTINUE
      IF (IPRINT.LT.3) GO TO 1999
C
C
C      PRINT STRESSES AND STRAINS AT GAUSS POINTS FOR EXTENSIVE OUTPUT.
      LINE = NL
      DO 1800 M=1,NM
C
C          VERIFY ELEMENT TYPE.
          IF(MTYPE(M).GE.4) GO TO 1800
          NGRPM=NGRP(M)
          XLEN = XL(M)
          IF(MSTAT(M).NE.3) CALL CEFO(M)
          DO 1790 K=1,3
              IL = 0
              GO TO (1710,1720,1730),K
              UNCONFINED CONCRETE.
              KN = 7
              J = MCODE(M)
              IF (MSTAT(M).EQ.3) GO TO 1715
              ELASTIC COMPUTATIONS.
              DO 1714 I=1,7
                  IF(K.EQ.2.AND.(I.LE.2.OR.I.GE.6)) GO TO 1714
                  DO 1712 L=1,3
                      IL = IL +1
                      CALL STRN(M,XPI(L,M),YGP(I,M),STRAIN(IL))
                      ELASMD = ET(J)
                      IF (STRAIN(IL).LT.0.E0) ELASMD = EC(J)
                      STRESS(IL) = ELASMD*STRAIN(IL)
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1712 CONTINUE
1714 CONTINUE
GO TO 1740
1715 KRESS = KDATA(LPSI+M) - 1 + 40*NGRP(M)
KRAIN = KDATA(LPI+M) - 1 + 5*NGRP(M)
1716 IL = 3*KN
DO 1718 L=1,IL
STRAIN(L) = DATA(KRAIN+L)
STRESS(L) = DATA(KRESS+8*L-2)
IF (STRAIN(L).GT.(STN(1,J)+DATA(KRESS+8*L))) STRESS(L) = 0.E0
1718 CONTINUE
GO TO 1740
C
1720 KN = 3
J = MATR(M)
IF (MSTAT(M).NE.3) GO TO 1711
KRESS = KDATA(LPSI+M) - 1 + 40*NGRP(M) + 248
KRAIN = KDATA(LPI+M) - 1 + 5*NGRP(M) + 31
GO TO 1716
C REINFORCING STEEL.
KN = NGRP(M)
1730 KRESS = KDATA(LPSI+M) - 1
KRAIN = KDATA(LPI+M) - 1
IF (KN.EQ.0) GO TO 1790
DO 1734 I=1,KN
J = MBAR(I,M)
DO 1733 L=1,3
IL = IL + 1
IF (MSTAT(M).EQ.3) GO TO 1732
CALL STRN(M,XPI(L,M),YBAR(I,M),STRAIN(IL))
OUTS3890
OUTS3900
OUTS3910
OUTS3920
OUTS3930
OUTS3940
OUTS3950
OUTS3960
OUTS3970
OUTS3980
OUTS3990
OUTS4000
OUTS4010
OUTS4020
OUTS4030
OUTS4040
OUTS4050
OUTS4060
OUTS4070
OUTS4080
OUTS4090
OUTS4100
OUTS4110
OUTS4120
OUTS4130
OUTS4140
OUTS4150
OUTS4160
OUTS4170
OUTS4180

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1732 ELASMD = ET(J)
1733 IF (STRAIN(IL).LT.0.E0) ELASMD = EC(J)
1734 STRESS(IL) = ELASMD*STRAIN(IL)
C GO TO 1733
C STRAIN(IL) = DATA(KRAIN+IL)
C STRESS(IL) = DATA(KRESS+IL*8)
1733 IF (STRAIN(IL).LT.DATA(KRESS+IL*8-3)) STRESS(IL)=-STRESS(IL)
1734 CONTINUE
C CONTINUE
C PRINT OUT HEADING.
1740 LINE = LINE + KN + 1
IF (LINE.LT.NL) GO TO 1750
CALL PAGE
LINE = LINE + KN + 5
WRITE(NPRT,6070) (SUMIT(JS,NOIM),JS=1,3),TIME
6070 FORMAT(14X,18HAVERAGE STRESSES (,3A4,52H) AT GAUSS POINTS OF REINF
FORCED CONCRETE ELEMENTS AT,1PE11.4,8H SECONDS//7X,7HELEMENT,5X,
25HNODES,5X,9HLOCATION , 3(9X,6HSTRESS,9X,6HSTRAIN)/)
1750 CONTINUE
C
C PRINT OUT RESULTS.
WRITE(NPRT,6071) M,IP(M),IQ(M),(LOCA(I,K),I=1,3),
(STRESS(L),STRAIN(L),L=1,3)
1 6071 FORMAT(10X,I2,5X,I2,4H TO ,I2,2X,3A4,1X,6(4X,1PE11.4))
IF (IL.LE.3) GO TO 1790
WRITE(NPRT,6072) (STRESS(L),STRAIN(L),L=4,IL)
6072 FORMAT ((40X,6(4X,1PE11.4))/)
1790 CONTINUE
1800 CONTINUE

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OUTS4190  
 OUTS4200  
 OUTS4210  
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 OUTS4280  
 OUTS4290  
 OUTS4300  
 OUTS4310  
 OUTS4320  
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 OUTS4340  
 OUTS4350  
 OUTS4360  
 OUTS4370  
 OUTS4380  
 OUTS4390  
 OUTS4400  
 OUTS4410  
 OUTS4420  
 OUTS4430  
 OUTS4440  
 OUTS4450  
 OUTS4460  
 OUTS4470  
 OUTS4480





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                IF(PCTFX(K).GE.1.E0) PCTFX(K) = 1.E0
                2000 CONTINUE
                GO TO 2070
C
C      STRESS AND STRAIN DATA COLLECTION FOR YIELDED ELEMENTS
C
C      2010 INDEX = KDATA(LPI+M)+21
C            STRAIN(1) = DATA(INDEX+(L-1)*11)
C            STRAIN(2) = DATA(INDEX+(L-1)*11+10)
C
C      STRESSES AND FAILURE CRITERIA AT TOP AND BOTTOM FLANGES
C
C            INDEX = KDATA(LPSI+M) -1
C            DO 2060 K=1,2
C              JJ = (K-1)*80+(L-1)*88+168
C              DO 2030 KK=1,8
C                S(KK) = DATA(INDEX+JJ+KK)
C              2030 CONTINUE
C            IF (S(1).LE.0.5E0) GO TO 2050
C            PCTYLD(K) = 1.E0
C            PCTFX(K) = 1.E0
C            STRESS(K) = 0.E0
C            LSA(K) = RUP
C            LSB(K) = URD
C            GO TO 2060
C      2050 POSNEG = -1.E0
C            IF(STRAIN(K)-S(5).GE.0.E0) POSNEG = 1.E0
C            STRESS(K) = S(8)*POSNEG
C            LSB(K) = TIC
C            LSA(K) = ELA
C            IF(ABS(S(6)).GE.1.E-4) LSA(K) = PLA

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OUTS4790
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OUTS4900
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OUTS4920
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OUTS4950
OUTS4960
OUTS4970
OUTS4980
OUTS4990
OUTS5000
OUTS5010
OUTS5020
OUTS5030
OUTS5040
OUTS5050
OUTS5060
OUTS5070
OUTS5080

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2060 KM = INT(S(2))*6 + 2
      PCTYLD(K) = S(8)/STS(KM,J)
      IF(PCTYLD(K).GE.1.E0) PCTYLD(K) = 1.E0
      PCTFX(K) = (STRAIN(K)-S(5))/(POSNEG*STN(7,J))
      IF(PCTFX(K).GE.1.E0) PCTFX(K) = 1.E0
      CONTINUE
C
C      PRINTING SECTION
C
2070 DO 2075 K=1,2
      SVSTRS((L-1)*2+K,M) = STRESS(K)
      SVSTRN((L-1)*2+K,M) = STRAIN(K)
      CONTINUE
2075 LINE = LINE + 3
      IF(LINE.LT.NL) GO TO 2080
      CALL PAGE
      LINE = 7
      WRITE(NPRT,6210) (SUNIT(JS,NDIM),JS=1,3), TIME
6210 FORMAT(13X,18H AVERAGE STRESSES (,3A4,
      * 38H) IN NONCOMPOSITE WIDE FLANGE ELEMENTS,
      2 3H AT,1PE11.4,8H SECONDS//21X,11H SITE IN THE,2X,2(9X,6HNORMAL
      3 ),6X,7HLOADING,2(4X,7HPERCENT),3H OF/1X,3HEND,3X,7HELEMENT,6X
      4 ,13HCROSS SECTION,10X,6HSTRESS,9X,6HSTRAIN,7X,5HSTATE,4X,
      5 9HOF YIELD,4X,8H FRACTURE/1X,3H-----,3X,7H-----,
      6 13H-----,2(3X,12H-----),3X,7H-----,3X,
      7 9H-----,3X,10H-----/)
2080 IPQ = IP(M)
      IF(L.EQ.2) IPQ = IQ(M)
      WRITE(NPRT,6220) IPQ,IP(M),IQ(M), (LABELS(K),K=1,3),STRESS(1),
      2 STRAIN(1),LSA(1),LSB(1),PCTYLD(1),PCTFX(1), (LABELS(K),K=4,6),OUTS5380
OUTS5090
OUTS5100
OUTS5110
OUTS5120
OUTS5130
OUTS5140
OUTS5150
OUTS5160
OUTS5170
OUTS5180
OUTS5190
OUTS5200
OUTS5210
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OUTS5230
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OUTS5370
OUTS5380

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3      STRESS(2), STRAIN(2), LSA(2), LSB(2), PCTYLD(2), PCTFX(2)
6220  FORMAT(1X,I2,5X,I2,1H-,I2,8X,3A4, 7X,2(1PE11.4,4X),2A4,2X,
2      2(2PF8.3,5X)/21X,3A4, 7X,2(1PE11.4,4X),2A4,2X,2(2PF8.3,5X)/)
2090  CONTINUE
2100  CONTINUE
      IF (IPRINT.LT.3) GO TO 2999

C      PRINT STRESSES AND STRAINS AT GAUSS POINTS FOR EXTENSIVE OUTPUT.
      LINE = NL
      DO 2150 M=1,NM

C
C      VERIFY ELEMENT TYPE.
      IF (MTYPE(M).NE.4) GO TO 2150
      J = MATW(M)
      LINE = LINE + 8
      IF (LINE.LT.NL) GO TO 2180
      CALL PAGE
      LINE = 8
      WRITE(NPRT,6211) (SUNIT(JS,NDIM),JS=1,3), TIME
6211  FORMAT (11X,18H AVERAGE STRESSES (,3A4,44H) AT GAUSS POINTS OF WIDE
2      1 FLANGE ELEMENTS AT,1PE11.4,8H SECONDS//7X,7HELEMENT,5X,6HNODES ,
2      2 3(9X,6HSTRESS,9X,6HSTRAIN)/)
2180  CONTINUE
      IF (MSTAT(M).EQ.3) GO TO 2186

C      STRESS AND STRAIN COMPUTATIONS FOR AN ELASTIC ELEMENT.
      XLEN = XL(M)
      CALL DEFO(M)
      IK = 0
      DO 2184 I=1,7

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OUTS5390
OUTS5400
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5000 CALL PAGE
C
C   COMPUTE KINETIC ENERGY.
VALUES(5) = 0.E0
IF (NHAS.EQ.0) GO TO 6501
DO 6500 I=1,NDF J
J = IDFI(I)
K = IDFII(I)
6500 VALUES(5) = VALUES(5) + 0.5E0*DAS(K,J)*VEL(K,J)**2
C
C   SYSTEM ENERGIES.
6501 IF (TIME.GT.TBEGIN) GO TO 6503
EBEGIN = VALUES(5)
PBEGIN = -0.5E0*VALUES(2)
POTEN = 0.E0
DO 6502 I=1,5
DO 6502 J=1,4
6502 ENERGY(I,J) = 0.E0
6503 ENERGY(1,3) = VALUES(3)
ENERGY(2,3) = VALUES(4)
ENERGY(3,3) = VALUES(5)
ENERGY(4,3) = VALUES(3)+VALUES(4)+VALUES(5)
ENERGY(5,3) = EBEGIN + POTEN - 0.5E0*VALUES(2)
IF (IANAL.EQ.1) POTEN = PBEGIN
DO 6504 I=1,5
6504 ENERGY(I,2) = ENERGY(I,3) - ENERGY(I,1)
IF (ENERGY(I,1).GT.TINY) ENERGY(I,4)=ENERGY(I,2)/ENERGY(I,1)*100.E0
IF (ENERGY(I,2).EQ.0.E0) ENERGY(I,4) = 0.E0
CONTINUE
6504 WRITE(NPRT,6508) TIME, (FUNIT(K,NDIM),K=1,4)

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OUTS6900
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OUTS6960
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OUTS6980
OUTS6990
OUTS7000
OUTS7010
OUTS7020
OUTS7030
OUTS7040
OUTS7050
OUTS7060
OUTS7070
OUTS7080
OUTS7090
OUTS7100
OUTS7110
OUTS7120
OUTS7130
OUTS7140
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OUTS7160
OUTS7170
OUTS7180

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6508  FORMAT(29X,20HSOLUTION ACCURACY AT,1PE11.4,8H SECONDS//36X,
      1  8HUNITS - ,4A4//41X,15HSYSTEM ENERGIES//27X,7HINITIAL,10X,
      2  6HCHANGE,10X,5HFINAL,7X,15HPER CENT CHANGE/10X,11(1H=),4(4X,
      3  12(1H=))//
      DO 6510 I=1,5
      IF (ENERGY(I,1).GT.TINY.OR.ENERGY(I,2).EQ.0.E0)
      1  WRITE(NPRT,6512) (ETYPE(K,I),K=1,3),(ENERGY(I,J),J=1,4)
      IF (ENERGY(I,1).LE.TINY.AND.ENERGY(I,2).NE.0.E0)
      1  WRITE(NPRT,6514) (ETYPE(K,I),K=1,3),(ENERGY(I,J),J=1,3)
      IF (I.EQ.3) WRITE (NPRT,6515)
      IF (I.EQ.4) WRITE (NPRT,6516)
      CONTINUE
6510  WRITE (NPRT,6516)
      FORMAT (10X,3A4,3X,3(1PE12.4,4X),0PG12.4)
6512  FORMAT (10X,3A4,3X,3(1PE12.4,4X),2X,8HINFINITE)
6514  FORMAT (21X,4(4X,12(1H=)))
6516  FORMAT (21X,4(4X,12(1H=)))
      DO 6518 I=1,5
6518  ENERGY(I,1) = ENERGY(I,3)
      LINE = 25
      WRITE (NPRT,6520)
6520  FORMAT(/8X,9HJOINT AND,7X,8HVALUE OF,7X,8HRESIDUAL,9X,8HRESIDUAL,
      2  6X,11HREL. ENERGY/8X,9HDIRECTION,5X,12HIMPOSED LOAD,4X,
      3  11HFORCE, MAX.,5X,12HENERGY, MAX.,7X,5HERROR/8X,9H-----,
      4  2(5X,12H-----,4X,11H-----)/)
      DO 5020 J=1,NJ
      LINE = LINE + 4
      IF(LINE.LT.NL) GO TO 5010
      CALL PAGE
      LINE = 8

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OUTS7190  
OUTS7200  
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OUTS7430  
OUTS7440  
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OUTS7480

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5010      WRITE(NPRT,6520)
        DO 5015 I=1,3
          DMNSLZ=AVGL
          IF(I.EQ.3) DMNSLZ=1.E0
          F(I,J) = F(I,J)/DMNSLZ
          WRITE(NPRT,6530)  J,AD(I),F(I,J),DER(I,J),RESENG(I,J),ERJF(I,J)
6530      FORMAT(1H, 9X,I2,3X,A2,1X,4(5X,1PE11.4))
          F(I,J)=F(I,J)*DMNSLZ
5015      CONTINUE
        WRITE(NPRT,6020)
5020      CONTINUE
        RETURN
        END
OUTS7490
OUTS7500
OUTS7510
OUTS7520
OUTS7530
OUTS7540
OUTS7550
OUTS7560
OUTS7570
OUTS7580
OUTS7590
OUTS7600
OUTS7610

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CPAGE	0	10		PAGE	0
			SUBROUTINE PAGE		
C				PAGE	10
C			THIS SUBROUTINE PRINTS PROBLEM TITLE AND PAGE NO.	PAGE	20
C				PAGE	30
			COMMON/LEADBK/IDUM1(29),HEAD(20),IDUM2(11)	PAGE	40
			COMMON/MAINBK/JD1(6),IPAGE,JD2(10),LINE,J03(24),NPRT,J04(6)	PAGE	50
			COMMON/PRNTBK/MPRINT	PAGE	60
			INTEGER HEAD	PAGE	70
				PAGE	80
C			IF (MPRINT.EQ.0.AND.IPAGE.GT.0) GO TO 30	PAGE	90
			IPAGE = IPAGE + 1	PAGE	100
20			FORMAT (1H1,5X,20A4,25X,4HPAGE,I5//)	PAGE	110
			WRITE (NPRT,20) HEAD,IPAGE	PAGE	120
			LINE = 12	PAGE	130
			RETURN	PAGE	140
30			WRITE (NPRT,40)	PAGE	150
40			FORMAT (1H0)	PAGE	160
			LINE = 3	PAGE	170
			RETURN	PAGE	180
			END	PAGE	190

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CPLOG      0 10
SUBROUTINE PLOG(IT)
C
C THIS SUBROUTINE SAVES THE PLOT FILE.
C
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DI,EPS,HEAD(20),
1 PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,PLOG
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCH,PLOG
2 NCRO,NDF,NDFD,NDFJ,NDIS,NOL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,PLOG
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,PLOG
4 NTIMES,NVEL,IINITD,PLOG
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BDM(10,45),PLOG
1 BWF(45),D(45),DP(45),OPP(45),OWF(45),EFL(10,45),EFLM(45),PLOG
2 HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),PLOG
3 TFWF(45),TWWF(45),UDM(45),URM(45),XBE(10,45),PLOG
4 XBE(45),XBE(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),PLOG
5 YFIBR(11,45),YLOS(45),XDM(45),PDF(7,45),DISM(45),PLOG
COMMON /PLOTBK/ ITER,PLOG
COMMON/SAVEBK/SAVACC(3,50),SAVAXL(2,45),SAVCRV(2,45),SAVMOM(2,45),PLOG
1 ,SAVSHR(2,45),SAVSRP(3,20),SAVSRQ(3,20),SAVXDJ(3,50),PLOG
2 SAVVEL(3,50),SVSTRN(12,45),SVSTRS(12,45),PLOG
INTEGER HEAD,DHEAD,PLOG
IF (ITER.GT.0) GO TO 20,PLOG
REWIND IT,PLOG
WRITE (IT) (HEAD(I),I=1,20),PLOG
WRITE (IT) IUNITS,NDF,NJ,NM,NLS,(IP(M),IQ(M),M=1,NM),PLOG

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AD-A038 317

VIRGINIA POLYTECHNIC INST AND STATE UNIV BLACKSBURG --ETC F/G 13/13  
RELIABILITY STUDY OF SINGER. VOLUME II. USER'S MANUAL.(U)  
JAN 77 A E SOMERS, S M HOLZER, J C BRADSHAW F29601-75-C-0050

UNCLASSIFIED

AFWL-TR-76-192-VOL-2

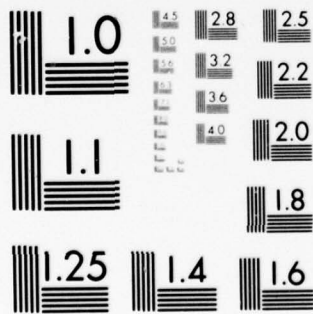
NL

4 OF 4  
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END

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38317



MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

20	WRITE (IT) (MTYPE (M), M=1, NM)	PLOG 290
	CONTINUE	PLOG 300
	ITER = ITER+1	PLOG 310
	WRITE (IT) ITER, TIME	PLOG 320
	DO 21 I=1, 3	PLOG 330
21	WRITE (IT) (SAVXOJ(I, J), J=1, NJ)	PLOG 340
	DO 22 I=1, 3	PLOG 350
22	WRITE (IT) (SAVACC(I, J), J=1, NJ)	PLOG 360
	DO 23 I=1, 3	PLOG 370
23	WRITE (IT) (SAVVEL(I, J), J=1, NJ)	PLOG 380
	WRITE (IT) (URM(M), M=1, NM)	PLOG 390
	WRITE (IT) (UDM(M), M=1, NM)	PLOG 400
	DO 24 I=1, 2	PLOG 410
24	WRITE (IT) (SAVCRV(I, M), M=1, NM)	PLOG 420
	DO 25 I=1, 2	PLOG 430
25	WRITE (IT) (SAVMOM(I, M), M=1, NM)	PLOG 440
	DO 26 I=1, 2	PLOG 450
26	WRITE (IT) (SAVSHR(I, M), M=1, NM)	PLOG 460
	DO 27 I=1, 2	PLOG 470
27	WRITE (IT) (SAVAXL(I, M), M=1, NM)	PLOG 480
	IF (NLS.EQ.0) GO TO 30	PLOG 490
	DO 28 I=1, 3	PLOG 500
28	WRITE (IT) (SAVSRP(I, M), M=1, NLS)	PLOG 510
	DO 29 I=1, 3	PLOG 520
29	WRITE (IT) (SAVSRQ(I, M), M=1, NLS)	PLOG 530
30	CONTINUE	PLOG 540
	DO 31 I=1, 12	PLOG 550
31	WRITE (IT) (SVSTRS(I, M), M=1, NM)	PLOG 560
	DO 32 I=1, 12	PLOG 570
32	WRITE (IT) (SVSTRN(I, M), M=1, NM)	PLOG 580

C  
C \*\*\*\*\* GLOSSARY FOR PLOG \*\*\*\*\*  
C  
RETURN  
END

PLOG 590  
PLOG 600  
PLOG 610  
PLOG 620  
PLOG 630



```

CPOTE 0 10
SUBROUTINE POTE (SOLN,VALUE)
C
C THIS SUBROUTINE CALCULATES THE VALUE OF THE POTENTIAL FUNCTION FORPOTE
C SPECIFIED VARIABLES.
C
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),DIS(3,50),ERJF(3,50),
1 ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
1 XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1 PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,POTE
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCH,POTE
2 NCRO,NDF,NDFJ,NDIS,NDL,NFF,NJOR,PINC,NJ,NJD,NJER,NL,NLD,
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRI,NSAVE,NTAB,NTAPE,
4 NTIMES,NVEL,IINITD
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),8MEM(45),8PP(45),8DM(10,45),POTE
1 8WF(45),D(45),OP(45),OPP(45),OWF(45),EFFL(10,45),EFLM(45),
2 HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),POTE
3 TFWF(45),TWF(45),UDM(45),URM(45),XBEG(10,45),
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),
5 YFIBR(11,45),YLDS(45),XDM(45),PDF(7,45),DISM(45)
COMMON/SEEK/DEFOR(90),STPSIZ(90),GRAD(90),GRADI(90),DELTAG(90),
1 DIRECT(90),DIAG(90),STEP(4),DSTEP(4),FVAL(4),VALUES(7),
2 DISACC,SSIZE,FUNACC,FUNMIN,CRITL,CRITU,NLIN
INTEGER HEAD,DHEAD
DIMENSION SOLN(90)
C
C INITIALIZE.
C
POTE 0
POTE 10
POTE 20
POTE 30
POTE 40
POTE 50
POTE 60
POTE 70
POTE 80
POTE 90
POTE 100
POTE 110
POTE 120
POTE 130
POTE 140
POTE 150
POTE 160
POTE 170
POTE 180
POTE 190
POTE 200
POTE 210
POTE 220
POTE 230
POTE 240
POTE 250
POTE 260
POTE 270
POTE 280

```

11	DO 11 I=1,4	POTE 290
C	VALUES(I)=0.E0	POTE 300
C	FORM 20 DISPLACEMENT ARRAYS.	POTE 310
C		POTE 320
		POTE 330
	DO 20 I=1,NDF J	POTE 340
	J=IDFI(I)	POTE 350
	K=IDFII(I)	POTE 360
20	XDJ(K,J)=SOLN(I)	POTE 370
	L=NDF J+1	POTE 380
	DO 21 I=L,NDF	POTE 390
	M=IDFI(I)	POTE 400
21	XDM(M)=SOLN(I)	POTE 410
C		POTE 420
C	CALCULATE CONTRIBUTIONS OF THE MASSES TO THE POTENTIAL FUNCTION.	POTE 430
C		POTE 440
	IF (DT.EQ.0.E0.OR.NMAS.EQ.0) GO TO 40	POTE 450
	DO 30 I=1,NDF J	POTE 460
	J=IDFI(I)	POTE 470
	K=IDFII(I)	POTE 480
	IF (DAS(K,J).EQ.0.E0) GO TO 30	POTE 490
	VALUES(1)=VALUES(1)+DAS(K,J)*((3.E0*SOLN(I)-6.E0*DIS(K,J))/(DT*DT)	POTE 500
	1-6.E0*VEL(K,J)/DT-2.E0*ACC(K,J))*SOLN(I)	POTE 510
	CONTINUE	POTE 520
30		POTE 530
C	CALCULATE CONTRIBUTIONS OF THE FORCING FUNCTIONS TO THE POTENTIAL	POTE 540
C	FUNCTION.	POTE 550
C		POTE 560
C	IF (IFOR.EQ.0.AND.NFF.EQ.0) GO TO 60	POTE 570
40	DO 50 I=1,NDF J	POTE 580



C  
C  
C

3 = RECOVERABLE INTERNAL ENERGY.  
4 = DISSIPATIVE INTERNAL ENERGY.  
5 = KINETIC ENERGY.  
END

POTE 890  
POTE 900  
POTE 910  
POTE 920





```

C
C
15
20
C
C

INTEGER HEAD, DHEAD
IF (NFILE.GT.0) GO TO 100

MOVE INFO FROM COMMON BLOCK TO UNIT
IF (LERR.EQ.0.AND.IERR.EQ.0) GO TO 20
PRINT 15
FORMAT(1H,62H**NO FILE WRITTEN BECAUSE OF INPUT OR STORAGE ERROR
1S(REGO)***
GO TO 200
REWIND NSAVE
WRITE(NSAVE) DATA, KDATA, ICARD, IP, IPL, IQ, IQL, MATR, MATW, MBAR,
1 MCODE, MSHEAR, MSTAT, MTIES, MTYPE, NGRP, NSPAC, NTIES,
2 DENS, EC, EPSU, ST, FCFY, G, PR, S, SLOPE, ST, STN, STS, UNLK, ICODE, NAME,
3 OAS, OIS, ERJF, ERJH, ERJZ, F, FOR, VEL, X, XDJ, Y, IDFI, IDFII,
4 AVDM, AVG, CA, CB, CC, CD, CE, DHEAD, DT, EPS, HEAD, PI, RERF, RERH, RERZ, SERR,
5 IANAL, ICURV, IERR, IFAIL, IFOR, ILIN, IPAGE, IPLOT, IPRINT, IREC, ISTART,
6 ISTOP, ISTRES, ITAPE, IUNITS, IYLD, LERR, LINE, NACC, NCM, NCRD,
7 NOF, NOFD, NOFJ, NOIS, NDL, NFF, NJOR, NINC, NJ, NJD, NJER, NL, NLD, NLS, NLSR,
8 NM, NMAS, NMAT, NMATD, NMD, NPLOT, NPRT, NSAVE, NTAB, NTAPE, NTIMES, NVEL
WRITE(NSAVE) BETA, BMEM, BPP, BWF, D, OP, OPP, DMF, EFFL, EFLM, HMEM, HTOP,
AHTWF, POP, SPRING, STIES, TFWF, TMMF, UDM, URM, WFP, XBEG, XBEGM, XBEGS,
BXL, XPI, YBAR, YFIBR, YLDS, ZI, AGRP, ATIES,
DLCURV, LFF, LFFI, LMAXI, LMAX, LP, LPI, LPSI, LTAB, LTABI, NMAX, NMAXI,
EDEFOR, STPSIZ, GRAD, GRADI, DELTAG, DIRECT, DIAG, STEP, DSTEP, FVAL, DISACC,
ESSIZE, FUNACC, FUNMIN, CRITL, CRITU, NLIN,
FSRP, SRQ, UX, UY, UZ, XLEN, AREA, ZZI, IMAT
GO TO 200

MOVE INFO FROM UNIT TO COMMON BLOCKS

```

REGO 290  
REGO 300  
REGO 310  
REGO 320  
REGO 330  
REGO 340  
REGO 350  
REGO 360  
REGO 370  
REGO 380  
REGO 390  
REGO 400  
REGO 410  
REGO 420  
REGO 430  
REGO 440  
REGO 450  
REGO 460  
REGO 470  
REGO 480  
REGO 490  
REGO 500  
REGO 510  
REGO 520  
REGO 530  
REGO 540  
REGO 550  
REGO 560  
REGO 570  
REGO 580

C	100	REWIND NTAPE	REGO 590
		READ(NTAPE) DATA, KDATA, ICARD, IP, IPL, IQ, IQL, MATR, MATW, MBAR,	REGO 600
		1 MCODE, MSHEAR, MSTAT, MTIES, MTYPE, NGRP, NSPAC, NTIES,	REGO 610
		2 DENS, EC, EPSU, ST, FCFY, G, PR, S, SLOPE, ST, STN, STS, UNLK, ICODE, NAME,	REGO 620
		3 OAS, DIS, ERJF, ERJH, ERJZ, F, FOR, VEL, X, XDJ, Y, IOFI, IDFI,	REGO 630
		4 AVDM, AVGL, CA, CB, CC, CD, CE, DHEAD, DT, EPS, HEAD, PI, RERF, RERH, RERZ, SERR,	REGO 640
		4 TBEGIN, THALT, TIME, TINK, TINY, TPROB,	REGO 650
		5 IANAL, ICURV, IERR, IFAIL, IFOR, ILIN, IPAGE, IPLOT, IPRINT, IREC, ISTART,	REGO 660
		6 ISTOP, ISTRES, ITAPE, IUNITS, IYLD, LERR, LINE, NACC, NCM, NCRD,	REGO 670
		7 NDF, NDFD, NDFJ, NDIS, NDL, NFF, NJOR, NINC, NJ, NJO, NJER, NL, NLD, NLS, NLSR,	REGO 680
		8 NM, NMAS, NMAT, NMAID, NMD, NPLOT, NPRI, NSAVE, NTAB, NTAPE, NTIMES, NVEL	REGO 690
		READ(NTAPE) BETA, BMEM, BPP, BMF, D, OP, DPP, DMF, EFFL, EFLM, HMEM, HTOP,	REGO 700
		AHTWF, PDP, SPRING, STIES, TFMF, TWMF, UDM, URM, WFP, XBEG, XBEGM, XBEGS,	REGO 710
		8 XL, XPI, YBAR, YFIBR, YLDS, ZI, AGRP, ATIES,	REGO 720
		DLCURV, LFF, LFFI, LMAXI, LMAX, LP, LPI, LPSI, LTAB, LTABI, NMAX, NMAXI,	REGO 730
		EDEFOR, STPSIZ, GRAD, GRADI, DELTAG, DIRECT, DIAG, STEP, DSTEP, FVAL, DISACC,	REGO 740
		ESSIZE, FUNACC, FUNMIN, CRITL, CRITU, NLIN,	REGO 750
		FSRP, SRQ, UX, UY, UZ, XLEN, AREA, ZZI, IMAT	REGO 760
	200	RETURN	REGO 770
		END	REGO 780
			REGO 790



```

CREIN 0 10
SUBROUTINE REIN (MATL,RAINX,URS,UDS)
C
C DEFINITION OF STRESS HISTORY CURVE PARAMETERS
C TRANSMITTED VIA COMMON ARRAY S(9)
C
C S(1)= XFAIL= FIBER FAILURE CODE; 0= NOT RUPTURED,1= RUPTURED
C S(2)= RELOD = RELOADING INDICATOR; 0= VIRGIN CURVE,1= RELOADING CURVE
C S(3)= RMAX = MAXIMUM STRAIN
C S(4)= SMAX = MAXIMUM STRESS
C S(5)= ZRAINX = STRAIN ORIGIN
C S(6)= PLAS = PLASTIC OFFSET
C S(7)= SSEGM= LINE SEGMENT OF MATERIAL CURVE CONTAINING LAST STRAIN
C S(8)= SRESX= ABSOLUTE VALUE OF LAST STRESS
C S(9)= SRAINX=LAST STRAIN
C
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),
$ XFAIL,RELO,RMAX,SMAX,ZRAINX,PLAS,SSEGM,SRESX,SRAINX,
1 SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)
C
C DEFINE STRAIN ORIGIN ^ ELASTIC MODULUS
C
J= MATL
ZERON = STN(1,J)+ ZRAINX
YIT = SLOPE(1,J)
YIC = YIT
IF (SSEGM .LT. 1.E0) SSEGM = 1.E0
SEGM = SSEGM
PRMAX = RMAX
PSMAX = SMAX
REIN 0
REIN 10
REIN 20
REIN 30
REIN 40
REIN 50
REIN 60
REIN 70
REIN 80
REIN 90
REIN 100
REIN 110
REIN 120
REIN 130
REIN 140
REIN 150
REIN 160
REIN 170
REIN 180
REIN 190
REIN 200
REIN 210
REIN 220
REIN 230
REIN 240
REIN 250
REIN 260
REIN 270
REIN 280

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```

C
C IF LOAD HAS RECYCLED ADJUST STRESS-STRAIN CURVE
  IF (RELD .LT. 1.E0 ) GO TO 2
  SAVE = SLOPE(2,J)
  SLOPE(2,J) = SLOPE(8,J)
  SLOPE(1,J) = SLOPE(7,J)
  SAVN = STN(2,J)
  STN(2,J) = STN(8,J)
  SAVS = STS(2,J)
  STS(2,J) = STS(8,J)
  N = 7

C
C TEST FOR TENSION OR COMPRESSION
  2 IF (SMAX.LT. 0.E0 ) GO TO 200
  IF (RELD .LT. 1.E0 .AND. RAINX .LE. ZERON) GO TO 200
  GO TO 100

C
C TENSILE CURVE --COME FROM PREVIOUS COMP LOAD
C IF ELASTIC MEMBER DO NOT ALTER CURVE
C
  90 IF (RELD .LT. 1.E0 .AND. SMAX .GT. -STS(2,J)) GO TO 95

C
C DETERMINE NEW ZERO STRAIN AND NEW STRAIN ORIGIN.
  ZRAINX = ZRAINX + PLAS
  ZERON = STN(1,J) + ZRAINX

C
C ALTER STRESS-STRAIN CURVE IF INITIAL LOAD REVERSAL
  IF (RELD .EQ. 1.E0 ) GO TO 95
  SLOPE(1,J) = SLOPE(7,J)
  SAVE = SLOPE(2,J)

```

```

REIN 290
REIN 300
REIN 310
REIN 320
REIN 330
REIN 340
REIN 350
REIN 360
REIN 370
REIN 380
REIN 390
REIN 400
REIN 410
REIN 420
REIN 430
REIN 440
REIN 450
REIN 460
REIN 470
REIN 480
REIN 490
REIN 500
REIN 510
REIN 520
REIN 530
REIN 540
REIN 550
REIN 560
REIN 570
REIN 580

```

REIN 590  
 REIN 600  
 REIN 610  
 REIN 620  
 REIN 630  
 REIN 640  
 REIN 650  
 REIN 660  
 REIN 670  
 REIN 680  
 REIN 690  
 REIN 700  
 REIN 710  
 REIN 720  
 REIN 730  
 REIN 740  
 REIN 750  
 REIN 760  
 REIN 770  
 REIN 780  
 REIN 790  
 REIN 800  
 REIN 810  
 REIN 820  
 REIN 830  
 REIN 840  
 REIN 850  
 REIN 860  
 REIN 870  
 REIN 880

SLOPE(2,J)= SLOPE(8,J)  
 SAVN= STN(2,J)  
 STN(2,J)= STN(8,J)  
 SAVS= STS(2,J)  
 STS(2,J)= STS(8,J)  
 RELO = 1.E0

C  
 C INITIALIZE CURVE PARAMETERS

95 SMAX = 0.E0  
 RMAX = 0.E0  
 PLAS = 0.E0  
 SEGM = 1.E0  
 PSMAX = 0.E0  
 SRAINX= ZERON  
 PRMAX = ZERON  
 SRESX = 0.E0  
 SSEGM = 1.E0

C  
 C TENSILE LOADING

C 100 ISIGN = 1

C RESX = YIT \* (RAINX-ZERON -PLAS)

C  
 C IF COMP STRESS GO TO COMP CURVE  
 C IF (RESX .LT. 0.E0) GO TO 190

C  
 C TEST FOR UNLOADING OR RELOADING (KEEP STRESS A BRANCH TO ENERGY)  
 C IF (RESX .LT. SMAX) GO TO 300

```

C          C CALCULATE EFFECT STRAIN
C          STZ = RAINX - ZERON
C
C          C INCREMENT THRU STRESS-STRAIN CURVE TO LOCATE STRESS
C          IPT=SEGM*1.1E0
C          DO 50 I=IPT,N
C          IF(I.GT.8.OR.J.GT.9) PRINT 49,SEGM,I,J,N
C          FORMAT(1H,7HSEGMENT,E14.7,4H I= ,I2,4H J= ,I2,4H N= ,I2)
C          IF (STZ.GT. STN(I,J)) GO TO 50
C          II= I-1
C          RESX = STS(II,J) + SLOPE(II,J) *(STZ - STN(II,J))
C          SEGM = II
C          GO TO 60
C          50 CONTINUE
C
C          C STRAIN EXCEEDS RUPTURE STRAIN
C          SEGM = N-1
C          XFAIL = 1.E0
C          RESX= STS(7,J)
C          STZ= STN(N,J)
C          60 RMAX = RAINX
C          SMAX = RESX
C          PLAS = STZ - RESX/YIT
C          GO TO 300
C
C          C COMPRESSIVE CURVE --COME FROM PREVIOUS TENSILE LOADING
C
C          C IF ELASTIC MEMBER DO NOT ALTER CURVE
C
REIN 890
REIN 900
REIN 910
REIN 920
REIN 930
REIN 940
REIN 950
REIN 960
REIN 970
REIN 980
REIN 990
REIN1000
REIN1010
REIN1020
REIN1030
REIN1040
REIN1050
REIN1060
REIN1070
REIN1080
REIN1090
REIN1100
REIN1110
REIN1120
REIN1130
REIN1140
REIN1150
REIN1160
REIN1170
REIN1180

```

```

190 IF (RELD .LT. 1.E0 .AND. SMAX .LT. STS (2,J)) GO TO 195
C
C DETERMINE NEW ZERO STRAIN AND DEFINE NEW STRAIN ORIGIN.
ZRAINX = ZRAINX + PLAS
ZERON = STN(1,J) + ZRAINX
C
C ALTER STRESS-STRAIN CURVE IF INITIAL LOAD REVERSAL
IF (RELD .EQ. 1.E0 ) GO TO 195
SLOPE(1,J) = SLOPE(7,J)
SAVE = SLOPE(2,J)
SLOPE(2,J) = SLOPE(8,J)
SAVS = STS(2,J)
STS(2,J) = STS(8,J)
SAVN = STN(2,J)
STN(2,J) = STN(8,J)
RELD = 1.E0
C
C INITIALIZE CURVE PARAMETERS
195 SMAX = 0.E0
RMAX = 0.E0
SRAINX = ZERON
SRESX = 0.E0
PLAS = 0.E0
SEGM = 1.E0
PSMAX = 0.E0
PRMAX = ZERON
SSEGM = 1.E0
C
C COMPRESSIVE LOADING
C
REIN1190
REIN1200
REIN1210
REIN1220
REIN1230
REIN1240
REIN1250
REIN1260
REIN1270
REIN1280
REIN1290
REIN1300
REIN1310
REIN1320
REIN1330
REIN1340
REIN1350
REIN1360
REIN1370
REIN1380
REIN1390
REIN1400
REIN1410
REIN1420
REIN1430
REIN1440
REIN1450
REIN1460
REIN1470
REIN1480

```



```

200 ISIGN = -1
C
C CALCULATE TEST STRESS
  RESX= YIC *(RAINX-ZERON-PLAS)
C
C IF TENSILE STRESS GO TO TENSION CURVE
  IF (RESX.GT. 0.E0) GO TO 90
C
C TEST FOR UNLOADING OR RELOADING (KEEP STRESS ^ BRANCH TO ENERGY)
  IF (RESX .GT. SMAX) GO TO 300
C
C CALCULATE EFFECT STRAIN
  STZ = RAINX - ZERON
C
C INCREMENT THRU STRESS-STRAIN CURVE TO LOCATE STRESS
  IPT=SEGM+1.1E0
  DO 150 I=IPT,N
    IF (STZ .LT. -STN(I,J)) GO TO 150
    II= I-1
    RESX = -STS(II,J) + SLOPE(II,J)*( STZ + STN(II,J))
    SEGM =II
    GO TO 160
  150 CONTINUE
C
C STRAIN EXCEEDS RUPTURE STRAIN
  XFAIL = 1.E0
  SEGM = N-1
  RESX= -STS(7,J)
  STZ= STN(N,J)
  160 RMAX = RAINX

```

```

REIN1490
REIN1500
REIN1510
REIN1520
REIN1530
REIN1540
REIN1550
REIN1560
REIN1570
REIN1580
REIN1590
REIN1600
REIN1610
REIN1620
REIN1630
REIN1640
REIN1650
REIN1660
REIN1670
REIN1680
REIN1690
REIN1700
REIN1710
REIN1720
REIN1730
REIN1740
REIN1750
REIN1760
REIN1770
REIN1780

```

```

      SMAX = RESX
      PLAS = STZ - RESX/YIC
C
C  C PROCEED WITH ENERGY CALCULATIONS
C
      300 URS= 0.E0
      UDS= 0.E0
      IF(XFAIL.GT.0.E0) GO TO 400
C
C  C CALCULATE ABS VALUE OF STRESS
      ARESX = ABS(RESX)
C
C  C IF RELOADING TO MASTER CURVE LOCATE INTERSECTING PT
      PSMAX=ABS(PSMAX)
      IF (SRESX .LT. PSMAX ) SRESX = PSMAX
C
C  C CALCULATE RECOVERABLE ENERGY
      URS = 0.5E0 *RESX*RESX/YIT
C
C  C TEST TO SEE IF ON INITIAL ELASTIC CURVE- BRANCH TO ENERGY
      IF(RELD .LT. 1.E0 .AND. SEGM .EQ. 1.E0 ) GO TO 400
C
C  C TEST TO SEE IF ON UNLOAD OR RELOAD SECTION - BRANCH TO ENERGY
      IF (ISIGN .GT. 0 .AND. RESX .LT. SMAX ) GO TO 400
      IF (ISIGN .LT. 0 .AND. RESX .GT. SMAX ) GO TO 400
C
C  C CALCULATE DISSIPATED ENERGY (PREVIOUS RECOVERABLE)*2
      UDS = PSMAX*PSMAX/YIT
C
C  C CALCULATE INCREASE IN UDS DUE TO CHANGED LOADING

```

```

REIN1790
REIN1800
REIN1810
REIN1820
REIN1830
REIN1840
REIN1850
REIN1860
REIN1870
REIN1880
REIN1890
REIN1900
REIN1910
REIN1920
REIN1930
REIN1940
REIN1950
REIN1960
REIN1970
REIN1980
REIN1990
REIN2000
REIN2010
REIN2020
REIN2030
REIN2040
REIN2050
REIN2060
REIN2070
REIN2080

```

```

C IF RELOADING TO MASTER CURVE LOCATE INTERSECTING PT
C IF (( SRAINX.GT.0.E0 .AND. SRAINX.LT.PRMX ) .OR.
1 ( SRAINX.LT.0.E0 .AND. SRAINX.GT.PRMX )) SRAINX = PRMAX
C ARE THE LAST STRAIN ^ THE PRESENT STRAIN IN THE SAME LINE SEGMENT
C IF (SSEGM.LT.SEGM) GO TO 330
C
C CALCULATE UDS FOR POINTS IN THE SAME SEGMENT
R = ABS((ARESX + SRESX)*(RAINX-SRAINX))
IF (R .LT. 0.E0 ) R = -R
UDS = UDS + R
GO TO 360
C
C FIND ABS VALUE OF LAST STRAIN
330 R = ABS(SRAINX-ZERON)
C
C LOCATE END OF LINE SEGMENT FOR PREVIOUS LOADING
IPT = SSEGM + 1.1E0
C
C ACCUMULATE AREA UNDER CURVE
N = SEGM
DO 340 I = IPT, N
UDS = UDS + (SRESX + STS(I,J)) * (STN(I,J) - R)
SRESX = STS(I,J)
340 R = STN(I,J)
C
C USE ABS VALUE OF EFFECTIVE STRAIN
STZ = ABS(STZ)
UDS = UDS + (ARESX + STS(N,J)) * (STZ - STN(N,J))

```

```

REIN2090
REIN2100
REIN2110
REIN2120
REIN2130
REIN2140
REIN2150
REIN2160
REIN2170
REIN2180
REIN2190
REIN2200
REIN2210
REIN2220
REIN2230
REIN2240
REIN2250
REIN2260
REIN2270
REIN2280
REIN2290
REIN2300
REIN2310
REIN2320
REIN2330
REIN2340
REIN2350
REIN2360
REIN2370
REIN2380

```

```

360 UDS = 0.5E0 *UDS -URS
C
C CHECK ^ RESET CURVE TO INITIAL SHAPE
400 IF (RELD .LT. 1.E0) GO TO 450
    SLOPE(1,J) = YIT
    SLOPE(2,J) = SAVS
    STS(2,J) = SAVS
    STN(2,J) = SAVN
C
C STORE PARAMETERS FOR NEXT CYCLE
450 SRainX = RAINX
    SRESX = ARESX
    SSEGM = SEGM
    RETURN
C ***** GLOSSARY FOR REIN *****
C
C ARESX      = ABSOLUTE VALUE OF STRESS.
C IPT       = POINT ON A LINE SEGMENT.
C ISIGN      = 1, TENSION ; -1, COMPRESSION.
C N          = NO OF POINTS IN STRESS-STRAIN CURVE (FOR STEEL N=7).
C PRMAX      = PREVIOUS MAXIMUM STRAIN.
C PSMAX      = PREVIOUS MAXIMUM STRESS.
C R          = INTERMEDIATE STEP IN ENERGY AREA CALCULATION.
C RESX       = STRESS IN QUESTION.
C SAVE, SAVN, SAVS = TEMPORARY STORAGE FOR YIELD POINT CURVE DATA.
C SEGM       = LINE SEGMENT NO OF PREVIOUS STRAIN STATE.
C STZ        = EFFECTIVE STRAIN.
C VIC        = YOUNG+S MODULUS IN COMPRESSION.
C YIT        = YOUNG+S MODULUS IN TENSION.
C ZERON      = EFFECTIVE STRAIN ORIGIN.
REIN2390
REIN2400
REIN2410
REIN2420
REIN2430
REIN2440
REIN2450
REIN2460
REIN2470
REIN2480
REIN2490
REIN2500
REIN2510
REIN2520
REIN2530
REIN2540
REIN2550
REIN2560
REIN2570
REIN2580
REIN2590
REIN2600
REIN2610
REIN2620
REIN2630
REIN2640
REIN2650
REIN2660
REIN2670
REIN2680

```



REIN2690  
REIN2700

C  
END

```

CREJO 0 10
SUBROUTINE REJO
C
C THIS SUBROUTINE READS AND CHECKS JOINT COORDINATE AND JOINT RESTRAINTS
C
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),DIS(3,50),ERJF(3,50),
1 ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),
1 XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)
COMMON/LEADBK/AVOM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1 PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
INTEGER HEAD,DHEAD
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCH,
2 NCRO,NOF,NDFD,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRI,NSAVE,NTAB,NTAPE,
4 NTIMES,NVEL,IINITD
COMMON/SCALE/EGSIF,EGSIL
DIMENSION IRESTR(3,50),IERROR(5,50),IRES(3),JNUM(50)
DATA KZ,KB/1H0,1H /

C INITIALIZE VALUES TO BE USED IN SUBROUTINE
C
C
IC=0
IIUNIT=IUNITS
IIERR=IERR
NOFJ=0
JJ=0
JBIG=0
XEGSIL = 1.E0
DO 30 I=1,NJD

```

JNUM(I)=99999	REJO 290
X(I)=99999.	REJO 300
Y(I)=99999.	REJO 310
DO 10 J=1,3	REJO 320
IRESTR(J,I)=99999	REJO 330
DO 20 J=1,5	REJO 340
IERROR(J,I)=0	REJO 350
CONTINUE	REJO 360
READ BLOCK 2 HEADING (REQUIRED)	REJO 370
	REJO 380
	REJO 390
READ (NCRD,40) DHEAD	REJO 400
FORMAT (20A4)	REJO 410
READ BLOCK 2, CARD 2 (AT LEAST TWO REQUIRED) AND TEST DATA.	REJO 420
	REJO 430
	REJO 440
FORMAT (I5,5X,2E10.0,2X,3A1)	REJO 450
READ (NCRD,50) L,A,B,(IRES(K),K=1,3)	REJO 460
IRT=1	REJO 470
IF ((IRES(1).EQ.KZ).OR.(IRES(1).EQ.KB)) IRT=0	REJO 480
IRES(1)=IRT	REJO 490
IRT=1	REJO 500
IF ((IRES(2).EQ.KZ).OR.(IRES(2).EQ.KB)) IRT=0	REJO 510
IRES(2)=IRT	REJO 520
IRT=1	REJO 530
IF ((IRES(3).EQ.KZ).OR.(IRES(3).EQ.KB)) IRT=0	REJO 540
IRES(3)=IRT	REJO 550
PERFORM CHECKS ON DATA AND STORE.	REJO 560
	REJO 570
	REJO 580

C	CHECK FOR LAST CARD	REJO 590
C	IF (L.EQ.0) GO TO 130	REJO 600
C		REJO 610
C	CHECK FOR JOINT NUMBER LARGER THAN ALLOWED BY PROGRAM	REJO 620
C	IF (L.LE.NJD) GO TO 70	REJO 630
C		REJO 640
C		REJO 650
C	IF INPUT JOINT NUMBER TOO LARGE, SET JOINT NUMBER EQUAL TO MAXIMUM	REJO 660
C	ALLOWABLE AND SET ERROR FLAG	REJO 670
	L=NJD	REJO 680
	IERROR(1,L)=1	REJO 690
	IERR=IERR+1	REJO 700
	GO TO 120	REJO 710
C		REJO 720
C	CHECK FOR REPEATED JOINT NUMBERS WITH CONFLICTING DATA	REJO 730
C	IF (JNUM(L).EQ.99999) GO TO 80	REJO 740
70	IF (JNUM(L).EQ.L.AND.X(L).EQ.A.AND.Y(L).EQ.B.AND.IRESTR(1,L).EQ.IRREJO 750	
	1ES(1).AND.IRESTR(2,L).EQ.IRES(2).AND.IRESTR(3,L).EQ.IRES(3)) GO TO 60	REJO 760
	2 60	REJO 770
	IERROR(3,L)=1	REJO 780
	IERR=IERR+1	REJO 790
	GO TO 60	REJO 800
C		REJO 810
C	DETERMINE LARGEST JOINT NUMBER INPUT	REJO 820
80	IF (L.GT.JBIG) JBIG=L	REJO 830
C		REJO 840
C	INCREMENT JOINT COUNTER	REJO 850
	JJ=JJ+1	REJO 860
C		REJO 870
C	STORE JOINT NUMBER	REJO 880



C	JNUM(L)=L	REJO 890
C	STORE JOINT COORDINATES.	REJO 900
	X(L) = A	REJO 910
	Y(L) = B	REJO 920
C		REJO 930
C	CHECK FOR JOINTS WITH NO COORDINATES.	REJO 940
	IF ((A.EQ.0.E0).AND.(B.EQ.0.E0)) IC=IC+1	REJO 950
	IF (IC.LE.1) GO TO 100	REJO 960
	IC=IC-1	REJO 970
	IERROR(2,L)=1	REJO 980
	IERR=IERR+1	REJO 990
C		REJO1000
C	STORE JOINT RESTRAINTS	REJO1010
100	DO 110 I=1,3	REJO1020
110	IRESTR(I,L)=IRES(I)	REJO1030
120	CONTINUE	REJO1040
C		REJO1050
C	RETURN TO READ NEXT JOINT COORDINATE DATA CARD	REJO1060
	GO TO 60	REJO1070
C		REJO1080
C	MAKE TOTAL SET CHECKS AND STORE DATA.	REJO1090
C		REJO1100
C		REJO1110
C	NUMBER OF JOINTS EQUALS LARGEST JOINT NUMBER INPUT	REJO1120
130	NJ=JBIG	REJO1130
C		REJO1140
C	CHECK THAT AT LEAST TWO JOINTS HAVE BEEN INPUT	REJO1150
	IF (NJ.GE.2) GO TO 150	REJO1160
	IERR=IERR+1	REJO1170
		REJO1180

140	C	CALL PAGE	REJ01190
	C	PRINT 140	REJ01200
	150	FORMAT (1H,77H*** LESS THAN TWO JOINTS INPUT TO THE JOINT COORDINATE DATA BLOCK (REJO). ***)	REJ01210
		GO TO 490	REJ01220
	C		REJ01230
	C	CHECK THAT ALL JOINT NUMBERS UP TO LARGEST JOINT NUMBER INPUT HAVE	REJ01240
	150	DO 200 I=1,NJ	REJ01250
		IF (JNUM(I).NE.99999) GO TO 160	REJ01260
		IERROR(4,I)=1	REJ01270
		IERR=IERR+1	REJ01280
		GO TO 200	REJ01290
	C		REJ01300
	C	COUNT DEGREES OF FREEDOM AND CHECK THAT THIS NUMBER DOES NOT EXCEED	REJ01310
	160	MAXIMUM ALLOWABLE	REJ01320
		DO 190 K=1,3	REJ01330
		IF (IRESTR(K,I).NE.0) GO TO 180	REJ01340
		NDFJ=NDFJ+1	REJ01350
		IF (NDFJ.LE.NDFD) GO TO 170	REJ01360
		NDFJ=NDFD	REJ01370
		IERROR(5,I)=1	REJ01380
		IERR=IERR+1	REJ01390
	C		REJ01400
	170	STORE DEGREE OF FREEDOM NUMBER IN RESTRAINT CODE STORAGE LOCATION	REJ01410
	C	IRESTR(K,I)=NDFJ	REJ01420
	C		REJ01430
		STORE DEGREE OF FREEDOM LOCATION	REJ01440
		IDFI(NDFJ)=I	REJ01450
		IDFII(NDFJ)=K	REJ01460
		GO TO 190	REJ01470
			REJ01480

```

C
C
C
180
190
200
210
220
C
C
230
C
C
240
260
C
C

      OUTPUT BLOCK DATA IN PRINTED FORM.
      IF (IRESTR(K,I).EQ.1) IRESTR(K,I)=0
      CONTINUE
      CONTINUE
      NDF=NDFJ
      CONTINUE
      CALL PAGE
      FORMAT (1H ,20A4,/)
      WRITE (NPRT,220) DHEAD

      OUTPUT JOINT COORDINATE DATA BLOCK HEADING
      FORMAT (1H ,32X,32HJOINT COORDINATES AND RESTRAINTS//1H ,9HJOINT NREJ01620
10.,5X,12HX-COORDINATE,5X,12HY-COORDINATE,5X,14HX-DISPLACEMENT,5X,1REJ01630
24HY-DISPLACEMENT,6X,10HZ-ROTATION)
      WRITE (NPRT,230)
      LINE=LINE+3

      CHECK FOR OUTPUT UNITS (ENGLISH OR METRIC)
      IF(IIUNIT.LE.1) WRITE(NPRT,260)
      IF(IIUNIT.GE.2) WRITE(NPRT,240)
      FORMAT (18X,6HMETERS,11X,6HMETERS,/)
      FORMAT (18X,3HIN.,14X,3HIN.,/)
      LINE=LINE+2
      DO 460 J=1,NJ
      ITAG = 1

      CONVERT UNITS IF NECESSARY.
      XJ = X(J)*XEGSIL

```

```

REJ01490
REJ01500
REJ01510
REJ01520
REJ01530
REJ01540
REJ01550
REJ01560
REJ01570
REJ01580
REJ01590
REJ01600
REJ01610
REJ01620
REJ01630
REJ01640
REJ01650
REJ01660
REJ01670
REJ01680
REJ01690
REJ01700
REJ01710
REJ01720
REJ01730
REJ01740
REJ01750
REJ01760
REJ01770
REJ01780

```

```

C
C
C
C
300
310
320
330
C
C
340
350
C
C
360
370

YJ = Y(J)*XEGSIL

OUTPUT METRIC UNIT DATA
290 IF(IIUNIT.EQ.0.OR.IIUNIT.EQ.1) GO TO 340
WRITE(NPRT,350) JNUM(J),XJ,YJ,(IRESTR(K,J),K=1,3)

C
C
300 REPRINT PAGE AND TABLE HEADINGS, IF NEEDED.
LINE=LINE+1
IF (LINE.LE.NL) GO TO 330
CALL PAGE
WRITE (NPRT,230)
IF(IIUNIT.EQ.0.OR.IIUNIT.EQ.3) GO TO 310
WRITE (NPRT,240)
GO TO 320
WRITE (NPRT,260)
LINE=LINE+5
GO TO (360,380,400,420,440,460), ITAG

C
C
340 OUTPUT ENGLISH UNIT DATA
WRITE(NPRT,350) JNUM(J),XJ,YJ,(IRESTR(K,J),K=1,3)
350 FORMAT (1H,15,9X,0PE12.5,5X,0PE12.5,7X,15,14X,15,13X,15)
GO TO 300

C
C
360 OUTPUT ERROR MESSAGES
IF (IERROR(2,J).EQ.0) GO TO 380
370 FORMAT (1H,9H***JOINT,15,91H IS UNACCEPTABLE SINCE A JOINT IS ALREADY GIVEN AT THE ORIGIN OF THE COORDINATES (REJO).***)
PRINT 370, JNUM(J)
ITAG=2
GO TO 300

```

```

REJO1790
REJO1800
REJO1810
REJO1820
REJO1830
REJO1840
REJO1850
REJO1860
REJO1870
REJO1880
REJO1890
REJO1900
REJO1910
REJO1920
REJO1930
REJO1940
REJO1950
REJO1960
REJO1970
REJO1980
REJO1990
REJO2000
REJO2010
REJO2020
REJO2030
REJO2040
REJO2050
REJO2060
REJO2070
REJO2090

```



```

380 IF (IERROR(3,J).EQ.0) GO TO 400
390 FORMAT (1H ,46H*** TWO DIFFERENT SETS OF DATA INPUT FOR JOINT,15,1REJ02100
13H (REJO). ***)
PRINT 390, JNJM(J)
ITAG=3
GO TO 300
400 IF (IERROR(4,J).EQ.0) GO TO 420
PRINT 410, J
410 FORMAT (1H ,16H*** JOINT NUMBER,15,22H NOT INPUT (REJO). ***)
ITAG=4
GO TO 300
420 IF (IERROR(5,J).EQ.0) GO TO 440
430 FORMAT (1H ,37H*** NO. OF DEGREES OF FREEDOM EXCEEDS,15,65H,LARGESREJ02210
1Y NO. OF DEGREES OF FREEDOM ALLOWED BY PROGRAM (REJO). ***)
PRINT 430, NDFD
ITAG=5
GO TO 300
440 IF (IERROR(1,J).EQ.0) GO TO 460
450 FORMAT (1H ,36H*** JOINT NUMBER INPUT WHICH EXCEEDS,15,53H, LARGESREJ02270
1Y JOINT NUMBER ALLOWED BY PROGRAM (REJO). ***)
PRINT 450, NJD
ITAG=6
GO TO 300
460 CONTINUE
C
C IF INPUT UNITS MATCH OUTPUT UNITS, FINISHED
C IF (IIUNIT.EQ.0.OR.IIUNIT.EQ.2) GO TO 490
C
C IF INPUT ERRORS ENCOUNTERED, FINISHED
C IF (IERR.GT.IIERR) GO TO 490
REJ02090
REJ02100
REJ02110
REJ02120
REJ02130
REJ02140
REJ02150
REJ02160
REJ02170
REJ02180
REJ02190
REJ02200
REJ02210
REJ02220
REJ02230
REJ02240
REJ02250
REJ02260
REJ02270
REJ02280
REJ02290
REJ02300
REJ02310
REJ02320
REJ02330
REJ02340
REJ02350
REJ02360
REJ02370
REJ02380

```

C	OUTPUT JOINT DATA IN DIFFERENT DIMENSIONAL UNITS, IF NECESSARY.	REJ02390
C		REJ02400
C		REJ02410
C	IF INPUT AND OUTPUT UNITS SPECIFIED DO NOT MATCH, OUTPUT OTHER SET	REJ02420
	XEGSIL = EGSIL	REJ02430
	IF(IIUNIT.EQ.1) IIUNIT = 2	REJ02440
	IF(IIUNIT.EQ.3) IIUNIT = 0	REJ02450
	GO TO 210	REJ02460
	RETURN	REJ02470
	END	REJ02480

490

```

CSECT  0 10
SUBROUTINE SECT
C
C THIS SUBROUTINE LOCATES INTEGRATION SECTIONS, PREPARES FIBER DATA,
C AND SMEARS OUT LATERAL AND LONGITUDINAL REINFORCEMENT.
C
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1  MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2  MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/MAINBK/IANAL,ICURV,ISTRES,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,SECT
1  IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,SECT
2  NCRD,NDF,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,SECT
3  NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,SECT
4  NTIMES,NVEL,IINITD
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BDM(10,45),SECT
1  BWF(45),D(45),DP(45),OPP(45),OWF(45),EFFL(10,45),EFLM(45),SECT
2  HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),SECT
3  TFWF(45),TWWF(45),UDM(45),URM(45),XBEG(10,45),SECT
4  XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),SECT
5  YFIBR(11,45),YLOS(45),XDM(45),PDF(7,45),DISM(45)
SECT  0
SECT 10
SECT 20
SECT 30
SECT 40
SECT 50
SECT 60
SECT 70
SECT 80
SECT 90
SECT 100
SECT 110
SECT 120
SECT 130
SECT 140
SECT 150
SECT 160
SECT 170
SECT 180
SECT 190
SECT 200
SECT 210
SECT 220
SECT 230
SECT 240
SECT 250
SECT 260
SECT 270
SECT 280

C
GAUSS2 = 0.57735026918963E0
GAUSS3 = 0.77459666924148E0

C
C BEGIN DO LOOP OVER MEMBER NUMBER.
DO 100 M=1,NM

C
C DETERMINE X-DISTANCES FROM P-END OF MEMBER TO INTEGRATION SECTION.
XLH=0.5E0*XL(M)
XLA=GAUSS3*XLH

```

SECT 290  
SECT 300  
SECT 310  
SECT 320  
SECT 330  
SECT 340  
SECT 350  
SECT 360  
SECT 370  
SECT 380  
SECT 390  
SECT 400  
SECT 410  
SECT 420  
SECT 430  
SECT 440  
SECT 450  
SECT 460  
SECT 470  
SECT 480  
SECT 490  
SECT 500  
SECT 510  
SECT 520  
SECT 530  
SECT 540  
SECT 550  
SECT 560  
SECT 570  
SECT 580

```

XPI(1,M)=XLH-XLA
XPI(2,M)=XLH
XPI(3,M)=XLH+XLA

C CALCULATE Y-DISTANCES FROM REFERENCE AXIS FOR EACH FIBER.
IF (MTYPE(M).EQ.4) GO TO 80
IF (NTIES(M).NE.0) GO TO 20
COVR=HMEM(M)-D(M)
DPP(M)=HMEM(M)-2.E0*COVR
GO TO 30

20 COVR=(HMEM(M)-OPP(M))/2.E0
30 YFIBR(1,M)=HTOP(M)
YFIBR(11,M)=HTOP(M)-HMEM(M)
YFIBR(12,M)=HTOP(M)-COVR
DINC=DPP(M)/8.E0
DO 40 I=3,10
YFIBR(I,M)=YFIBR(I-1,M)-DINC
YFG=0.5E0*COVR*GAUSS2
YFH=HTOP(M)-0.5E0*COVR
YWG=(0.5E0*HMEM(M)-COVR)*GAUSS3
YWH=HTOP(M)-0.5E0*HMEM(M)
YFB=HTOP(M)-HMEM(M)+0.5E0*COVR

C SHEAR OUT LATERAL REINFORCEMENT FOR R/C MEMBER.
NT=NTIES(M)
IF (NT.EQ.0) GO TO 60
NSPACE=0
PDPS=0.E0
PPFS=0.E0
DO 50 J=1,NT

```



```

50      POPS=POPS+PDP(J,M)
        PPFS=PPFS+PDF(J,M)
        NSPACE=NSPACE+NSPAC(J,M)
        STIES(7,M)=XL(M)/FLOAT(NSPACE)
        PDP(7,M)=POPS/FLOAT(NT)
        PDF(7,M)=PPFS/FLOAT(NT)

C      C SMEAR OUT LONGITUDINAL REINFORCEMENT FOR R/C MEMBER.
60      NG=NGRP(M)
        IF (NG.EQ.0) GO TO 95
        DO 70 K=1,NG
70      AGRP(K,M)=AGRP(K,M)*EFFL(K,M)/XL(M)
        GO TO 95

C      C WIDE FLANGE MEMBER.
80      YFIBR(1,M)=HTWF(M)
        YFIBR(2,M)=HTWF(M)-TFWF(M)
        YFIBR(11,M)=HTWF(M)-DNWF(M)
        YFIBR(10,M)=YFIBR(11,M)+TFWF(M)
        DINC=(YFIBR(2,M)-YFIBR(10,M))/8.E0
        DO 90 J=3,9
90      YFIBR(J,M)=YFIBR(J-1,M)-DINC
        YFG=0.5E0*GAUSS2*TFWF(M)
        YFH=HTWF(M)-0.5E0*TFWF(M)
        YWG=(0.5E0*DNWF(M)-TFWF(M))*GAUSS3
        YWH=HTWF(M)-0.5E0*DNWF(M)
        YFB=HTWF(M)-DNWF(M)+0.5E0*TFWF(M)
        YGP(1,M)=YFH+YFG
        YGP(2,M)=YFH-YFG
        YGP(3,M)=YWH+YWG
95

```

```

SECT 590
SECT 600
SECT 610
SECT 620
SECT 630
SECT 640
SECT 650
SECT 660
SECT 670
SECT 680
SECT 690
SECT 700
SECT 710
SECT 720
SECT 730
SECT 740
SECT 750
SECT 760
SECT 770
SECT 780
SECT 790
SECT 800
SECT 810
SECT 820
SECT 830
SECT 840
SECT 850
SECT 860
SECT 870
SECT 880

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SECT 890  
SECT 900  
SECT 910  
SECT 920  
SECT 930  
SECT 940  
SECT 950  
SECT 960  
SECT 970  
SECT 980  
SECT 990  
SECT1000  
SECT1010  
SECT1020  
SECT1030  
SECT1040  
SECT1050  
SECT1060

YGP(4,M)=YMH  
YGP(5,M)=YMH-YMG  
YGP(6,M)=YFB+YFG  
YGP(7,M)=YFB-YFG

100 CONTINUE  
RETURN

C \*\*\*\*\* GLOSSARY FOR SECT \*\*\*\*\*

C COVR = CONCRETE COVER FOR TOP AND BOTTOM REINFORCEMENT.  
C DINC = DEPTH INCREMENT FOR LOCATING CONCRETE FIBERS.  
C NG = NUMBER OF LONGITUDINAL REINFORCEMENT GROUPS IN MEMBER.  
C NSPACE = TOTAL NUMBER OF STIRRUP SPACINGS IN MEMBER.  
C NT = NUMBER OF LATERAL REINFORCEMENT GROUPS IN MEMBER.  
C XPI = X-DISTANCE OF INTEGRATION SECTION FROM P-END OF MEMBER.  
C YFIBR = FIBER Y-DISTANCE FROM REFERENCE AXIS.

C  
END

```

CSEEK      0  i0
SUBROUTINE SEEK (DEFORM,ENG)
C
C      THIS SUBROUTINE OBTAINS THE DISPLACEMENT SOLUTION FOR THE CURRENT
C      TIME STEP. A FUNCTION MINIMIZATION PROCEDURE IS EMPLOYED.
C
COMMON DATA(10000), KDATA(500)
COMMON/ELEMENT/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1  MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2  MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1  PI,REFR,RRH,RRZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLT,IPRINT,SEEK 110
1  IREG,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,SEEK 120
2  NCRO,NDF,NDFJ,NOIS,NDL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,SEEK 130
3  NLS,NLSR,NH,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,SEEK 140
4  NTIMES,NVEL,IINITO
COMMON/SEEK8K/DEFOR(90),STPSIZ(90),GRAD(90),GRADI(90),DELTAG(90),SEEK 150
1  DIRECT(90),DIAG(90),STEP(4),DSTEP(4),FVAL(4),VALUES(7),SEEK 160
2  DISACC,SSIZE,FUNACC,FUNMIN,CRITL,CRITU,NLINSEEK 170
SEEK 180
SEEK 190
SEEK 200
SEEK 210
SEEK 220
SEEK 230
SEEK 240
SEEK 250
SEEK 260
SEEK 270
SEEK 280

INTEGER HEAD,DHEAD
DIMENSION DEFORM(90),CURV(4095)

EQUIVALENCE (DATA(1),CURV(1))

INITIALIZE

IF (IINITO.GE.0) GO TO 40
IINITO = 0

```

```

10 READ (NCRD,10) (DEFORM(I),I=1,NDF)
   FORMAT (8E10.0)
   WRITE (NPRT,20)
20 FORMAT (47H THE FOLLOWING INITIAL GUESS (SCALED) WAS USED--)
   WRITE (NPRT,30) (DEFORM(I),I=1,NDF)
30 FORMAT (1H ,(25X,1P5E17.9))
C
C SET CURVATURES EQUAL TO THE IDENTITY MATRIX IF THIS IS THE FIRST
C OF MINMIZ FOR THE CURRENT PROBLEM (ICURV=1). OTHERWISE, USE THE
C PREVIOUS CURVATURE MATRIX (ICURV=0).
C
40 IF (ICURV.EQ.0) GO TO 70
   ICURV = 0
   DISACC=ABS(DISACC)
   SSIZE=ABS(SSIZE)
   K=NDF*(NDF+1)/2
   DO 50 I=1,K
     CURV(I)=0.E0
50   DO 60 I=1,NDF
     K=NDF*(I-1)+I-I*(I-1)/2
     CURV(K)=1.E0
     DIAG(I)=1.E0
60   STPSIZ(I)=SSIZE
70   KLIN = 1
     KOUNT=0
     NCOUNT=0
     MINIM=1
     IDENT=1
     STEP(1)=1.E0
     EMAX=0.E0

```

```

SEEK 290
SEEK 300
SEEK 310
SEEK 320
SEEK 330
SEEK 340
SEEK 350
USEEK 360
SEEK 370
SEEK 380
SEEK 390
SEEK 400
SEEK 410
SEEK 420
SEEK 430
SEEK 440
SEEK 450
SEEK 460
SEEK 470
SEEK 480
SEEK 490
SEEK 500
SEEK 510
SEEK 520
SEEK 530
SEEK 540
SEEK 550
SEEK 560
SEEK 570
SEEK 580

```



```

C
C
C
      INITIAL FUNCTION VALUE
      CALL POTE (DEFORM,ENGY)
      KOUNT=KOUNT+1
      WRITE (NPRT,80)
      FORMAT (25HMINIMIZATION PERFORMANCE////)
      IF (IPRINT.LE.1) GO TO 120
      WRITE (NPRT,100)
      FORMAT (14H INITIAL POINT)
      WRITE (NPRT,110) ENGY,(DEFORM(I),I=1,NDF)
      FORMAT (16H FUNCTION VALUE,9X,9H VARIABLES/3X,0PE17.9,5X,5E17.9/(2SE17.9/
15X,5E17.9))
      INITIAL GRADIENT
      IF (IPRINT.GT.0) WRITE (NPRT,130) KLIN
      FORMAT (/20H0LINEAR MINIMIZATION,I4)
      ILOOP=1
      GRADM=0.E0
      IF (IPRINT.GT.2) WRITE (NPRT,150)
      FORMAT (10H GRADIENT,15X,35HSTEP SIZE USED IN COMPUTING GRADIENT)
      DO 170 I=1,NDF
      CALL DELT (DEFORM,STPSIZ(I),I,ENGG,0)
      NCOUNT=NCOUNT+1
      GRADM=GRADM+ENGG*ENGG
      IF (IPRINT.GT.2) WRITE (NPRT,160) ENGG,STPSIZ(I)
      FORMAT (3X,0PE17.9,5X,E17.9)
      GRAD(I)=ENGG
      IF (GRADM.NE.0.E0) GO TO 220
120
130
140
150
160
170
      SEEK 590
      SEEK 600
      SEEK 610
      SEEK 620
      SEEK 630
      SEEK 640
      SEEK 650
      SEEK 660
      SEEK 670
      SEEK 680
      SEEK 690
      SEEK 700
      SEEK 710
      SEEK 720
      SEEK 730
      SEEK 740
      SEEK 750
      SEEK 760
      SEEK 770
      SEEK 780
      SEEK 790
      SEEK 800
      SEEK 810
      SEEK 820
      SEEK 830
      SEEK 840
      SEEK 850
      SEEK 860
      SEEK 870
      SEEK 880

```

```

180      ILOOP=ILOOP+1
      IF (ILOOP.GT.5) GO TO 190
      DO 190 I=1,NDF
      STPSIZ(I)=STPSIZ(I)*8.E0
      GO TO 140
190      WRITE (NPRT,200)
200      FORMAT (32H0ZERO INITIAL GRADIENT IN MINMIZ)
      WRITE (NPRT,210)
210      FORMAT (73H ** ABNORMAL COMPLETION OF MINIMIZATION, ANALYSIS TERM
1INATED (SEEK). ***)
      IERR=1
      GO TO 940
220      IF (IPRINT.EQ.2) WRITE (NPRT,230) (GRAD(I), I=1,NDF)
230      FORMAT (12H GRADIENTS,,13X,1P5E17.9/(25X,5E17.9))
      IF (IPRINT.GT.1) WRITE (NPRT,240) (DIAG(I),I=1,NDF)
240      FORMAT (12H CURVATURES,13X,1P5E17.9/(25X,5E17.9))
      C
      C
      C
      SET UP FOR A MINIMIZATION ALONG A LINE
      DX=0.E0
      EPVAL=1.E0
      EQVAL=1.E0
      K=0
      DO 290 I=1,NDF
      DIRECT(I)=0.E0
      DO 260 J=1,NDF
      K=K+1
      DIRECT(I)=DIRECT(I)-CURV(K)*GRAD(J)
260      IF (I.EQ.1) GO TO 280
      J1=I-1

```

```

      SEEK 890
      SEEK 900
      SEEK 910
      SEEK 920
      SEEK 930
      SEEK 940
      SEEK 950
      SEEK 960
      SEEK 970
      SEEK 980
      SEEK 990
      SEEK1000
      SEEK1010
      SEEK1020
      SEEK1030
      SEEK1040
      SEEK1050
      SEEK1060
      SEEK1070
      SEEK1080
      SEEK1090
      SEEK1100
      SEEK1110
      SEEK1120
      SEEK1130
      SEEK1140
      SEEK1150
      SEEK1160
      SEEK1170
      SEEK1180

```

```

270 DO 270 J=1,J1
280 L=NDF*(J-1)+I-J*(J-1)/2
290 DIRECT(I)=DIRECT(I)-CURV(L)*GRAD(J)
300 IF (DIRECT(I).EQ.0.E0) GO TO 290
310 EPVAL = AMIN1(EPVAL,ABS(DISACC/DIRECT(I)))
320 EQUAL = AMIN1(EQUAL,(EPS/10.E0)*ABS(DEFORM(I)/DIRECT(I)))
330 DX=DX+GRAD(I)*DIRECT(I)
340 CONTINUE
350 EPVAL=.05E0*EPVAL
360 C
370 C IF DIRECTION IS NOT DOWNHILL, SET CURVATURES EQUAL TO IDENTITY.
380 C
390 IF (DX.LT.0.E0) GO TO 340
400 IREC=IREC+1
410 PRINT 300
420 FORMAT (93H * THE PREDICTED DIRECTION IS NOT DOWNHILL, CURVATURES
430 1 SET EQUAL TO IDENTITY MATRIX (SEEK).*)
440 DX = 0.E0
450 EPVAL=1.E0
460 EQUAL=1.E0
470 K=NDF*(NDF+1)/2
480 DO 310 I=1,K
490 CURV(I)=0.E0
500 DO 320 I=1,NDF
510 K=NDF*(I-1)+I-I*(I-1)/2
520 CURV(K)=1.E0
530 DIAG(I)=1.E0
540 DIRECT(I)=-GRAD(I)
550 IF (DIRECT(I).EQ.0.E0) GO TO 320
560 EPVAL = AMIN1(EPVAL,ABS(DISACC/DIRECT(I)))
570
580
590
600
610
620
630
640
650
660
670
680
690
700
710
720
730
740
750
760
770
780
790
800
810
820
830
840
850
860
870
880
890
900
910
920
930
940
950
960
970
980
990

```

```

SEEK1190
SEEK1200
SEEK1210
SEEK1220
SEEK1230
SEEK1240
SEEK1250
SEEK1260
SEEK1270
SEEK1280
SEEK1290
SEEK1300
SEEK1310
SEEK1320
SEEK1330
SEEK1340
SEEK1350
SEEK1360
SEEK1370
SEEK1380
SEEK1390
SEEK1400
SEEK1410
SEEK1420
SEEK1430
SEEK1440
SEEK1450
SEEK1460
SEEK1470
SEEK1480

```

```

320  EQUAL = AMIN1(EQUAL,(EPS/10.E0)*ABS(DEFORM(I)/DIRECT(I)))
      DX=DX+GRAD(I)*DIRECT(I)
      CONTINUE
      EPVAL=.05E0*EPVAL
      IF (IPRINT.GT.1) WRITE (NPRT,240) (DIAG(I),I=1,NDF)
      IF (IPRINT.GT.0) WRITE (NPRT,330) (DIRECT(I),I=1,NDF)
      FORMAT (12H DIRECTIONS,13X,1P5E17.9/(25X,5E17.9))
      C
      C
      C
      MAKE FIRST STEP ALONG LINE
      IF (ENGY.LE.FUNMIN) GO TO 350
      STEP(2)=2.E0*(FUNMIN-ENGY)/DX
      IF (STEP(2).LE.1.E0) GO TO 360
      STEP(2)=1.E0
      STEP(2)=AMAX1(STEP(2),EQUAL)
      FVAL(1)=ENGY
      STEP(1)=0.E0
      KKK=0
      IF (IPRINT.GT.1) WRITE (NPRT,370)
      FORMAT (16H FUNCTION VALUE,9X,27HFRACTION OF DIRECTION TAKEN)
      ILOOP=1
      DO 390 I=1,NDF
      DEFOR(I)=DEFORM(I)+STEP(2)*DIRECT(I)
      CALL POTE (DEFOR,FVAL(2))
      KOUNT=KOUNT+1
      IF (IPRINT.GT.1) WRITE (NPRT,160) FVAL(2),STEP(2)
      C
      C
      C
      TEST FOR CHANGE IN FUNCTION VALUE
      IF (FVAL(2).NE.FVAL(1)) GO TO 430

```



```

400 ILOOP=ILOOP+1
    IF (ILOOP.LE.5) GO TO 420
    WRITE (NPRT,400)
    FORMAT (40H NO CHANGE IN FUNCTION VALUE ALONG LINE.)
    WRITE (NPRT,410)
    FORMAT (35H NORMAL COMPLETION OF MINIMIZATION.)
    GO TO 920
410 STEP(2)=8.E0*STEP(2)
    GO TO 380
420
C
C
C
430 MAKE SECOND STEP ALONG LINE BY PARABOLIC INTERPOLATION.
    STEP2=0.5E0*DX*STEP(2)**2/(DX*STEP(2)+(FVAL(1)-FVAL(2)))
    IF (STEP2.LE.0.E0) STEP2=2.E0*STEP(2)
    IF (FVAL(2).LT.FVAL(1)) GO TO 450
    STEP(2)=STEP2
    KKK=KKK+1
    IF (KKK.LT.2) GO TO 380
    FVAL(3)=FVAL(2)
    FVAL(2)=ENGY
    STEP(3)=STEP(2)
    STEP(2)=0.E0
    STEP(1)=-STEP(3)
    DO 440 I=1,NDF
    DEFOR(I)=DEFORM(I)+STEP(1)*DIRECT(I)
    CALL POTE (DEFOR,FVAL(1))
    KOUNT=KOUNT+1
    IF (IPRINT.GT.1) WRITE (NPRT,160) FVAL(1),STEP(1)
    GO TO 480
440
450 MINIM=2

```

```

SEEK1790
SEEK1800
SEEK1810
SEEK1820
SEEK1830
SEEK1840
SEEK1850
SEEK1860
SEEK1870
SEEK1880
SEEK1890
SEEK1900
SEEK1910
SEEK1920
SEEK1930
SEEK1940
SEEK1950
SEEK1960
SEEK1970
SEEK1980
SEEK1990
SEEK2000
SEEK2010
SEEK2020
SEEK2030
SEEK2040
SEEK2050
SEEK2060
SEEK2070
SEEK2080

```

```

460 IF (STEP2.GT.4.E0*STEP(2)) STEP2=4.E0*STEP(2)
    IF (ABS(STEP(2)-STEP2).LT.EPVAL) STEP2=STEP(2)+1.1E0*EPVAL
    IF (ABS(STEP(2)-STEP2).LT..03E0*ABS(STEP(2))) STEP2=1.1E0*STEP(2)
    DO 460 I=1,NDF
        DEFOR(I)=DEFORM(I)+STEP2*DIRECT(I)
    IF (STEP2.GT.STEP(2)) GO TO 470
    STEP(3)=STEP(2)
    STEP(2)=STEP2
    FVAL(3)=FVAL(2)
    CALL POTE (DEFOR,FVAL(2))
    KOUNT=KOUNT+1
    IF (IPRINT.GT.1) WRITE (NPRT,160) FVAL(2),STEP(2)
    GO TO 480
470 STEP(3)=STEP2
    CALL POTE (DEFOR,FVAL(3))
    KOUNT=KOUNT+1
    IF (IPRINT.GT.1) WRITE (NPRT,160) FVAL(3),STEP(3)

C      DETERMINE LOCATION OF MINIMUM ALONG LINE
C
C      INIT=0
    CALL FITS (STEP,FVAL,DSTEP,AVAIL,INIT)
    MINIM=1
480 DO 500 I=2,3
    IF (FVAL(I).LT.FVAL(MINIM)) MINIM=I
    IE=2.E0+SIGN(1.E0,DSTEP(2))
    IF (AVAIL.EQ.0.E0) IE=2.E0+SIGN(1.E0,FVAL(1)-FVAL(2))
    IF (AVAIL.LT.0.E0) IE=4-IE
    IF (AVAIL.LE.0.E0.OR.ABS(DSTEP(2)).GT.ABS(4.E0*DSTEP(IE))) DSTEP(
12)=4.E0*DSTEP(IE)
500

```

```

SEEK2090
SEEK2100
SEEK2110
SEEK2120
SEEK2130
SEEK2140
SEEK2150
SEEK2160
SEEK2170
SEEK2180
SEEK2190
SEEK2200
SEEK2210
SEEK2220
SEEK2230
SEEK2240
SEEK2250
SEEK2260
SEEK2270
SEEK2280
SEEK2290
SEEK2300
SEEK2310
SEEK2320
SEEK2330
SEEK2340
SEEK2350
SEEK2360
SEEK2370
SEEK2380

```

```

STEP3=STEP(2)+DSTEP(2)
IF (ABS(STEP3-STEP(MINIM)).LT.EPVAL) GO TO 580
IF (ABS(STEP3-STEP(MINIM)).LT..03E0*ABS(STEP(MINIM))) GO TO 580
IF (DSTEP(IE).LT.DSTEP(2)) IE=IE+1
IF (IE.EQ.4) GO TO 520
DO 510 LL=IE,3
L=3-LL+IE
STEP(L+1)=STEP(L)
FVAL(L+1)=FVAL(L)
STEP(IE)=STEP3
DO 530 I=1,NDF
DEFOR(I)=DEFORM(I)+STEP3*DIRECT(I)
CALL POTE (DEFOR,FVAL(IE))
KOUNT=KOUNT+1
IF (IPRINT.GT.1) WRITE (NPRT,160) FVAL(IE),STEP(IE)
IF (IE.EQ.1) GO TO 480
KKK=1
IF (IE.EQ.4) GO TO 560
IF (FVAL(1).GT.FVAL(4)) GO TO 540
INIT=0
CALL FITS (STEP,FVAL,DSTEP,AVAL,INIT)
IF (STEP(2)+DSTEP(2).LT.STEP(4).AND.AVAL.GT.0.E0) GO TO 490
GO TO 550
KKK=2
INIT=1
CALL FITS (STEP,FVAL,DSTEP,AVAL,INIT)
IF (STEP(3)+DSTEP(2).GT.STEP(1).AND.AVAL.GT.0.E0) GO TO 560
KKK=1
IF (FVAL(2).LT.FVAL(1).AND.FVAL(2).LE.FVAL(3).OR.FVAL(2).LE.FVAL(1)
1).AND.FVAL(2).LT.FVAL(3)) GO TO 480

```

510  
520  
530  
540  
550

SEE #2390  
SEEK2400  
SEEK2410  
SEEK2420  
SEEK2430  
SEEK2440  
SEEK2450  
SEEK2460  
SEEK2470  
SEEK2480  
SEEK2490  
SEEK2500  
SEEK2510  
SEEK2520  
SEEK2530  
SEEK2540  
SEEK2550  
SEEK2560  
SEEK2570  
SEEK2580  
SEEK2590  
SEEK2600  
SEEK2610  
SEEK2620  
SEEK2630  
SEEK2640  
SEEK2650  
SEEK2660  
SEEK2670  
SEEK2680

560	DO 570 I=1,3	SEEK2690
	STEP(I)=STEP(I+1)	SEEK2700
570	FVAL(I)=FVAL(I+1)	SEEK2710
	IF (KKK.EQ.2) GO TO 490	SEEK2720
	GO TO 480	SEEK2730
C		SEEK2740
C	END OF MINIMIZATION ALONG LINE	SEEK2750
C		SEEK2760
580	IF (IPRINT.EQ.1) GO TO 590	SEEK2770
	IF (IPRINT.LE.0) GO TO 620	SEEK2780
	WRITE (NPRT,600) FVAL(MINIM),STEP(MINIM)	SEEK2790
600	FORMAT (3H *,0PE17.9,5X,E17.9)	SEEK2800
590	WRITE (NPRT,610) KOUNT,NCOUNT	SEEK2810
610	FORMAT (28H FUNCTION SUBROUTINE CALLS=,I5/20H GRADIENT SUBROUTINE	SEEK2820
	1E CALLS=,I5)	SEEK2830
C		SEEK2840
C	IF THERE WAS NO MOTION, RETURN	SEEK2850
C		SEEK2860
620	IF (STEP(MINIM).NE.0.E0) GO TO 640	SEEK2870
	WRITE (NPRT,630)	SEEK2880
630	FORMAT (36H NO MOTION IN THE LINEAR MINIMIZATION.)	SEEK2890
	WRITE (NPRT,410)	SEEK2900
	GO TO 920	SEEK2910
C		SEEK2920
C	IF THE FUNCTION VALUE HAS NOT CHANGED, RETURN	SEEK2930
C		SEEK2940
640	IF (FVAL(MINIM).NE.ENGY) GO TO 660	SEEK2950
	WRITE (NPRT,650)	SEEK2960
650	FORMAT (57H LINEAR MINIMIZATION FAILED TO CHANGE THE FUNCTION VALUE	SEEK2970
	1E.)	SEEK2980



```

C
C
C
660
    WRITE (NPRT,410)
    GO TO 920
    TEST FOR CONVERGENCE AND UPDATE SOLUTION
    ENGY=FVAL(MINIM)
    ETEST=AMAX1(1.E0,ABS(STEP(MINIM)))
    EMAX=0.E0
    DO 670 I=1,NDF
    EMAX=AMAX1(EMAX,ABS(ETEST*DIRECT(I)))
    DIRECT(I)=STEP(MINIM)*DIRECT(I)
    DEFORM(I)=DEFORM(I)+DIRECT(I)
    GRADI(I)=GRAD(I)
    IF (IPRINT.LE.0) GO TO 700
    WRITE (NPRT,690) EMAX
    FORMAT (28H MINIMIZATION ACCURACY =,E20.10)
    WRITE (NPRT,110) ENGY,(DEFORM(I),I=1,NDF)
    IF (EMAX.GT.DISACC) GO TO 720
    WRITE (NPRT,710)
    FORMAT (51H CONVERGENCE OF MINIMIZATION TO SPECIFIED ACCURACY.)
    WRITE (NPRT,410)
    GO TO 920
    NOTE IF MINIMUM WAS FOUND ALONG NEGATIVE DIRECTION
    IF (STEP(MINIM).GE.0.E0) GO TO 740
    IF (IPRINT.LE.0) GO TO 740
    PRINT 730
    IREC=IREC+1
    FORMAT (54H** MINIMUM LOCATED ALONG NEGATIVE DIRECTION (SEEK). **)SEEK3280
730

```

```

SEEK2990
SEEK3000
SEEK3010
SEEK3020
SEEK3030
SEEK3040
SEEK3050
SEEK3060
SEEK3070
SEEK3080
SEEK3090
SEEK3100
SEEK3110
SEEK3120
SEEK3130
SEEK3140
SEEK3150
SEEK3160
SEEK3170
SEEK3180
SEEK3190
SEEK3200
SEEK3210
SEEK3220
SEEK3230
SEEK3240
SEEK3250
SEEK3260
SEEK3270
SEEK3280

```

SEEEK3290  
SEEEK3300  
SEEEK3310  
SEEEK3320  
SEEEK3330  
SEEEK3340  
SEEEK3350  
SEEEK3360  
SEEEK3370  
SEEEK3380  
SEEEK3390  
SEEEK3400  
SEEEK3410  
SEEEK3420  
SEEEK3430  
SEEEK3440  
SEEEK3450  
SEEEK3460  
SEEEK3470  
SEEEK3480  
SEEEK3490  
SEEEK3500  
SEEEK3510  
SEEEK3520  
SEEEK3530  
SEEEK3540  
SEEEK3550  
SEEEK3560  
SEEEK3570  
SEEEK3580

```

780      GO TO 790
        STPSIZ(I)=2.E0*SQRT(ETAM*ABS(ENGY)/DIAG(I))
        STPSIZ(I)=STPSIZ(I)*(1.E0-DIAG(I)*STPSIZ(I)/(3.E0*DIAG(I)*STPS
790      1IZ(I)+4.E0*ABS(GRAD(I))))
        STPSIZ(I)=SIGN(STPSIZ(I),GRAD(I))
        IF (.5E0*ABS(DIAG(I)*STPSIZ(I)/GRAD(I)).LT..01E0) GO TO 800
        STPSIZ(I)=100.E0*ABS(ENGY*ETAM/GRAD(I))
        STPSIZ(I)=ABS(GRAD(I))+SQRT(GRAD(I)**2+200.E0*ABS(ENGY)*DIAG(
1I)*ETAM)
        STPSIZ(I)=100.E0*ABS(ENGY)*ETAM/STPSIZ(I)
800      CALL DELT (DEFORM,STPSIZ(I),I,ENGG,0)
        NCOUNT=NCOUNT+1
        IF (IPRINT.GT.2) WRITE (NPRT,160) ENGG,STPSIZ(I)
810      GRAD(I)=ENGG
        IDENT=0
        IF (IPRINT.EQ.2) WRITE (NPRT,230) (GRAD(I),I=1,NDF)
C
C
C      UPDATE CURVATURES
        AVAL=0.E0
        DO 820 I=1,NDF
          DELTAG(I)=GRAD(I)-GRAD(I)
          AVAL=AVAL+DELTAG(I)*DIRECT(I)
          IF (AVAL.EQ.0.E0) AVAL=TINY
          AA=AVAL/STEP(MINIM)
          C1=1.E0/AVAL-DX/AA**2
          C2=2.E0/AA
          B=0.E0
          K=0
        DO 850 I=1,NDF

```

```

SEEK3590
SEEK3600
SEEK3610
SEEK3620
SEEK3630
SEEK3640
SEEK3650
SEEK3660
SEEK3670
SEEK3680
SEEK3690
SEEK3700
SEEK3710
SEEK3720
SEEK3730
SEEK3740
SEEK3750
SEEK3760
SEEK3770
SEEK3780
SEEK3790
SEEK3800
SEEK3810
SEEK3820
SEEK3830
SEEK3840
SEEK3850
SEEK3860
SEEK3870
SEEK3880

```

```

DIAG(I)=DIAG(I)+C1*DELTA(I)**2+C2*DELTA(I)*GRADI(I)
DEFOR(I)=0.E0
DO 830 J=I,NDF
  K=K+1
  DEFOR(I)=DEFOR(I)+CURV(K)*DELTA(J)
  IF (I.EQ.1) GO TO 850
  J1=I-1
  DO 840 J=1,J1
    L=NDF*(J-1)+I-J*(J-1)/2
    DEFOR(I)=DEFOR(I)+CURV(L)*DELTA(J)
  840 DEFOR(I)=DEFOR(I)*DELTA(I)
  850 IF (IPRINT.GT.1) WRITE (NPRT,240) (DIAG(I),I=1,NDF)
  K=0
  DO 860 I=1,NDF
    DO 860 J=I,NDF
      K=K+1
      CURV(K)=CURV(K)+DIRECT(I)*DIRECT(J)/AVAL+DEFOR(I)*DEFOR(J)/B
  CHECK THAT DIAGONAL ELEMENTS ARE POSITIVE

  DO 910 I=1,NDF
    K=NDF*(I-1)+I-I*(I-1)/2
    IF (CURV(K).GT.0.E0) GO TO 910
    WRITE (NPRT,870) I
    FORMAT (51H * NEGATIVE DIAGONAL IN CURVATURE-INVERSE MATRIX,,I4,SEEK4130
  143H ROW ZEROED, DIAGONAL SET TO UNITY. (SEEK)*
    CURV(K)=1.E0
    DIAG(I)=1.E0
    IF (NDF.EQ.1) GO TO 910
    IF (I.EQ.NDF) GO TO 890

```

830

840

850

860

C

C

C

870

SEEK3890

SEEK3900

SEEK3910

SEEK3920

SEEK3930

SEEK3940

SEEK3950

SEEK3960

SEEK3970

SEEK3980

SEEK3990

SEEK4000

SEEK4010

SEEK4020

SEEK4030

SEEK4040

SEEK4050

SEEK4060

SEEK4070

SEEK4080

SEEK4090

SEEK4100

SEEK4110

SEEK4120

SEEK4130

SEEK4140

SEEK4150

SEEK4160

SEEK4170

SEEK4180



```

J1=I+1
DO 880 J=J1,NDF
K=K+1
CURV(K)=0.E0
880 IF (I.EQ.1) GO TO 910
J1=I-1
DO 900 J=1,J1
L=NDF*(J-1)+I-J*(J-1)/2
CURV(L)=0.E0
900 CONTINUE
C
C GO BACK FOR ANOTHER ITERATION
C
C GO TO 250
C
C RETURN TO CALLING PROGRAM
C
C IF (IPRINT.GT.0) GO TO 940
WRITE (NPRT,110) ENGY,(DEFORM(I),I=1,NDF)
WRITE (NPRT,610) KOUNT,NCOUNT
WRITE(NPRT,930) KLIN
930 FORMAT (23H LINEAR MINIMIZATIONS=,I10)
WRITE (NPRT,690) EMAX
940 RETURN
C
C ***** GLOSSARY FOR SEEK *****
C
C AVAL = ESTIMATE OF SIGN OF CURVATURE; IF POSITIVE, PARABOLA OPENS
C        UPWARD, IF NEGATIVE PARABOLA OPENS DOWNWARD.
C CURV  = INVERSE MATRIX OF SECOND ORDER PARTIAL DERIVATIVES
SEEK4190
SEEK4200
SEEK4210
SEEK4220
SEEK4230
SEEK4240
SEEK4250
SEEK4260
SEEK4270
SEEK4280
SEEK4290
SEEK4300
SEEK4310
SEEK4320
SEEK4330
SEEK4340
SEEK4350
SEEK4360
SEEK4370
SEEK4380
SEEK4390
SEEK4400
SEEK4410
SEEK4420
SEEK4430
SEEK4440
SEEK4450
SEEK4460
SEEK4470
SEEK4480

```

C DEFOR = (CURVATURES) OF THE FUNCTION.  
 C DEFORM = NEW ESTIMATE OF DEFORMATION VECTOR.  
 C DELTAG = DEFORMATION VECTOR.  
 C DELTAG = VECTOR OF CHANGES IN THE GRADIENT.  
 C DIAG = SECOND DERIVATIVES OF THE FUNCTION ALONG COORDINATE  
 DIRECTIONS (MAIN DIAGONAL OF CURVATURE MATRIX).  
 C DIRECT = DIRECTION VECTOR.  
 C DISACC = ACCURACY REQUIRED OF THE DISPLACEMENT COMPONENTS.  
 C DSTEP = DIFFERENCE OF TWO SUCCESSIVE STEPSIZES.  
 C DX = DIRECTIONAL DERIVATIVE OF THE FUNCTION ALONG THE LINE;  
 SCALAR PRODUCT OF THE GRADIENT VECTOR AND THE DIR. VECTOR.  
 C EMAX = MAXIMUM CHANGE IN VALUE OF ALL DISPLACEMENTS.  
 C ENGG = ENERGY GRADIENT FOR ONE DEGREE-OF-FREEDOM.  
 C ENGY = VALUE OF THE POTENTIAL FUNCTION.  
 C EPVAL = ACCURACY MEASURE OF EVAL BASED ON DISACC.  
 C EQVAL = ACCURACY MEASURE OF EVAL BASED ON MAGNITUDE OF DEFORM.  
 C ETAM = MEASURE OF ENERGY IMBALANCE.  
 C ETEST = MEASURE OF MAXIMUM STEPSIZE.  
 C FUNACC = ESTIMATE OF RELATIVE ERROR IN FUNCTION EVALUATIONS.  
 C FUNMIN = A LOWER BOUND ON THE FUNCTION.  
 C FVAL = FUNCTION VALUE.  
 C GFAD = CURRENT GRADIENT VECTOR.  
 C GRADI = PREVIOUS GRADIENT VECTOR.  
 C GRADM = SQUARE OF THE MAGNITUDE OF THE GRADIENT VECTOR.  
 C IDENT = FLAG TO IDENTIFY WHETHER OR NOT STEPSIZE SHOULD BE UPDATED.  
 C IF = SUBSCRIPT IDENTIFYING THE VALUE OF EVAL CLOSEST TO THE MIN.  
 C IINITO = INDEX FOR INITIAL GUESS OF DISPLACEMENTS.  
 C ILOOP = NUMBER OF TIMES A ZERO INITIAL GRADIENT IS FOUND.  
 C INIT = INDEX IDENTIFYING LINEAR SEARCH STEP.  
 C KKK = COUNT OF NUMBER OF STEPS TAKEN ALONG LINE.

SEEK4490  
 SEEK4500  
 SEEK4510  
 SEEK4520  
 SEEK4530  
 SEEK4540  
 SEEK4550  
 SEEK4560  
 SEEK4570  
 SEEK4580  
 SEEK4590  
 SEEK4600  
 SEEK4610  
 SEEK4620  
 SEEK4630  
 SEEK4640  
 SEEK4650  
 SEEK4660  
 SEEK4670  
 SEEK4680  
 SEEK4690  
 SEEK4700  
 SEEK4710  
 SEEK4720  
 SEEK4730  
 SEEK4740  
 SEEK4750  
 SEEK4760  
 SEEK4770  
 SEEK4780



```

CSTEN 0 10
SUBROUTINE STEN(M,UR,UD,IFLAG)
C
C THIS SUBROUTINE CALCULATES THE CONTRIBUTION OF THE STEEL
C REINFORCEMENT TO THE TOTAL MEMBER ENERGY.
C
COMMON DATA(10000),KDATA(500)
COMMON/ELEMENT/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),
1 SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)
COMMON/LEADBK/AVJM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),OT,EPS,HEAD(20),
1 PI,REF,REH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLT,IPRINT,
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLO,LERR,LINE,NACC,NCM,
2 NCRO,NDF,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,NDFJ,
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,
4 NTIMES,NVEL,IINITD
COMMON/MEMBER/AGRP(10,45),ATTES(6,45),BPP(45),BPP(10,45),
1 BWF(45),D(45),DPP(45),DWF(45),EFFL(10,45),EFLM(45),
2 HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),
3 TFWF(45),TWWF(45),UDM(45),URM(45),X3EG(10,45),
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),
5 YFIBR(11,45),YLODS(45),XDM(45),PDF(7,45),DISM(45)
COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB,
1 LABI,NMAX,NMAXI
COMMON/STRNBK/SRP(4),SRQ(4),UX,UY,UZ,XLEN,AREA,ZZI,IMAT
INTEGER HEAD,DHEAD

```

STEN 0  
STEN 10  
STEN 20  
STEN 30  
STEN 40  
STEN 50  
STEN 60  
STEN 70  
STEN 80  
STEN 90  
STEN 100  
STEN 110  
STEN 120  
STEN 130  
STEN 140  
STEN 150  
STEN 160  
STEN 170  
STEN 180  
STEN 190  
STEN 200  
STEN 210  
STEN 220  
STEN 230  
STEN 240  
STEN 250  
STEN 260  
STEN 270  
STEN 280



```

C
C DIMENSION STRAIN(5),URI(5),UDI(5),GAUSS(3)
C INITIALIZE
  NG = NGRP(M)
  ISTAT=MSTAT(M)
  GAUSS(1)=5.E0/9.E0
  GAUSS(2)=8.E0/9.E0
  GAUSS(3)=GAUSS(1)
C RETRIEVE BEGINNING (ZERO) INDEXES FOR STRAIN AND STRESS HISTORIES.
  KRAIN=KDATA(LPI+M)-1
  KRESS=KDATA(LPSI+M)-1
C
C BEGIN DO LOOP OVER GROUP NUMBER.
C
  DO 70 I=1,NG
    MATL=MBAR(I,M)
    AG=AGRP(I,M)
    YLOC=YBAR(I,M)
    KS=KRESS+24*(I-1)
    KR=KRAIN+3*(I-1)
    CON = AG*XLEN/2.E0
C
C DETERMINE ENERGY DENSITY AT INTEGRATION SECTIONS.
  DO 60 J=1,3
    XLOC=XPI(J,M)
C RETRIEVE STRAIN AND STRESS HISTORY.
    IF(ISTAT.EQ.3) GO TO 18
    DO 16 L=1,9
      S(L)=0.E0
16    GO TO 25
  
```

```

18      LS=KS+8*(J-1)
        S(1)=DATA(LS+1)
        IF(S(1).EQ.1.E0) GO TO 30
        DO 20 L=2,8
20      S(L)=DATA(LS+L)
        S(9)=DATA(KR+J)
        C FIND STRAIN AT INTEGRATION SECTION.
25      CALL STRN(M,XLOC,YLOC,STRAIN(J))
        C OBTAIN STEEL ENERGY DENSITY.
        CALL REIN(MATL,STRAIN(J),URI(J),UDI(J))
        GO TO 40
        C IF FIBER HAS FAILED, SET ENERGY DENSITY TO ZERO.
30      URI(J)=0.E0
        UDI(J)=0.E0
        GO TO 65
        C UPDATE STRAIN AND STRESS HISTORY IF IFLAG=3.
40      IF(IFLAG.NE.3.OR.ISTAT.NE.3) GO TO 65
        DO 50 L=1,8
50      DATA(LS+L)=S(L)
        DATA(KR+J)=S(9)
        C ACCUMULATE ENERGY FOR THIS GROUP.
65      UR = UR + CON*GAUSS(J)*URI(J)
        UD = UD + CON*GAUSS(J)*UDI(J)
        CONTINUE
70      CONTINUE
        IF (IFLAG.NE.3.OR.ISTAT.NE.3) GO TO 110
        KR=KRAIN+3*NG
        KS=KRESS+24*NG
        XLOC=0.E0
        DO 100 I=1,2

```

```

STEN 590
STEN 600
STEN 610
STEN 620
STEN 630
STEN 640
STEN 650
STEN 660
STEN 670
STEN 680
STEN 690
STEN 700
STEN 710
STEN 720
STEN 730
STEN 740
STEN 750
STEN 760
STEN 770
STEN 780
STEN 790
STEN 800
STEN 810
STEN 820
STEN 830
STEN 840
STEN 850
STEN 860
STEN 870
STEN 880

```

```

IF(I.EQ.2) XL0C=XLEN
J=I
DO 90 K=1,NG
CALL STIRN(M,XLOC,YBAR(K,M),TRAIN)
IF(ABS(TRAIN).LT.TINY) TRAIN=TINY
S(9)=DATA(KR+J)
LS=KS+8*(J-1)
DO 75 L=1,8
S(L)=DATA(LS+L)
CALL REIN(MATL,TRAIN,URE,UDE)
DATA(KR+J)=S(9)
DO 80 L=1,8
DATA(LS+L)=S(L)
J=J+2
CONTINUE
CONTINUE
RETURN
C
C ***** GLOSSARY FOR STEN *****
C
C AG = AREA OF LONGITUDINAL STEEL GROUP.
C CON = TEMPORARY CONSTANT.
C I = LONGITUDINAL STEEL GROUP NUMBER.
C J = INTEGRATION SECTION NUMBER.
C KR = STRAIN INDEX FOR EACH STEEL GROUP.
C KRAIN = ZERO INDEX FOR STRAIN HISTORY STORAGE.
C KRES = ZERO INDEX FOR STRESS HISTORY STORAGE.
C KS = STRESS INDEX FOR EACH STEEL GROUP.
C LS = STRESS INDEX FOR EACH INTEGRATION SECTION.
C M = MEMBER NUMBER.

```

```

STEN 890
STEN 900
STEN 910
STEN 920
STEN 930
STEN 940
STEN 950
STEN 960
STEN 970
STEN 980
STEN 990
STEN1000
STEN1010
STEN1020
STEN1030
STEN1040
STEN1050
STEN1060
STEN1070
STEN1080
STEN1090
STEN1100
STEN1110
STEN1120
STEN1130
STEN1140
STEN1150
STEN1160
STEN1170
STEN1190

```

C MATL = MATERIAL NUMBER OF LONGITUDINAL STEEL GROUP.  
 C NG = NUMBER OF LONGITUDINAL STEEL GROUPS IN MEMBER.  
 C UD = DISSIPATIVE ENERGY DENSITY FOR MEMBER.  
 C UR = RECOVERABLE ENERGY DENSITY FOR MEMBER.  
 C XLEN = LENGTH OF MEMBER.  
 C YLOC = DISTANCE FROM REFERENCE AXIS TO STEEL GROUP.  
 C

END

STEN1190  
 STEN1200  
 STEN1210  
 STEN1220  
 STEN1230  
 STEN1240  
 STEN1250  
 STEN1260



```

CSTOR 0 10
SUBROUTINE STOR (M)
C
C THIS SUBROUTINE ESTABLISHES STORAGE SPACE FOR STRESS-STRAIN
C HISTORY OF AN INELASTIC MEMBER.
C
COMMON DATA(10000), KOATA(500)
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,STOR 90
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,STOR 100
2 NCRD,NDF,NDFD,NDFJ,NDIS,NOL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,STOR 110
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,STOR 120
4 NTIMES,NVEL,IINITD
COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB,STOR 130
1 LTABI,NMAX,NMAXI
C COUNT NO. OF ELEMENTS WITH MSTAT = 3.
IYLD = IYLD + 1
C CALCULATE STRAIN AND STRESS HISTORY STORAGE REQUIREMENTS.
L=LMAX+1
LSTN=5*NGRP(M)+58
IF (MTYPE(M).EQ.4) LSTN=43
LSTS=8*LSTN
LMAX=LMAX+LSTN+LSTS
C
C COMPARE WITH AVAILABLE STORAGE.
IF (LMAX.LE.NMAX) GO TO 20
PRINT 10
FORMAT (//1H ,62H*** PROBLEM STORAGE REQUIREMENTS EXCEED DATA ARRASTOR 280
10

```



```

CSTRN      0  10
C          SUBROUTINE STRN (M,X,Y,STRAIN)
C
C          SUBROUTINE TO CALCULATE LONGITUDINAL STRAIN AT ANY POINT
C          C WITHIN THE MACRO ELEMENT BASED ON LOCAL DISPLACEMENTS.
C
C          COMMON /MEMBER/ DUMMY1(5365),XDM(45),DUMMY2(360)
C          COMMON/STRNBK/SRP(4),SRQ(4),UX,UY,UZ,XLEN,AREA,ZZI,IMAT
C
C          XI = X/XLEN
C          ETA = Y/XLEN
C
C          DERIVATIVES OF DISPLACEMENT FUNCTIONS.
C          P1P = 4.E0*XI - 1.E0
C          P4P = 4.E0 - 8.E0*XI
C          P2P = 6.E0*(XI-XI**2)
C          P3P = 3.E0*XI**2 - 2.E0*XI
C          P2PP = 6.E0 - 12.E0*XI
C          P3PP = 6.E0*XI - 2.E0
C
C          NORMAL STRAIN AT ANY POINT X,Y (XI,ETA).
C          STRAIN = P1P*UX + P4P*XDM(M) + .5E0*(P2P*UY+P3P*UZ)**2
C          - ETA*(P2PP*UY+P3PP*UZ)
C          1
C          RETURN
C
C          ***** GLOSSARY FOR STRN *****
C
C          ETA = NONDIMENSIONAL Y LOCATION.
C          M = MEMBER OR ELEMENT NUMBER.
C          P1P = PHI-ONE-PRIME, DERIVATIVE OF PHI1 W.R.T. X - THE 1

```

C	CORRESPONDS TO THE X-DIRECTION, 2 TO Y, 3 TO Z OR ROTATION,	STRN 290
C	AND 4 CORRESPONDS TO THE INTERNAL NODE.	STRN 300
C	STRAIN = NORMAL STRAIN AT X,Y WITHIN THE ELEMENT.	STRN 310
C	UX = LOCAL DISPLACEMENT IN THE X OR 1 DIRECTION.	STRN 320
C	X = X COORDINATE WITHIN THE ELEMENT.	STRN 330
C	XOM = LONGITUDINAL DISPLACEMENT OF THE INTERNAL NODE.	STRN 340
C	XI = NONDIMENSIONAL X LOCATION.	STRN 350
C	XLEN = LENGTH OF THE ELEMENT.	STRN 360
C	Y = Y COORDINATE WITHIN THE ELEMENT.	STRN 370
C		STRN 380
C		STRN 390

END



```

CSUMY      0 10
SUBROUTINE SUMY
C THIS SUBROUTINE PRINTS A SUMMARY OF PROBLEM CHARACTERISTICS, AS IN
C BY SINGER
C
COMMON/ELEMET/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),SUMY
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),SUMY
1 SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)SUMY
COMMON/JOINTS/ACC(3,50),BET(3,50),DAS(3,50),JIS(3,50),ERJF(3,50),SUMY
1 ERJH(3,50),ERJZ(3,50),F(3,50),FOR(3,50),VEL(3,50),X(50),SUMY
1 XDJ(3,50),Y(50),DER(3,50),RESENG(3,50),IDFI(90),IDFII(90)SUMY
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),SUMY
1 PI,REF,REH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
INTEGER HEAD,DHEAD
COMMON/MAINBK/IANAL,ICURV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,SUMY
1 IREG,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,SUMY
2 NGRO,NDF,NDFJ,NDIS,NDL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,SUMY
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,SUMY
4 NTIMES,NVEL,IINITD
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BOM(10,45),SUMY
1 BWF(45),J(45),DP(45),OPP(45),DWF(45),EFFL(10,45),EFLM(45),SUMY
2 HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),SUMY
3 TFWF(45),TWWF(45),UDM(45),URM(45),XBEG(10,45),SUMY
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),SUMY
5 YFIBR(11,45),YLDS(45),XDM(45),PDF(7,45),DISM(45)
PRINT THE PAGE NUMBER
CALL PAGE

```

10	FORMAT (1H,30X,34H CHARACTERISTICS OF THE SIMULATION,///)	SUMY 290
	WRITE (NPRT,10)	SUMY 300
C	PRINT THE TABLE HEADING	SUMY 310
C		SUMY 320
20	FORMAT (1H0,10HITEM CLASS,8X,16HITEM DESCRIPTION)	SUMY 330
	WRITE (NPRT,20)	SUMY 340
30	FORMAT(1H,11(1H-),7X,70(1H-))///	SUMY 350
	WRITE (NPRT,30)	SUMY 360
C		SUMY 370
C	PRINT THE PARAMETERS OF THE STRUCTURE.	SUMY 380
C		SUMY 390
40	FORMAT (11H PARAMETERS,9X,15,7H JOINTS,/,20X,15,9H ELEMENTS,/,7H OSUMY 400	
	1F THE,13X,15,10H MATERIALS,/,20X,15,13H POINT MASSES,/,10H STRUCTUSUMY 410	
	2RE,///)	SUMY 420
	LINE=LINE+9	SUMY 430
	NEL=NM+NLS	SUMY 440
	WRITE (NPRT,40) NJ,NEL,NMAT,NMAS	SUMY 450
C		SUMY 460
C	PRINT KINEMATIC CONDITIONS.	SUMY 470
C		SUMY 480
50	FORMAT (10H KINEMATIC,10X,15,27H DEGREES OF FREEDOM (TOTAL)/20X,	SUMY 490
	115,27H ELEMENT DEGREES OF FREEDOM/20X,15,33H LEAF SPRING RIGIDITY SUMY 500	
	2CONSTRAINTS/11H CONDITIONS,9X,15,34H DISPLACEMENTS PRESCRIBED AS ZSUMY 510	
	3ERO ,///)	SUMY 520
	LINE=LINE+8	SUMY 530
	IF (LINE.GE.NL) CALL PAGE	SUMY 540
	NRC=NJ*3-NDFJ	SUMY 550
	WRITE (NPRT,50) NDF,NM,NLSR,NRC	SUMY 560
C		SUMY 570
C	PRINT FORCE CONDITIONS.	SUMY 580

```

C 60
    FORMAT (6H FORCE,14X,15,25H JOINT LOADING CONDITIONS,/,20X,15,21H
1DISTRIBUTED LOADINGS,/,11H CONDITIONS,9X,15,16H FUNCTION TABLES,/,
2/)
    LINE=LINE+6
    IF (LINE.GE.NL) CALL PAGE
    WRITE (NPRT,60) NFF,NOL,NTAB
C
C 70
    PRINT INITIAL CONDITION DATA
C
    FORMAT (8H INITIAL,12X,15,32H JOINTS WITH DISPLACEMENTS GIVEN/,20XSUMY 590
1,15,30H JOINTS WITH VELOCITIES GIVEN,/,11H CONDITION,9X,15,33H JSUMY 600
2JOINTS WITH ACCELERATIONS GIVEN,/,20X,15,24H JOINTS WITH JERKS GIVSUMY 610
3EN,/,6H DATA,14X,15,31H JOINTS WITH POINT FORCES GIVEN//)
    WRITE (NPRT,70) NDIS,NVEL,NACC,NJER,NJOR
    LINE=LINE+8
    IF (LINE.GE.NL) CALL PAGE
C
C 80
    PRINT SIMULATION ASSUMPTIONS
C
    FORMAT (12H ASSUMPTIONS,8X,23H TIME-HISTORY STARTS AT,0PE12.4,9H SSUMY 790
1SECONDS.,/,1H,20X,12HIT STOPS AT,0PE12.4,9H SECONDS.,/,1H,19X,44SUMY 800
2H MAXIMUM TOLERABLE RELATIVE ENERGY ERROR IS,0PE12.4,1H.,/,7H OF SUMY 810
3THE,13X,48H THE MAXIMUM COMPUTER RUN TIME FOR THIS CASE IS,0PE12. SUMY 820
44,9H MINUTES.)
    LINE=LINE+12
    IF (LINE.GE.NL) CALL PAGE
    WRITE (NPRT,80) TBEGIN,THALT,SERR,TPROB
    IF (IUNITS-1) 100,120,130
    FORMAT (1H,19X,53H INPUT IS IN ENGLISH UNITS, OUTPUT IS IN ENGLISHSUMY 880
90

```

100	1H 100.)	SUMY 890
	WRITE (NPRT,90)	SUMY 900
	GO TO 180	SUMY 910
110	FORMAT (1H,19X,70H INPUT IS IN ENGLISH UNITS, OUTPUT IS IN STANDASUMY 920	
	1R0 INTERNATIONAL UNITS.)	SUMY 930
120	WRITE (NPRT,110)	SUMY 940
	GO TO 180	SUMY 950
130	IF (IUNITS-2) 120,150,170	SUMY 960
140	FORMAT (1H,19X,70H INPUT IS IN STANDARD INTERNATIONAL UNITS, OUTPSUMY 970	
	1UT IS IN STANDARD 100.)	SUMY 980
150	WRITE (NPRT,140)	SUMY 990
	GO TO 180	SUMY1000
160	FORMAT (1H,19X,70H INPUT IS IN STANDARD INTERNATIONAL UNITS, OUTPSUMY1010	
	1UT IS IN ENGLISH UNITS.)	SUMY1020
170	WRITE (NPRT,160)	SUMY1030
180	IF(ILIN.EQ.1) GO TO 220	SUMY1040
190	FORMAT (1H,20X,73HJOINT ROTATIONS AND ELEMENT DISTORTIONS ARE ASSSUMY1050	
	1UMED TO BE INFINITESIMALS.)	SUMY1060
	WRITE (NPRT,190)	SUMY1070
	GO TO 280	SUMY1080
210	FORMAT (1H,20X,70HJOINT ROTATIONS ARE ASSUMED FINITE, ELEMENT DISSUMY1090	
	1TORTIONS INFINITESIMAL.)	SUMY1100
220	WRITE (NPRT,210)	SUMY1110
	GO TO 280	SUMY1120
280	IF (ISTOP) 320,320,300	SUMY1130
290	FORMAT (11H SIMULATION,10X,63HCALCULATIONS ARE STOPPED ON POTENTIALSUMY1140	
	1LLY FATAL AND FATAL ERRORS.)	SUMY1150
300	WRITE (NPRT,290)	SUMY1160
	GO TO 340	SUMY1170
310	FORMAT (11H SIMULATION,9X,46HCALCULATIONS ARE STOPPED ONLY ON FATASUMY1180	



```

320 1L ERRORS.)
330 WRITE (NPRT,310)
      FORMAT (1H,20X,37HSHEAR MACRO FAILURE IS DEFINED BY CA=,0PE12.4,5SUMY1210
1H, C8=,0PE12.4,1H,/,1H,22X,3HCC=,0PE12.4,5H C0=,0PE12.4,
29H, AND CE=,0PE12.4,1H,///)
340 WRITE (NPRT,330) CA,C8,CC,C0,CE
      C
      C
      C
350 PRINT SIMULATION OPTIONS.
      IF (ISTART.GT.0) GO TO 370
      FORMAT (8H OPTIONS,13X,31HINPUT DATA IS IN PUNCHED CARDS.)
      LINE=LINE+9
      IF (LINE.GE.NL) CALL PAGE
      WRITE (NPRT,350)
      GO TO 380
360 FORMAT (8H OPTIONS,13X,21HINPUT DATA IS ON UNIT,15)
370 IST=11
      WRITE (NPRT,360) IST
380 IF (IPRINT) 400,400,430
390 FORMAT (1H,20X,48HTHE *MINIMUM* OF SIMULATION RESULTS IS PRINTED.
1)
400 WRITE (NPRT,390)
      GO TO 480
410 FORMAT (1H,20X,45HTHE *STANDARD* AMOUNT OF RESULTS IS PRINTED.)
420 WRITE (NPRT,410)
      GO TO 480
430 IF (IPRINT-2) 420,450,470
440 FORMAT (1H,20X,44H*DETAILS* OF SIMULATION RESULTS ARE PRINTED.)
450 WRITE (NPRT,440)
      GO TO 480
SUMY1190
SUMY1200
SUMY1210
SUMY1220
SUMY1230
SUMY1240
SUMY1250
SUMY1260
SUMY1270
SUMY1280
SUMY1290
SUMY1300
SUMY1310
SUMY1320
SUMY1330
SUMY1340
SUMY1350
SUMY1360
SUMY1370
SUMY1380
SUMY1390
SUMY1400
SUMY1410
SUMY1420
SUMY1430
SUMY1440
SUMY1450
SUMY1460
SUMY1470
SUMY1480

```

```

460  FORMAT (1H ,20X,50HALL PRINT STATEMENTS CITING RESULTS ARE EXECUTESUMY1490
      10. )
      SUMY1500
470  WRITE (NPRT,460)
      SUMY1510
480  IF (ISTRES) 500,520,530
      SUMY1520
490  FORMAT (8H FOR THE,13X,39HPRINTOUTS EXCLUDE STRESSES AND STRAINS.)SUMY1530
500  WRITE (NPRT,490)
      SUMY1540
      GO TO 590
      SUMY1550
510  FORMAT (8H FOR THE,13X,39HPRINTOUTS INCLUDE STRESSES AND STRAINS.)SUMY1560
520  WRITE (NPRT,510)
      SUMY1570
      GO TO 590
      SUMY1580
530  IF (ISTRES-2) 520,550,570
      SUMY1590
540  FORMAT (8H FOR THE,13X,36HPRINTOUTS INCLUDE STRESS RESULTANTS.)
      SUMY1600
550  WRITE (NPRT,540)
      SUMY1610
      GO TO 590
      SUMY1620
560  FORMAT (8H FOR THE,13X,59HPRINTOUTS INCLUDE STRESSES, STRAINS, ANDSUMY1630
      1 STRESS RESULTANTS.)
      SUMY1640
570  WRITE (NPRT,560)
      SUMY1650
580  FORMAT (1H ,20X,21HPRINTOUTS OCCUR EVERY,0PE12.4,35H SECONDS, OR LSUMY1660
      1ESS, OF THE HISTORY. )
      SUMY1670
590  WRITE (NPRT,580) TINK
      SUMY1680
      IF (ITAPE.EQ.0) GO TO 620
      SUMY1690
600  FORMAT (15H INPUT ^ OUTPUT,6X,37HCONTINUATION DATA IS WRITTEN ON USUMY1700
      1NIT ,I2)
      SUMY1710
      IST=11
      SUMY1720
      WRITE (NPRT,600) IST
      SUMY1730
      GO TO 630
      SUMY1740
610  FORMAT (15H INPUT ^ OUTPUT,6X,38HNO CONTINUATION DATA FILE IS WRITSUMY1750
      1TEN. )
      SUMY1760
620  WRITE (NPRT,610)
      SUMY1770
630  IF (IPLOT.EQ.0) GO TO 650
      SUMY1780

```

```

640      FORMAT (1H,20X,44HA DATA RETRIEVAL FILE IS WRITTEN ON FILE 10.) SUMY1790
      WRITE (NPRT,640) SUMY1800
650      CONTINUE SUMY1810
      C SUMY1820
      C SUMY1830
      C SUMY1840
      C SUMY1850
      C SUMY1860
      C SUMY1870
      C SUMY1880
      C SUMY1890
      C SUMY1900
      C SUMY1910
      C SUMY1920
      C SUMY1930
      C SUMY1940
      C SUMY1950
      C SUMY1960

      NOTE AVAILABLE STORAGE

      LINE=LINE+9
      IF (LINE.GE.NL) CALL PAGE
      NA=NJD-NJ
      NB=NMD-NM
      NC=NMATD-NMAT
      ND=NDFD-NDF
      FORMAT (1H0,8X,40H STORAGE STILL AVAILABLE FOR MODELING /11X,I5,I5,SUMY1910
      17H JOINTS /11X,I5,9H ELEMENTS /11X,I5,10H MATERIALS /11X,I5,9H FRESUMY1920
      2EDOMS ////) SUMY1930
      WRITE (NPRT,660) NA,NB,NC,ND SUMY1940
      RETURN SUMY1950
      END SUMY1960

```





C	IF (TX.GT.DATA(LFTP)) GO TO 10	TABL 290
C	VALUE=DATA(LFTP+1)	TABL 300
C	GO TO 70	TABL 310
C	IF TIME FOR EVALUATION IS GREATER THAN LAST TIME POINT, FUNCTION	TABL 320
C	FORCE AT LAST TIME POINT	ETABL 330
C		TABL 340
10	IF (TX.LT.DATA(LLTP)) GO TO 20	TABL 350
C	VALUE=DATA(LLTP+1)	TABL 360
	GO TO 70	TABL 370
		TABL 380
C	EVALUATE FUNCTION FOR EVALUATION TIME BETWEEN FIRST AND LAST TIME	TABL 390
C		TABL 400
C		TABL 410
20	LJTP = LFTP + 2*(J-1)	TABL 420
C	IF (TX.LE.DATA(LJTP)) GO TO 40	TABL 430
30	J=J+1	TABL 440
	LJTP=LJTP+2	TABL 450
	IF (TX.LE.DATA(LJTP)) GO TO 50	TABL 460
	GO TO 30	TABL 470
40	IF (TX.GE.DATA(LJTP-2)) GO TO 50	TABL 480
	J=J-1	TABL 490
	LJTP=LJTP-2	TABL 500
	GO TO 40	TABL 510
50	TJ=DATA(LJTP)	TABL 520
	FJ=DATA(LJTP+1)	TABL 530
	TI=DATA(LJTP-2)	TABL 540
	FI=DATA(LJTP-1)	TABL 550
	DELT=IJ-TI	TABL 560
	IF (DELT.EQ.0.E0) GO TO 60	TABL 570
	VALUE=FI+(FJ-FI)*(TX-TI)/DELT	TABL 580

GO TO 70  
VALUE=FI  
RETURN  
END

60  
70

TABL 590  
TABL 600  
TABL 610  
TABL 620

```

CTEST 0 10
SUBROUTINE TEST (IYFLAG)
C THIS SUBROUTINE TESTS FOR NEWLY YIELDED MEMBERS OF MSTAT(M)=2
C STATUS. IF SUCH MEMBERS ARE FOUND, THEIR STATUS IS CHANGED FROM
C ELASTIC TO PLASTIC FOR ALL FURTHER CALCULATIONS AND, UPON
C RETURN TO THE CALLING PROGRAM, THE CURRENT SOLUTION IS REPEATED
C WITH THESE MEMBERS PERMITTED TO YIELD.
C
COMMON/ELEMENT/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1 MATW(45),MBAR(10,45),MCODE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2 MTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),
1 SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)
COMMON/MAINBK/IANAL,ICURV,IERR,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,TEST 120
1 IREG,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,TEST 130
2 NCRD,NDF,NDFD,NDFJ,NDIS,NOL,NFF,NJOR,NINC,NJ,NJD,NJER,NL,NLD,TEST 140
3 NLS,NLSR,NM,NMAS,NMAT,NMATD,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,TEST 150
4 NTIMES,NVEL,IINITO
COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),BOM(10,45),TEST 170
1 BME(45),D(45),DP(45),DPP(45),DWE(45),EDEL(10,45),EELM(45),TEST 180
2 HMEM(45),HTOP(45),HWF(45),POP(7,45),SPRING(5,20),STIES(7,45),TEST 190
3 TFWF(45),TWWF(45),UDM(45),URM(45),XBEG(10,45),TEST 200
4 XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),TEST 210
5 YFIBR(11,45),YLOS(45),XDM(45),PDF(7,45),DISM(45)
COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB,
1 LTABI,NMAX,NMAXI
COMMON/STRNBK/SRP(4),SRQ(4),UX,UY,UZ,XLEN,AREA,ZZI,IMAT
C
C BEGIN DO LOOP OVER MEMBER NUMBER.
DO 70 M=1,NM

```





```

35 IF (ABS(EPST).GT.EXSTN) GO TO 50
C CONTINUE
C CHECK FIBER STRAINS AT ENDS OF LONGITUDINAL STEEL GROUPS.
C
C IF (L.EQ.4) GO TO 70
C NG=NGRP(M)
C DO 40 I=1,NG
C MAT=MBAR(I,M)
C STSTN=ABS(STN(2,MAT))
C BEG=XBEG(I,M)
C END=XBEG+EFFL(I,M)
C YB=YBAR(I,M)
C CALL STRN (M,9EG,YB,EPSE)
C IF (ABS(EPSE).GT.STSTN) GO TO 50
C CALL STRN (M,END,YB,EPSE)
C IF (ABS(EPSE).GT.STSTN) GO TO 50
C CONTINUE
C GO TO 70
C
C PRINT NEWLY YIELDED MEMBER NUMBER, CHANGE MEMBER STATUS CODE,
C AND ESTABLISH DATA STORAGE FOR STRAIN AND STRESS HISTORY.
C
C IF (IYFLAG.EQ.0) CALL PAGE
C IYFLAG = 1
C MSTAT(M)=3
C WRITE (NPRT,60) NAME(MAT),M
C FORMAT(10X,20HSTRAIN OF MATERIAL ,A4,37H EXCEEDS YIELD STRAIN,
C MEMBER NUMBER,I5,21H HAS YIELDED (TEST).)
C CALL STOR (M)

```

TEST 590  
TEST 600  
TEST 610  
TEST 620  
TEST 630  
TEST 640  
TEST 650  
TEST 660  
TEST 670  
TEST 680  
TEST 690  
TEST 700  
TEST 710  
TEST 720  
TEST 730  
TEST 740  
TEST 750  
TEST 760  
TEST 770  
TEST 780  
TEST 790  
TEST 800  
TEST 810  
TEST 820  
TEST 830  
TEST 840  
TEST 850  
TEST 860  
TEST 870  
TEST 880

```

C
C
70
C
C
C
C
      END OF DO LOOP OVER MEMBER NUMBER.
      CONTINUE
      MESSAGE PRINTOUT AND RETURN TO CALLING PROGRAM.
      IF (IYFLAG.NE.0) GO TO 90
      WRITE (NPRT,80)
      FORMAT (//1H,42HTHERE ARE NO NEWLY YIELDED MEMBERS (TEST).)
      GO TO 170
90
      IF (LERR.EQ.0.AND.IERR.EQ.0) GO TO 110
      PRINT 100
      FORMAT (1H,80H** THE ANALYSIS IS TERMINATED. CURRENT RESULTS FOTEST1010
100
1R THIS TIME STEP ARE PRINTED./5X,84HTHESE RESULTS ARE BASED ON LINTEST1020
2EAR ELASTIC RESPONSE FOR THE ABOVE MEMBERS (TEST). ***)
      GO TO 170
C
      PRINT STORAGE LOCATION INDEXES.
      WRITE (NPRT,120)
110
120
      FORMAT (//10X,46HSTORAGE LOCATION INDEXES IN DATA ARRAY (TEST)./)
      WRITE (NPRT,130) LCURV,LTAB,LFF,LP,LMAX,NMAX
130
      FORMAT (14X,17HMINIMIZATION DATA,I19/14X,15HFUNCTION TABLES,I21/14X,12HETEST1110
1X,17HFORCING FUNCTIONS,I19/14X,19HPLASTIC STRAIN DATA,I17/14X,12HETEST1110
2ND OF ARRAY,I24/14X,16HSPACES ALLOCATED,I20//)
      WRITE (NPRT,140)
140
      FORMAT (10X,47HSTORAGE LOCATION INDEXES IN KDATA ARRAY (TEST)./)
      WRITE (NPRT,150) LTABI,LFFI,LPI,LPSI,LMAXI,NMAXI
150
      FORMAT (14X,15HFUNCTION TABLES,I21/14X,17HFORCING FUNCTIONS,I19/14X,12HETEST1170
1X,19HPLASTIC STRAIN DATA,I17/14X,19HSTRESS HISTORY DATA,I17/14X,12HETEST1170
2HEND OF ARRAY,I24/14X,16HSPACES ALLOCATED,I20//)
      TEST 890
      TEST 900
      TEST 910
      TEST 920
      TEST 930
      TEST 940
      TEST 950
      TEST 960
      TEST 970
      TEST 980
      TEST 990
      TEST 1000
      FOTEST1010
      LINTEST1020
      TEST1030
      TEST1040
      TEST1050
      TEST1060
      TEST1070
      TEST1080
      TEST1090
      TEST1100
      TEST1110
      TEST1120
      TEST1130
      TEST1140
      TEST1150
      TEST1160
      TEST1170
      TEST1180

```

160	WRITE (NPRT,160)		TEST1190
	FORMAT (1H,78H THIS TIME STEP IS REPEATED WITH THE ABOVE MEMBERS		TEST1200
	REATED AS INELASTIC (TEST).)		TEST1210
	IF (IYLD.LI.NM) GO TO 168		TEST1220
	WRITE (NPRT,164)		TEST1230
164	FORMAT (1H,38H ***** ALL ELEMENTS HAVE YIELDED. *****)		TEST1240
168	CALL PAGE		TEST1250
170	RETURN		TEST1260
	END		TEST1270

```

CTICS 0 10
SUBROUTINE TICS(TIMN,IGA)
C
C THIS IS A MACHINE DEPENDENT SUBROUTINE.
C
COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1 PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
COMMON/MAINBK/IANAL,ICUFV,IERR,IFAIL,IFOR,ILIN,IPAGE,IPLOT,IPRINT,TICS
1 IREC,ISTART,ISTOP,ISTRES,ITAPE,IUNITS,IYLD,LERR,LINE,NACC,NCM,TICS
2 NCRD,NDF,NDFJ,NDIS,NFF,NJOR,NINC,NJ,NJO,NJER,NL,NLD,
3 NLS,NLSR,NM,NMAS,NMAT,NMD,NPLOT,NPRT,NSAVE,NTAB,NTAPE,
4 NTIMES,NVEL,IINITD
COMMON/TIMEBK/TCUM,INIT,KNT
INTEGER HEAD,DHEAD
IGA = 1
IF(INIT.EQ.1) GO TO 20
INITIALIZE STARTING POINT
CALL SECOND(T)
INIT=1
TT=0.E0
GO TO 40
KNT = KNT + 1
TIMN = (SECOND(TIMN) - T)/60.E0
CALL SECOND(T)
TCUM=TCUM+TIMN
TPER=TCUM/KNT
TEX=TCUM+TPER
IF(TEX.GE.IPROB.OR.TIME.GT.THALT) IGA=2
IF(TEX.GE.TPROB) PRINT 30
FORMAT(1H,63H**ESTIMATED CALCULATION TIME EXCEEDS ALLOWED PROBLE
TICS 0
TICS 10
TICS 20
TICS 30
TICS 40
TICS 50
TICS 60
TICS 70
TICS 80
TICS 90
TICS 100
TICS 110
TICS 120
TICS 130
TICS 140
TICS 150
TICS 160
TICS 170
TICS 180
TICS 190
TICS 200
TICS 210
TICS 220
TICS 230
TICS 240
TICS 250
TICS 260
TICS 270
TICS 280

```



TICS 290  
TICS 300  
TICS 310  
TICS 320  
TICS 330  
TICS 340  
TICS 350  
TICS 360

1M (TICS)\*\*\*)  
TT=TT+TIMN  
IF(TT.GE.15.0E0) GO TO 50  
RETURN  
CALL REGO(-ISTART)  
TT=0.E0  
GO TO 40  
END

40  
50

```

C      CHIDE      0 10
C      SUBROUTINE WIDE (M,UR,UO,IFLAG)
C      THIS SUBROUTINE GENERATES STRESS AND ENERGY CALCULATIONS FOR A
C      WIDE FLANGE STEEL MEMBER(M). THE CALCULATIONS ARE CONTROLLED
C      BY (IFLAG), WHERE
C      IFLAG=1, INDICATES THAT THE RECOVERABLE STRAIN ENERGY(UR)
C      AND THE DISSIPATIVE STRAIN ENERGY (UO) ARE REQUIRED.
C      IFLAG=3, INDICATES THAT STRESS RESULTS ARE REQUIRED FOR PRINT-
C      OUT AND FOR UPDATING THE STRESS HISTORY DATA BANK.
C      THE ELASTIC-PLASTIC STATUS OF THE MEMBER IS INDICATED BY
C      ISTAT=MSTAT(M), WHERE
C      ISTAT=1, INDICATES A MEMBER THAT IS RESTRICTED TO LINEAR
C      ELASTIC RESPONSE.
C      ISTAT=2, INDICATES A MEMBER THAT IS CURRENTLY LINEAR ELASTIC
C      BUT MAY GO INELASTIC.
C      ISTAT=3, INDICATES A MEMBER THAT IS INELASTIC.
C
C      COMMON DATA(10000),KDATA(500)
C      COMMON/ELEMENT/ICARD,IP(45),IPL(20),IQ(45),IQL(20),MATR(45),
1     MATW(45),MBAR(10,45),MCOE(45),MSHEAR(45),MSTAT(45),MTIES(45),
2     NTYPE(45),NGRP(45),NSPAC(6,45),NTIES(45)
C      COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),
1     SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)
C      COMMON/LEADBK/AVDM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1     PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPROB
C      INTEGER HEAD,DHEAD
C      COMMON/MEMBER/AGRP(10,45),ATIES(6,45),BMEM(45),BPP(45),9DM(10,45),
1     9WF(45),D(45),DP(45),OPP(45),DMF(45),EFFL(10,45),EFLM(45),
2     HMEM(45),HTOP(45),HTWF(45),PDP(7,45),SPRING(5,20),STIES(7,45),
3     TFWF(45),TWWF(45),UDM(45),URM(45),XBEG(10,45),

```

WIDE 0  
 WIDE 10  
 WIDE 20  
 WIDE 30  
 WIDE 40  
 WIDE 50  
 WIDE 60  
 WIDE 70  
 WIDE 80  
 WIDE 90  
 WIDE 100  
 WIDE 110  
 WIDE 120  
 WIDE 130  
 WIDE 140  
 WIDE 150  
 WIDE 160  
 WIDE 170  
 WIDE 180  
 WIDE 190  
 WIDE 200  
 WIDE 210  
 WIDE 220  
 WIDE 230  
 WIDE 240  
 WIDE 250  
 WIDE 260  
 WIDE 270  
 WIDE 280

```

4   XBEGM(45),XBEGS(6,45),XL(45),XPI(5,45),YBAR(10,45),YGP(7,45),
5   YFIBR(11,45),YLOS(45),XDM(45),PDF(7,45),DISM(45)
COMMON/STORE/LCURV,LFF,LFFI,LMAXI,LMAX,LP,LPI,LPSI,LTAB,
1   LTABI,NMAX,NMAXI
COMMON/STRNBK/SRP(4),SRQ(4),UX,UY,UZ,XLEN,AREA,ZZI,IMAT

C   DIMENSION GPS(7,3),UDMP(7,3),URMP(7,3),GAUSS(3)
C
C   INITIALIZE
C
C   ISTAT = MSTAT(M)
C   IMAT=MATW(M)
C   XLEN=XL(M)
C   GAUSS(1)=5.E0/9.E0
C   GAUSS(2)=8.E0/9.E0
C   GAUSS(3)=GAUSS(1)
C   UR=0.E0
C   DETERMINE LOCAL DEFORMATIONS
C   CALL DEFO(M)
C   CHECK FOR INELASTIC DEFORMATIONS.
C   UD=0.E0
C   IF(ISTAT.EQ.3) UD=UDM(M)
C   OBTAIN ADDRESSES OF STRAIN AND STRESS HISTORY STORAGE.
C   KRAIN=KDATA(LPI +M)-1
C   KRESS=KDATA(LPSI+M)-1
C
C   EVALUATE STRESSES AND ENERGY DENSITIES AT GAUSS POINTS.
C   KR=KRAIN
C   KS=KRESS
C   DO 100 I=1,7

```

```

WIDE 290
WIDE 300
WIDE 310
WIDE 320
WIDE 330
WIDE 340
WIDE 350
WIDE 360
WIDE 370
WIDE 380
WIDE 390
WIDE 400
WIDE 410
WIDE 420
WIDE 430
WIDE 440
WIDE 450
WIDE 460
WIDE 470
WIDE 480
WIDE 490
WIDE 500
WIDE 510
WIDE 520
WIDE 530
WIDE 540
WIDE 550
WIDE 560
WIDE 570
WIDE 580

```

```

DO 90 J=1,3
CALL STRN(M,XPI(J,M),YGP(I,M),GPS(I,J))
IF(ABS(GPS(I,J)).LT.TINY) GPS(I,J)=TINY
IF(ISTAT.EQ.3) GO TO 50
DO 40 L=1,9
S(L)=0.E0
GO TO 70
40
50 S(9)=DATA(KR+J)
LS=KS+8*(J-1)
DO 60 L=1,8
S(L)=DATA(LS+L)
60
70 CALL REIN(IMAT,GPS(I,J),URMP(I,J),UDMP(I,J))
C UPDATE IF IFLAG=3.
IF(IFLAG.NE.3.OR.ISTAT.NE.3) GO TO 90
DATA(KR+J)=S(9)
DO 80 L=1,8
DATA(LS+L)=S(L)
80
90 CONTINUE
KR=KR+3
100 KS=KS+24
C
C OBTAIN ENERGY CONTRIBUTION OF FLANGES AND WEB.
C
CONF=8WF(M)*TFWF(M)*XLEN/4.E0
CONW=TWWF(M)*(DWF(M)-2.E0*TFWF(M))*XLEN/4.E0
DO 110 I=1,2
DO 110 J=1,3
UR=UR+GAUSS(J)*URMP(I,J)*CONF
UD=UD+GAUSS(J)*UDMP(I,J)*CONF
110 DO 120 I=1,3

```

```

WIDE 590
WIDE 600
WIDE 610
WIDE 620
WIDE 630
WIDE 640
WIDE 650
WIDE 660
WIDE 670
WIDE 680
WIDE 690
WIDE 700
WIDE 710
WIDE 720
WIDE 730
WIDE 740
WIDE 750
WIDE 760
WIDE 770
WIDE 780
WIDE 790
WIDE 800
WIDE 810
WIDE 820
WIDE 830
WIDE 840
WIDE 850
WIDE 860
WIDE 870
WIDE 880

```



```

120      DO 120 J=1,3
          UR=UR+GAUSS(I)*GAUSS(J)*URMP(I+2,J)*CONW
          UD=UD+GAUSS(I)*GAUSS(J)*UDMP(I+2,J)*CONW
          DO 130 I=6,7
              DO 130 J=1,3
                  UR=UR+GAUSS(J)*URMP(I,J)*CONF
                  UD=UD+GAUSS(J)*UDMP(I,J)*CONF
130      C
C      STORE MEMBER ENERGY AND MEMBER END STATE DATA IF IFLAG=3
C
          IF(IFLAG.NE.3) GO TO 170
          URM(M)=UR
          UDM(M)=UD
          IF(ISTAT.NE.3) GO TO 170
          KR=KRAIN+21
          KS=KRESS+168
          DO 160 I=1,2
              XL0C=0.E0
              IF(I.EQ.2) XL0C=XL0N
              DO 150 K=1,11
                  CALL STRN(M,XL0C,YFIBR(K,M),STRAIN)
                  IF(ABS(STRAIN).LT.TINY) STRAIN=TINY
                  S(9)=DATA(KR+K)
                  LS=KS+8*(K-1)
              DO 135 L=1,8
                  S(L)=DATA(LS+L)
                  CALL REIN (IMAT,STRAIN,URE,UDE)
                  DATA(KR+K)=S(9)
              DO 140 L=1,8
                  DATA(LS+L)=S(L)
135      C
140      C

```

```

WIDE 890
WIDE 900
WIDE 910
WIDE 920
WIDE 930
WIDE 940
WIDE 950
WIDE 960
WIDE 970
WIDE 980
WIDE 990
WIDE1000
WIDE1010
WIDE1020
WIDE1030
WIDE1040
WIDE1050
WIDE1060
WIDE1070
WIDE1080
WIDE1090
WIDE1100
WIDE1110
WIDE1120
WIDE1130
WIDE1140
WIDE1150
WIDE1160
WIDE1170
WIDE1180

```

```

150 CONTINUE
   KR=KR+11
160 KS=KS+88
170 RETURN
C ***** GLOSSARY *****
C CON = TEMPORARY CONSTANT.
C IMAT = MATERIAL NUMBER OF WIDE FLANGE.
C KR = STRAIN INDEX FOR EACH FIBER.
C KS = STRESS INDEX FOR EACH FIBER.
C R = STRAIN AT MESH POINTS.
C UD = DISSIPATIVE ENERGY DENSITY FOR MEMBER.
C UR = RECOVERABLE ENERGY DENSITY FOR MEMBER.
C XLN = LENGTH OF MEMBER.
C

```

```

CZOCK      0 10
           BLOCK DATA

C
C
C      THIS SUBPROGRAM INITIALIZES VARIABLES STORED IN LABELED COMMON.

COMMON/FIBER/DENS(9),EC(9),EPSU(9),ET(9),FCFY(9),G(9),PR(9),S(9),
1  SLOPE(8,9),ST(17,6),STN(8,9),STS(8,9),UNLK(9),ICODE(9),NAME(9)
COMMON/LEADBK/AVOM,AVGL,CA,CB,CC,CD,CE,DHEAD(20),DT,EPS,HEAD(20),
1  PI,RERF,RERH,RERZ,SERR,TBEGIN,THALT,TIME,TINK,TINY,TPRO3
INTEGER HEAD,DHEAD
COMMON/SAVEBK/SAVACC(3,50),SAVAXL(2,45),SAVCRV(2,45),SAVMOM(2,45)
1  ,SAVSHR(2,45),SAVSRP(3,20),SAVSRQ(3,20),SAVXDJ(3,50),
2  SAVVEL(3,50),SVSTRN(12,45),SVSTRS(12,45)

C
DATA PI/3.1415926535898E0/,TPROB/20.E0/
DATA ST/33.E3,0.E0,33.E3,33.E3,49.E3,56.E3,58.E3,56.E3,2.57E4,
1  0.E0,.114E-2,.14E-1,.59E-1,.104E0,.150E0,.210E0,8.88E-4,
2  36.E3,0.E0,36.E3,36.E3,52.E3,58.E3,60.E3,59.E3,2.91E4,
3  0.E0,.125E-2,.14E-1,.59E-1,.104E0,.150E0,.200E0,1.01E-3,
4  40.E3,0.E0,40.E3,40.E3,66.E3,77.E3,80.E3,76.E3,1.49E4,
5  0.E0,.138E-2,.230E-1,.62E-1,.101E0,.140E0,.200E0,5.14E-4,
6  50.E3,0.E0,50.E3,50.E3,72.E3,89.E3,92.E3,90.E3,3.58E4,
7  0.E0,.173E-2,.13E-1,.48E-1,.84E-1,.12E0,.154E0,1.237E-3,
8  60.E3,0.E0,60.E3,60.E3,90.E3,103.E3,106.E3,100.E3,5.42E4,
9  0.E0,.208E-2,.60E-2,.33E-1,.60E-1,.87E-1,.136E0,1.879E-3,
$  75.E3,0.E0,75.E3,75.E3,110.E3,124.E3,130.E3,124.E3,7.5E4,
$  0.E0,.260E-2,.27E-2,.26E-1,.50E-1,.73E-1,.115E0,2.60E-3/
DATA SAVACC,SAVAXL,SAVCRV,SAVMOM,SAVSHR,SAVSRP,SAVSRQ,
1 SAVXDJ,SAVVEL,SVSTRN,SVSTRS/2010*0.E0/
END

```

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